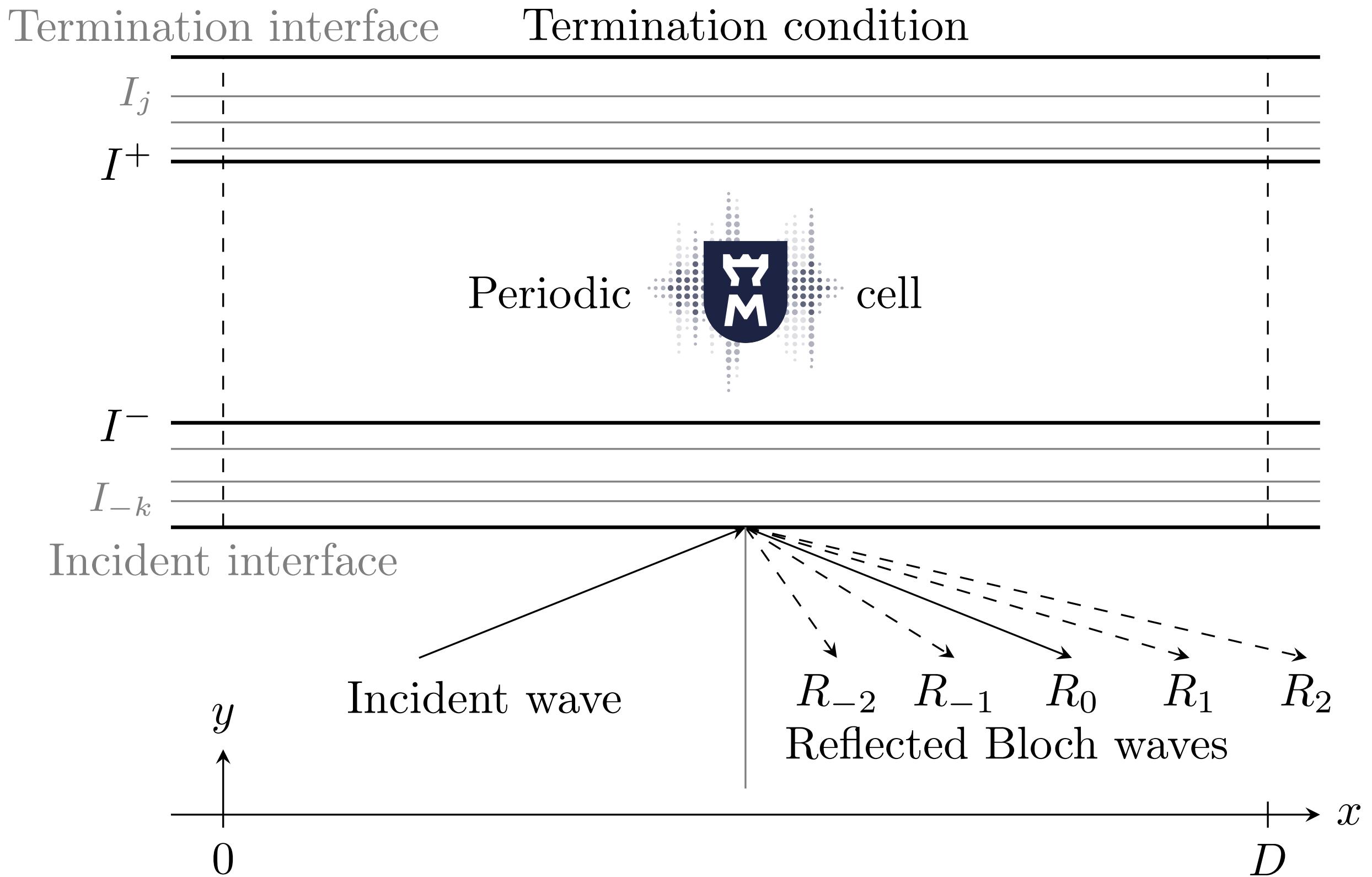


A recursive method to evaluate the scattering properties of grating stacks

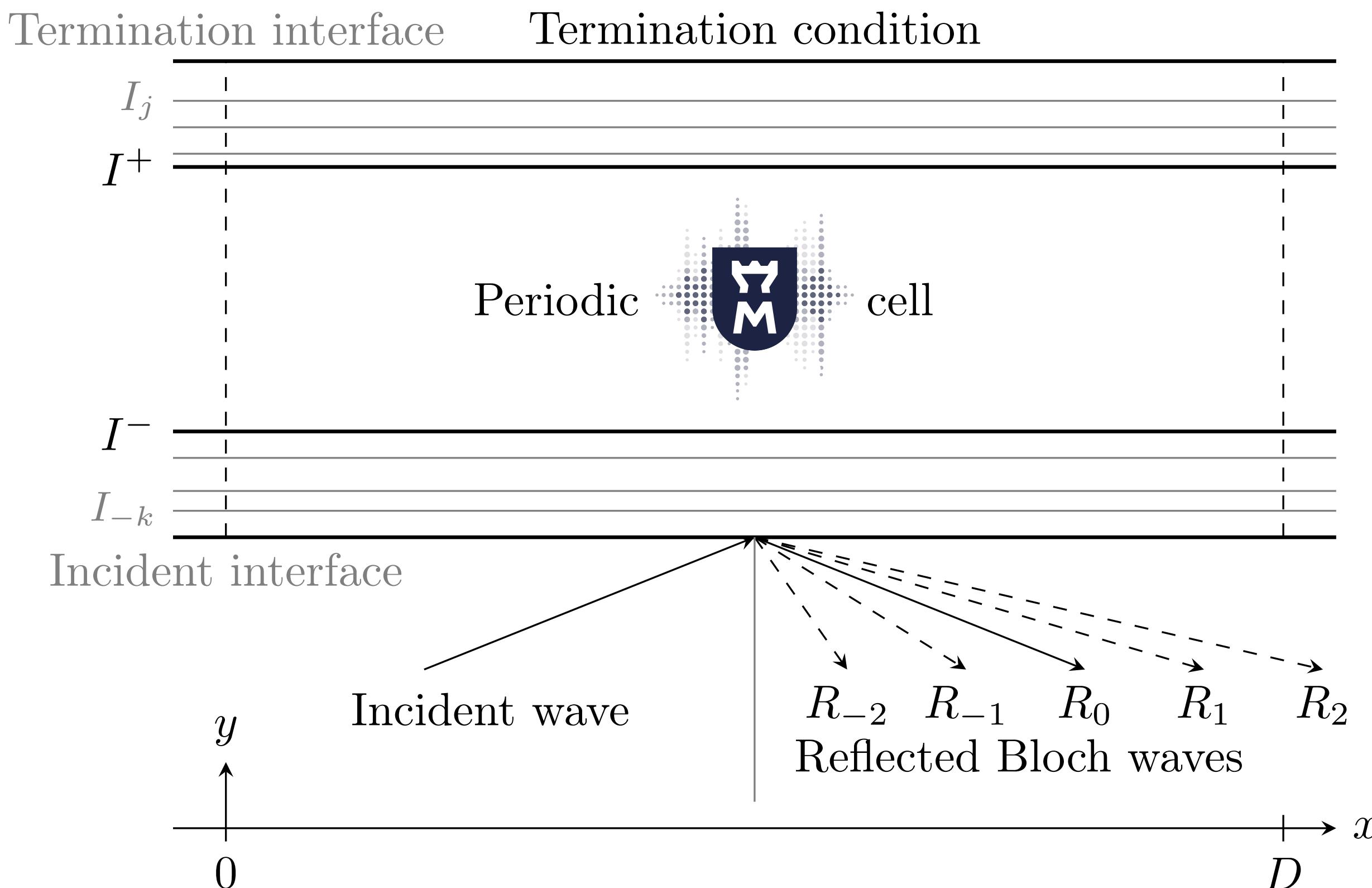
O. Dazel, M. Gaborit, and J.-P. Groby

Laboratoire d'Acoustique de l'Université du Mans (LAUM - UMR CNRS 6613)
Institut d'Acoustique - Graduate School (IA-GS) | Le Mans Université, France

Models for the acoustic response of grating stacks



Models for the acoustic response of grating stacks



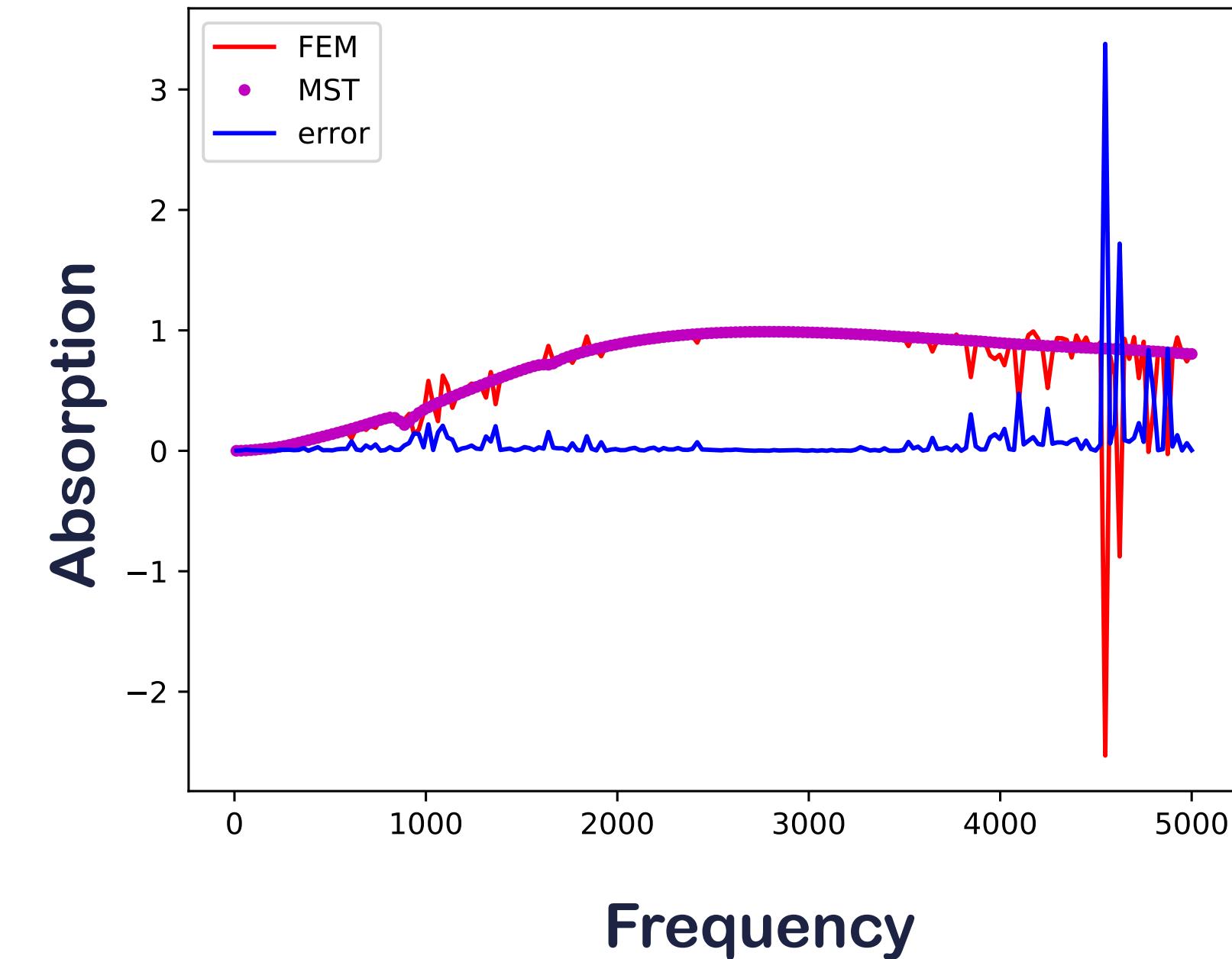
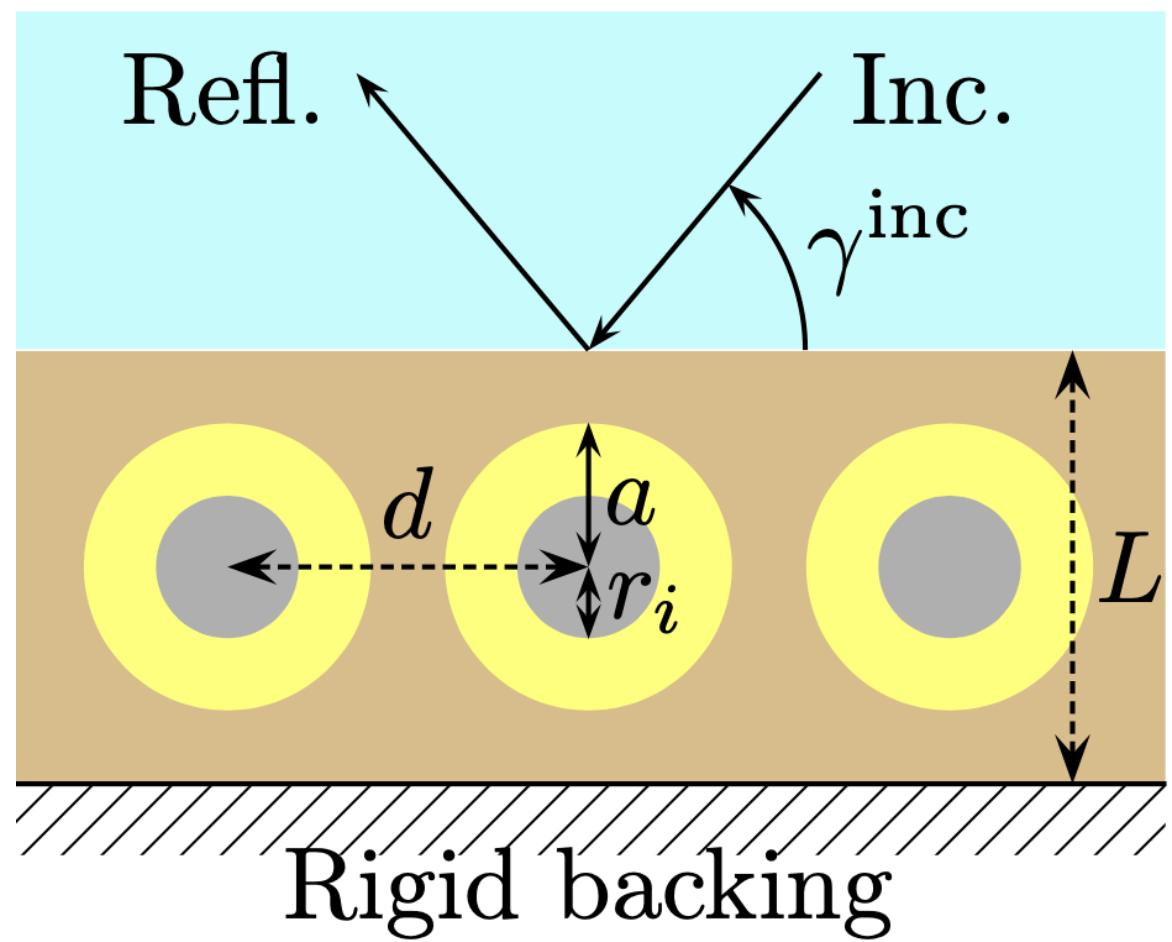
Comsol
Not the exact solution, Lots of dofs, PML, not fun ...

Gaborit et al AAA (2018)
Case of elastic plate, coupled problem

Parinello et al. JSV (2019)
Periodic TMM,
only nodal dofs (limited to quadratic elements)

Dazel et al. (CFA 2022)
Generalisation of Parinello's method,
available for higher orders

TMM and evanescent waves : stability issues



- Poroelastic core
- Bicomposite poroelastic steel inclusion

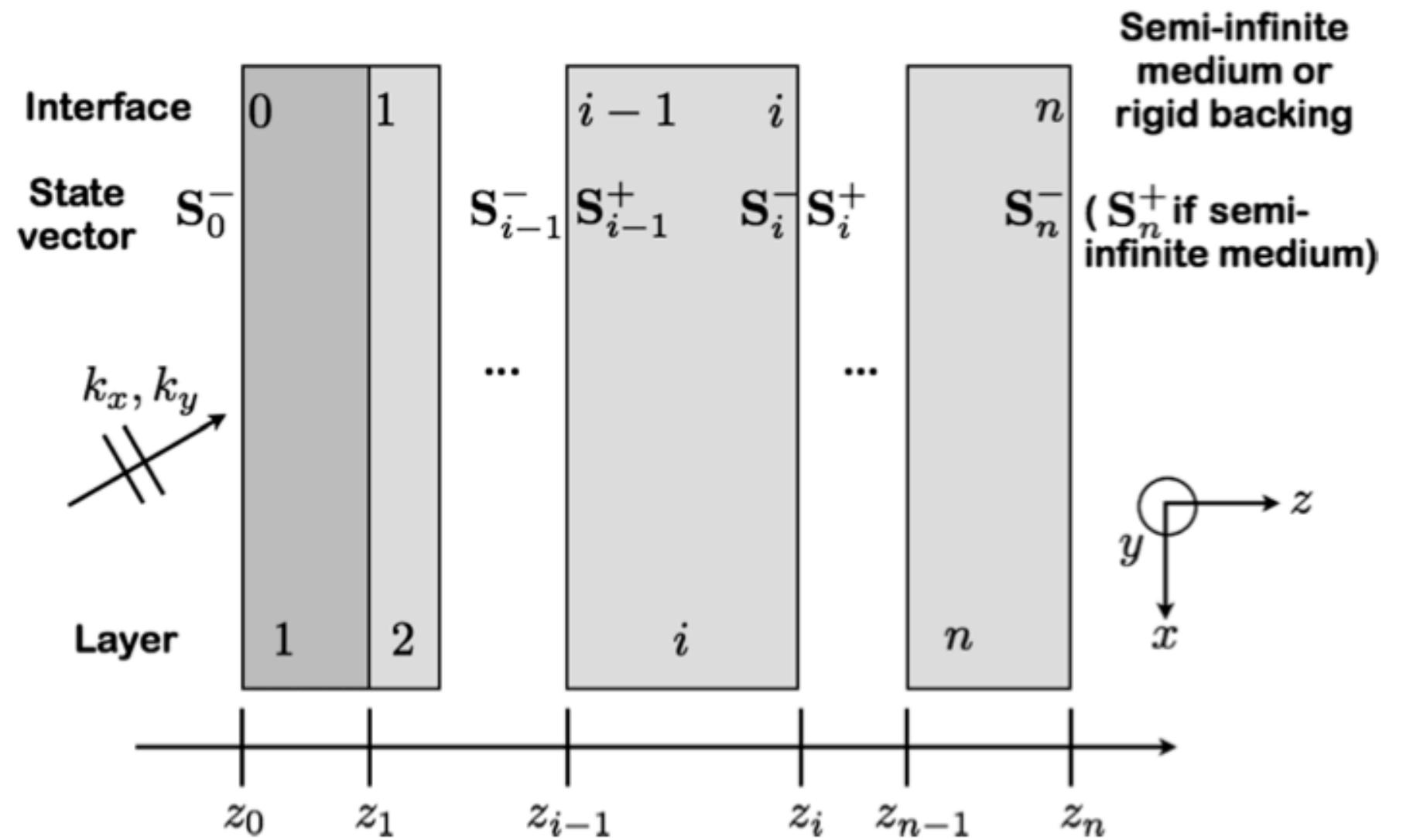
Origin of the instabilities

- Evanescent waves in TMM
- Boundary conditions in FEM

Objective of the presentation:
Adapt a stable recursive scheme to grating stacks (couple it with periodic FEM)

The Transfer Matrix Method

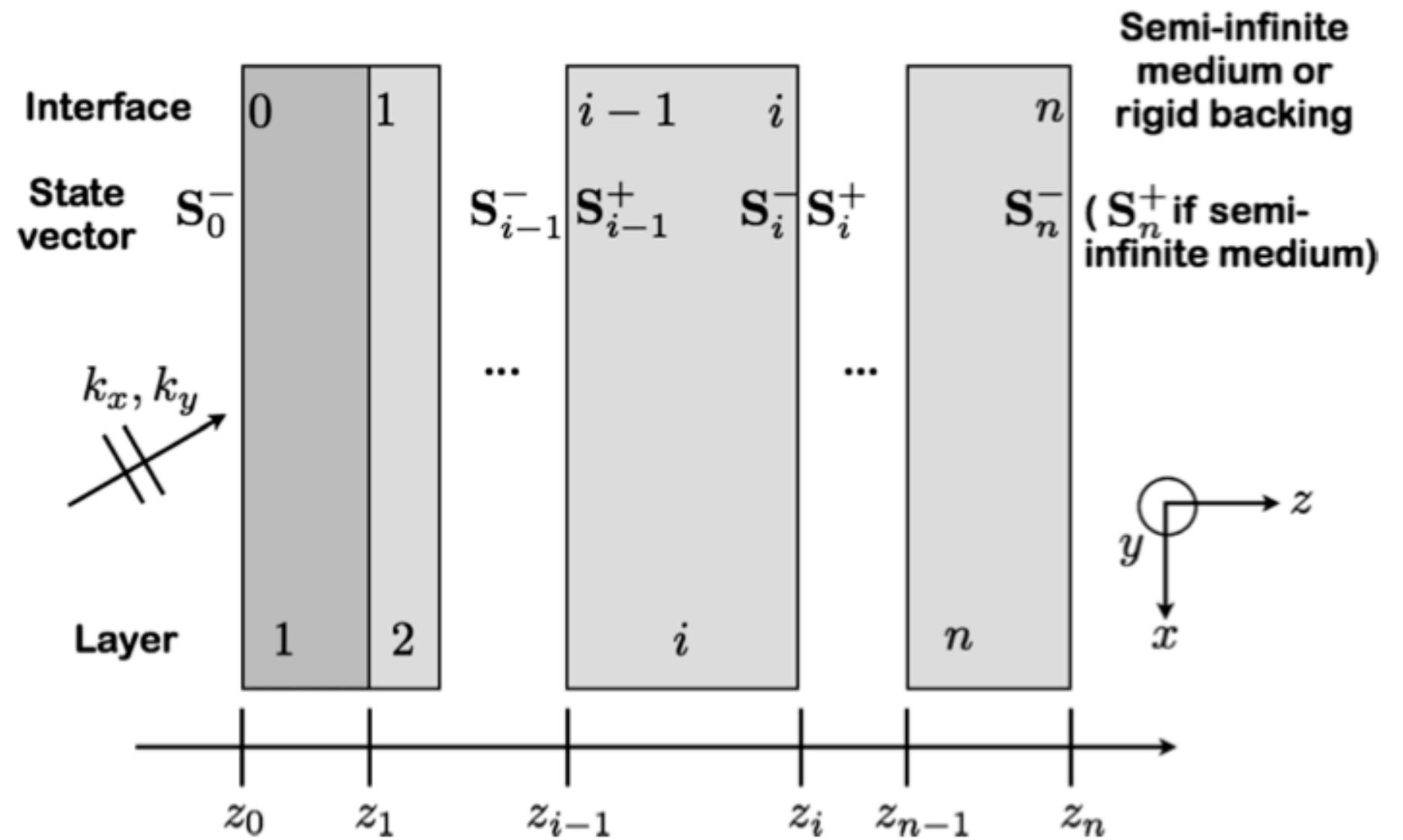
Thomson, JAP (1950)
Haskell, Bull. Seismol Soc. (1953)
Brouard et al., JSV (1995)



- Multilayer (plane) structures
- Plane (or quasi-plane if anisotropy) waves
- “Cheap”

The Transfer Matrix Method

Thomson, JAP (1950)
Haskell, Bull. Seismol Soc. (1953)
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- Multilayer (plane) structures
- Plane (or quasi-plane if anisotropy) waves
- “Cheap”

$$\mathbf{S}(z) = \begin{Bmatrix} p(z) \\ u_z(z) \end{Bmatrix}$$

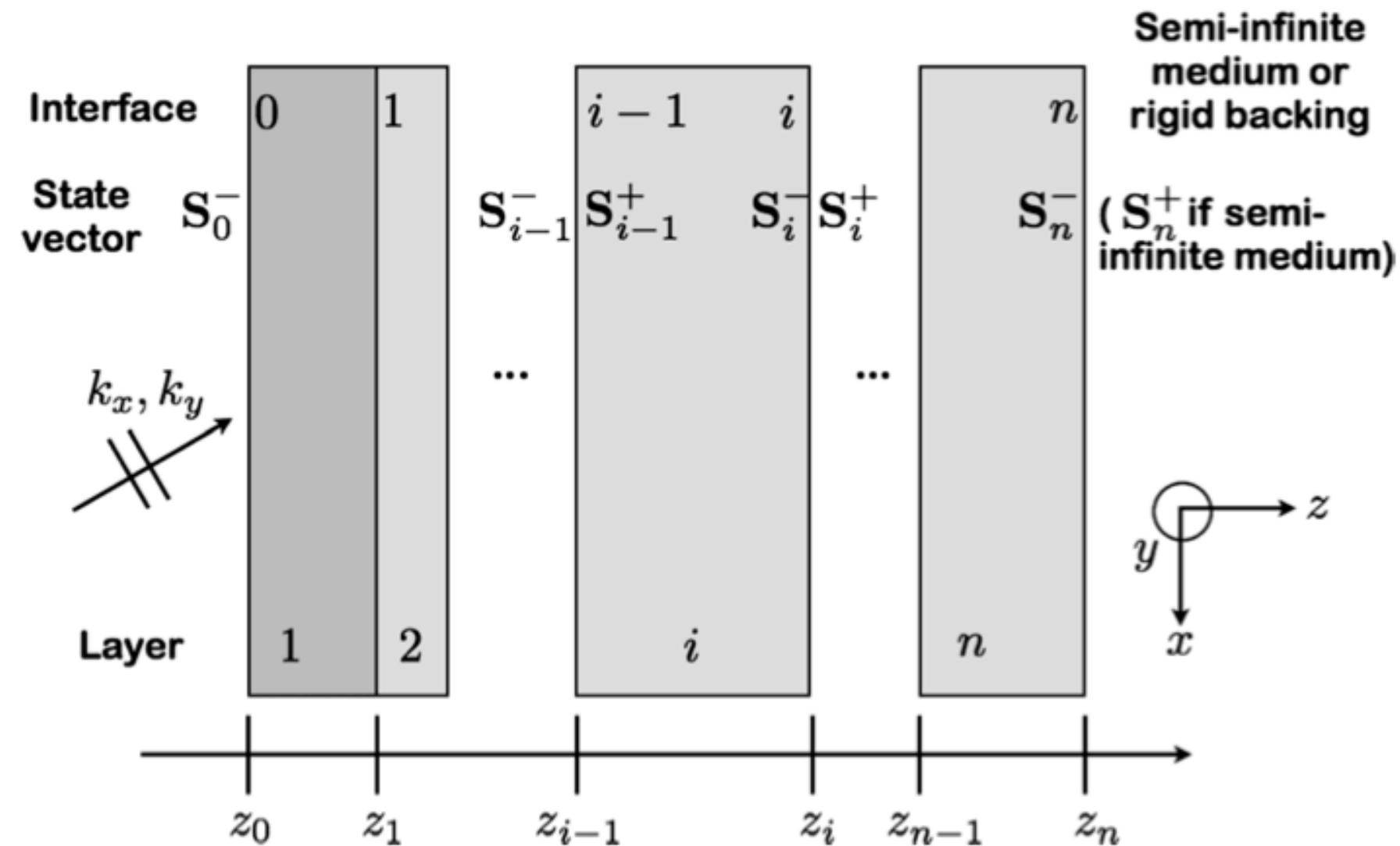
$$\mathbf{S}_i^- = [\mathbf{T}_i] \mathbf{S}_{i-1}^+$$

$$\mathbf{S}'(z) = [\alpha] \mathbf{S}(z)$$

$$[\mathbf{T}_i] = \exp(d_i[\alpha])$$

The Transfer Matrix Method

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Haskell, Bull. Seismol Soc. (1953)
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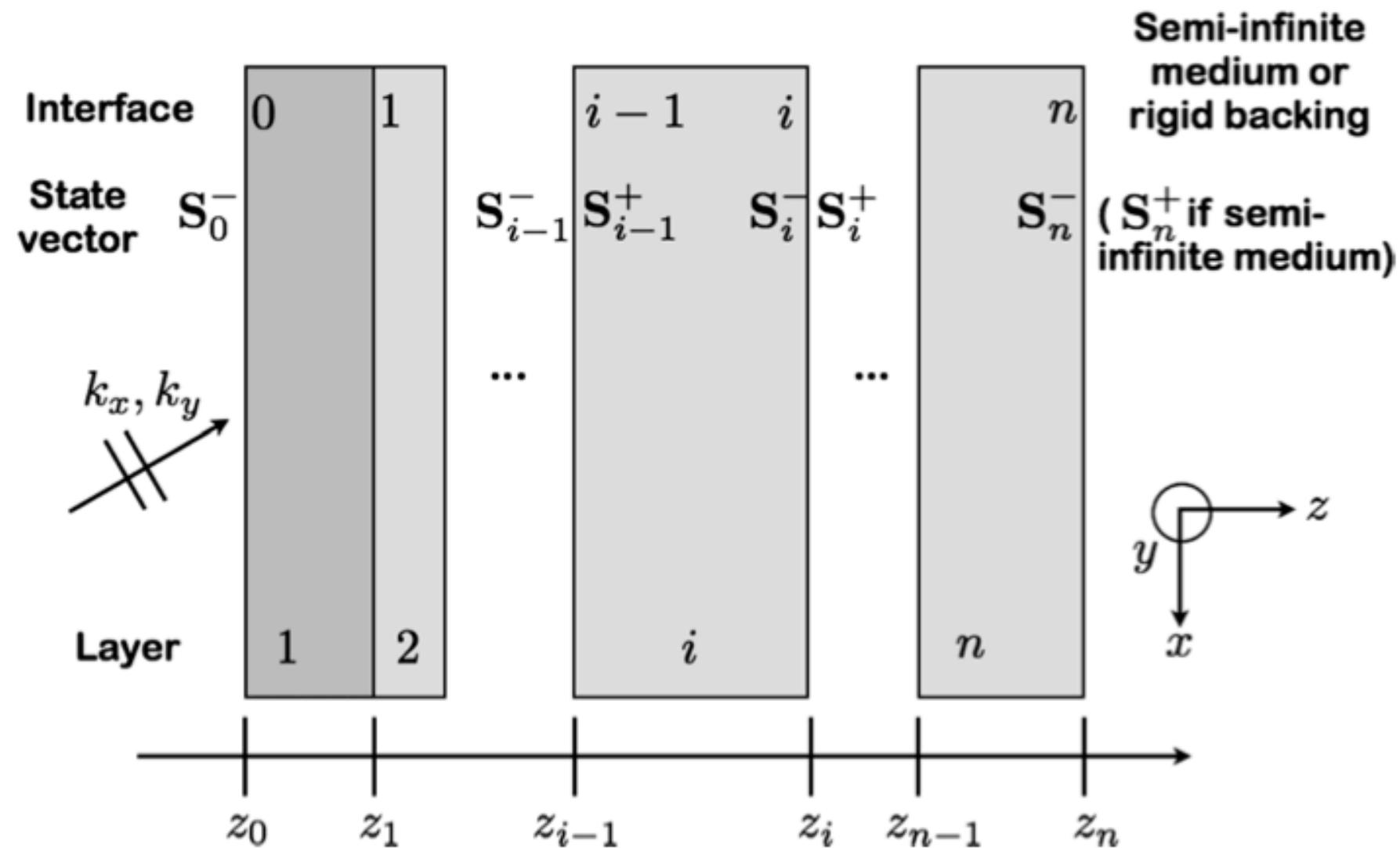
$$S'(z) = [\alpha] S(z)$$

$$[T_i] = \exp(d_i[\alpha])$$

- Choice of physical fields in the State Vector
- Relations at interfaces
 - Continuity of displacements
 - Continuity of stress
- Unstable
 - By nature
 - High frequencies
 - Highly damped materials

The Transfer Matrix Method

Thomson, JAP (1950)
 Haskell, Bull. Seismol Soc. (1953)
 Brouard et al., JSV (1995)



Medium of same type

$$[\mathbf{T}] = \prod_{i=1}^n [\mathbf{T}_i]$$

If not: a global system

- Multilayer (plane) structures
- Plane (or quasi-plane if anisotropy) waves
- “Cheap”

$$\mathbf{S}(z) = \begin{Bmatrix} p(z) \\ u_z(z) \end{Bmatrix}$$

$$\mathbf{S}_i^- = [\mathbf{T}_i] \mathbf{S}_{i-1}^+$$

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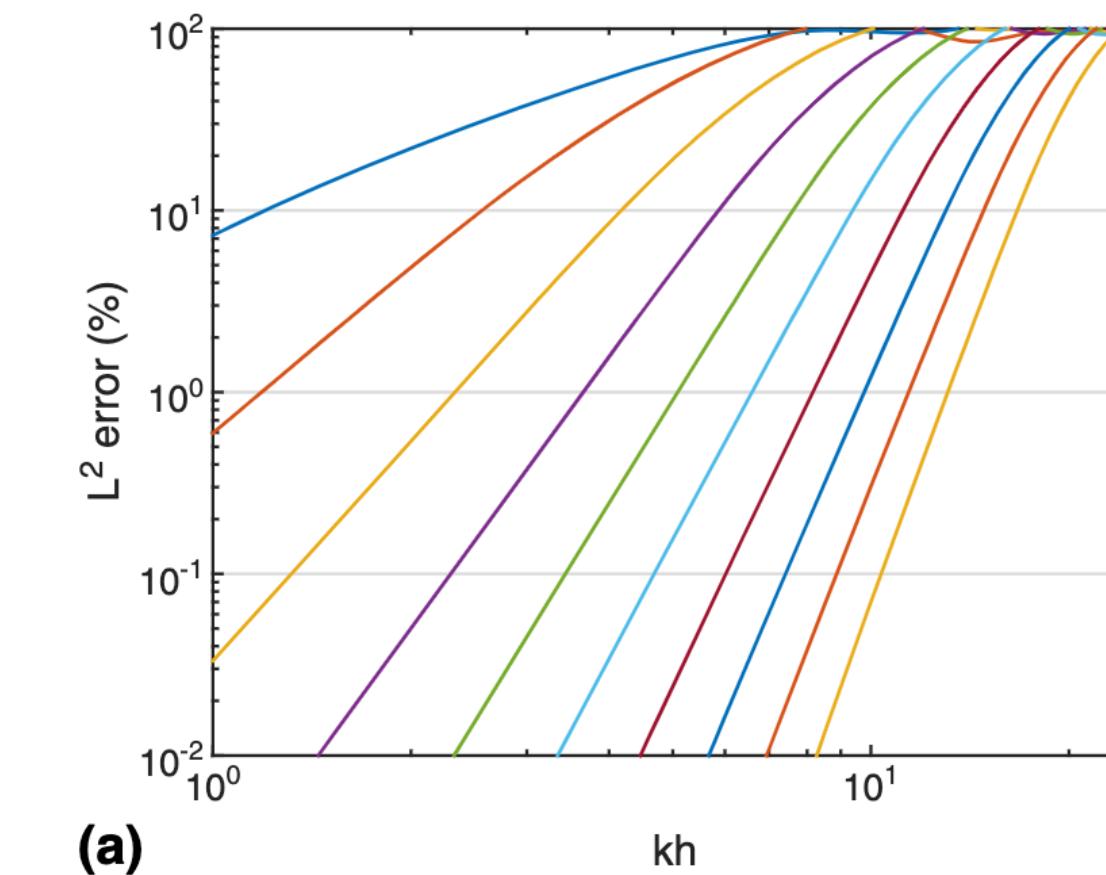
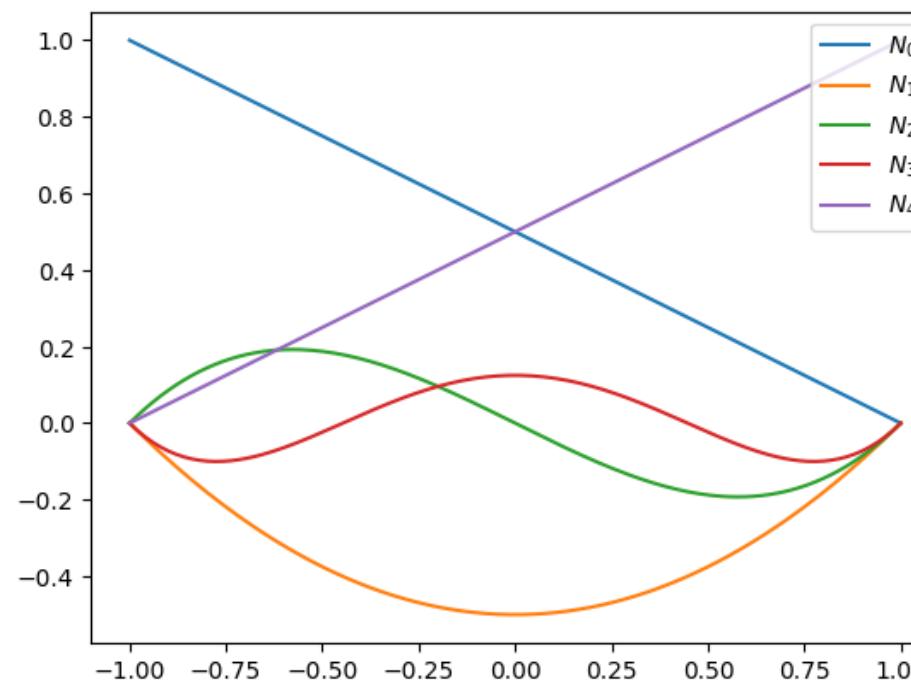
Finite-Element Method (higher order)

Šolín et al. Chapman & Hall (2003)
Bériot et al. IJNME (2016)
Jonckheere et al. IJNME (2022)

Weak form for a fluid

$$\forall q, \int_{\Omega} \nabla p \cdot \nabla q - k^2 p q \, d\Omega = \int_{\partial\Omega} \frac{\partial p}{\partial n} q \, dS$$

Lobatto shape functions



Stabilised implementation

$$\forall q, \int_{\Omega} \nabla p \cdot \nabla q - k^2 p q \, d\Omega + \int_{\partial\Omega} ik p q \, dS = \int_{\partial\Omega} \left(\frac{\partial p}{\partial n} + ik p \right) q \, dS$$

Incoming characteristics



Concept of characteristics

$$\begin{bmatrix} \mathbf{P}_1^+ & | & \mathbf{P}_1^- \end{bmatrix} \begin{Bmatrix} q_1^+ \\ q_1^- \end{Bmatrix} = \mathbf{S}_1 = \begin{Bmatrix} \frac{\partial p_1}{\partial n} \\ p_1 \end{Bmatrix}$$
$$\begin{Bmatrix} q_1^+ \\ q_1^- \end{Bmatrix} = \begin{Bmatrix} \frac{\partial p_1}{\partial n} - ikp_1 \\ \frac{\partial p_1}{\partial n} + ikp_1 \end{Bmatrix} \quad \begin{array}{c} \xrightarrow{q_1^+} \\ \xleftarrow{q_1^-} \end{array}$$

Fluid

Concept of characteristics

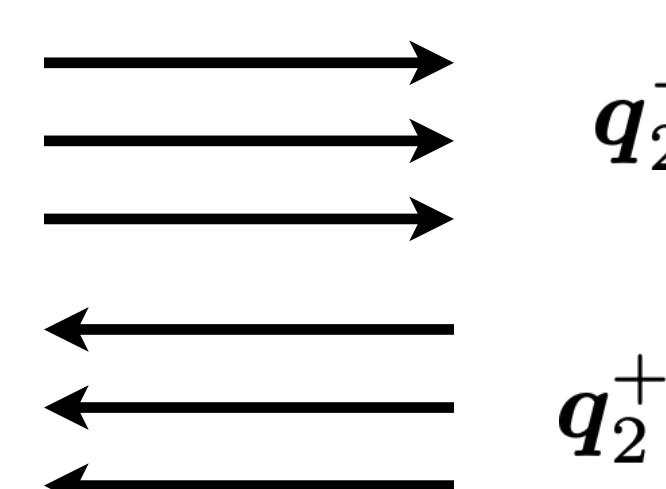
$$[\mathbf{P}_1^+ \quad | \quad \mathbf{P}_1^-] \begin{Bmatrix} q_1^+ \\ q_1^- \end{Bmatrix} = \mathbf{S}_1 = \begin{Bmatrix} \frac{\partial p_1}{\partial n} \\ p_1 \end{Bmatrix}$$
$$\begin{Bmatrix} q_1^+ \\ q_1^- \end{Bmatrix} = \begin{Bmatrix} \frac{\partial p_1}{\partial n} - ikp_1 \\ \frac{\partial p_1}{\partial n} + ikp_1 \end{Bmatrix}$$

Fluid

q_1^+
 \longleftarrow
 q_1^-

- Can be determined analytically (for all types of medium)
- # Characteristics = # Fields in the SV
- # relations at an interface = # incoming characteristics

Poroelastic material



The diagram illustrates the concept of characteristics across an interface. On the left, labeled 'Fluid', two horizontal arrows point right, labeled q_1^+ . On the right, labeled 'Poroelastic material', two horizontal arrows point left, labeled q_1^- . Between them, a vertical line contains five horizontal arrows pointing right, labeled q_2^- , and five horizontal arrows pointing left, labeled q_2^+ .

Concept of characteristics

$$[\boldsymbol{P}_1^+ \quad | \quad \boldsymbol{P}_1^-] \begin{Bmatrix} q_1^+ \\ q_1^- \end{Bmatrix} = \boldsymbol{S}_1 = \begin{Bmatrix} \frac{\partial p_1}{\partial n} \\ p_1 \end{Bmatrix} \quad | \quad \begin{matrix} \bullet \\ \bullet \\ \vdots \end{matrix}$$

$$\begin{aligned} \left\{ \begin{array}{l} q_1^+ \\ q_1^- \end{array} \right\} &= \left\{ \begin{array}{l} \frac{\partial p_1}{\partial n} - ikp_1 \\ \frac{\partial p_1}{\partial n} + ikp_1 \end{array} \right\} \quad \begin{array}{c} q_1^+ \\ \longrightarrow \\ q_1^- \end{array} \\ &\quad \left| \begin{array}{c} \longrightarrow \\ \longleftarrow \end{array} \right. \quad \begin{array}{c} q_2^- \\ \longrightarrow \\ q_2^+ \end{array} \end{aligned}$$

Fluid

Poroelastic material

- Can be determined analytically (for all types of medium)
 - # Characteristics = # Fields in the SV
 - # relations at an interface = # incoming characteristics

Well-posedness problem [Hadamard; Kreiss, Higdon]:

$$\begin{Bmatrix} q_1^- \\ q_2^+ \end{Bmatrix} = \begin{bmatrix} [R_{11}] & [T_{12}] \\ [T_{12}] & [R_{22}] \end{bmatrix} \begin{Bmatrix} q_1^+ \\ q_2^- \end{Bmatrix}$$

- Discontinuous Galerkin Methods
 - Mode matching
 - Domain decomposition
 - No a priori choice

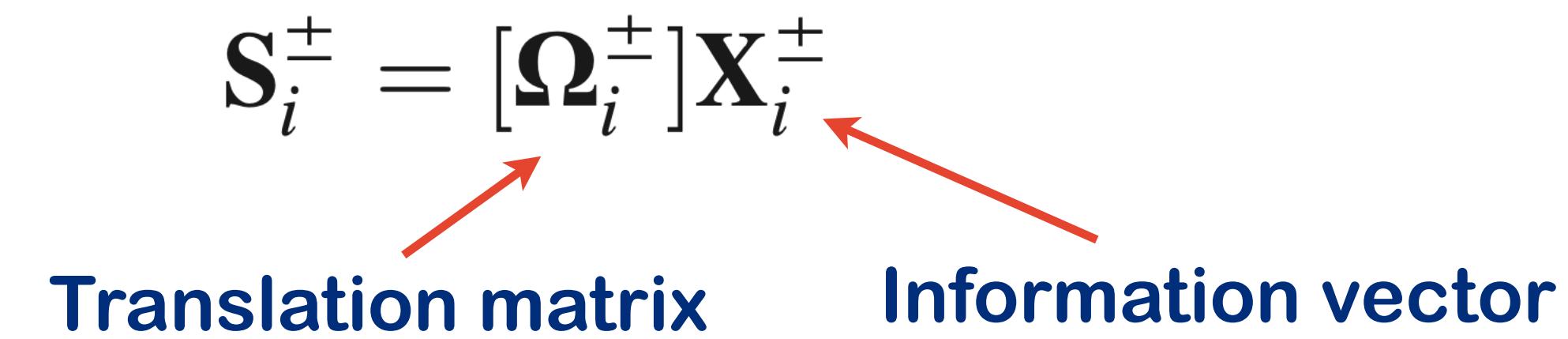
Recursive method

- Fix the stability problem of TMM
- Redaction could have been better

Dazel et al. JAP 2013

$$\mathbf{S}_i^\pm = [\boldsymbol{\Omega}_i^\pm] \mathbf{X}_i^\pm$$

Translation matrix Information vector





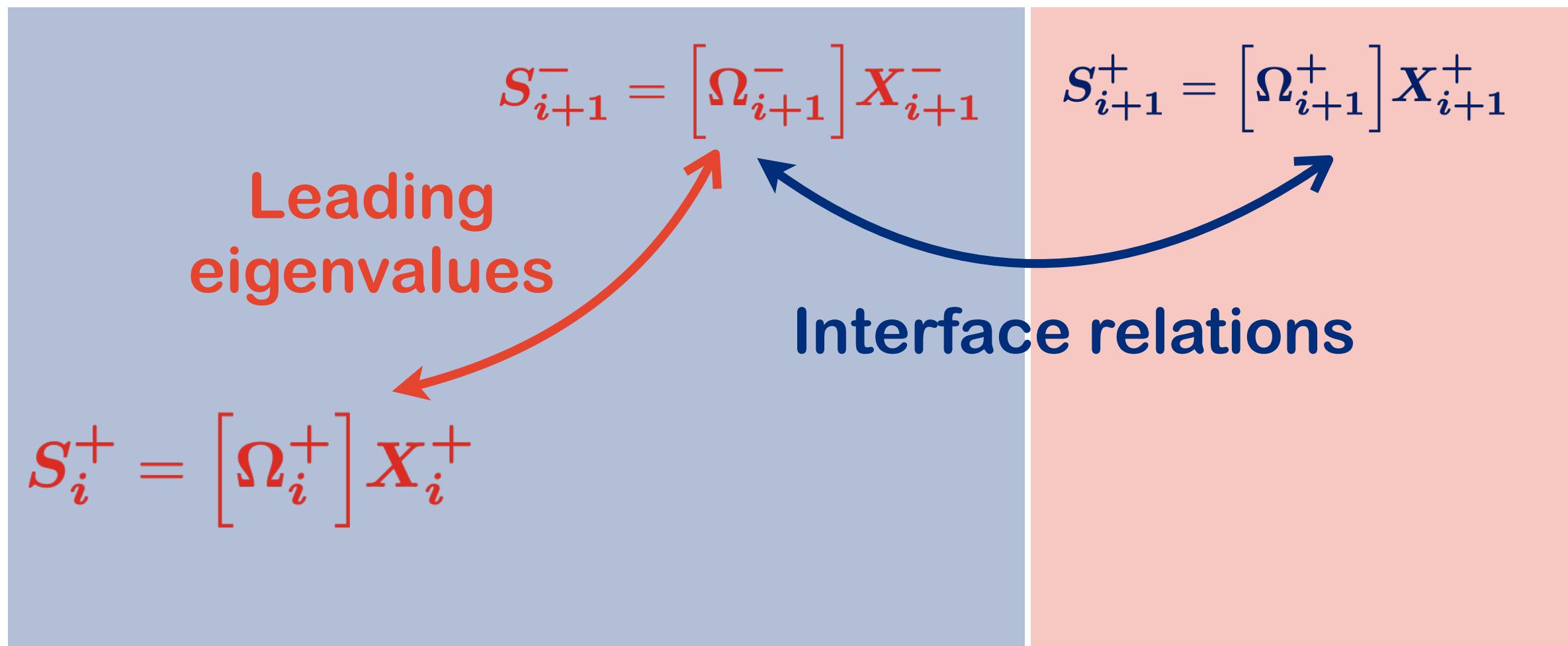
Recursive method

- Fix the stability problem of TMM
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Dazel et al. JAP 2013

$$S_i^\pm = [\Omega_i^\pm] X_i^\pm$$

Translation matrix Information vector



```
_list = [0.]*m+[1.] +[np.exp(-(lambda_[m+i]-lambda_[m-1])*self.d) for i in range(m)]
Lambda = np.diag(np.array(_list))
alpha_prime = Phi.dot(Lambda).dot(Phi_inv) # Eq (21)

xi_prime = Phi_inv[:m,:] @ Om # Eq (23)
_list = [np.exp(-(lambda_[m-1]-lambda_[i])*self.d) for i in range(m-1)] + [1.]
xi_prime_lambda = LA.inv(xi_prime).dot(np.diag(_list))
Om = alpha_prime.dot(Om).dot(xi_prime_lambda)

Om[:,m-1] += Phi[:,m-1]

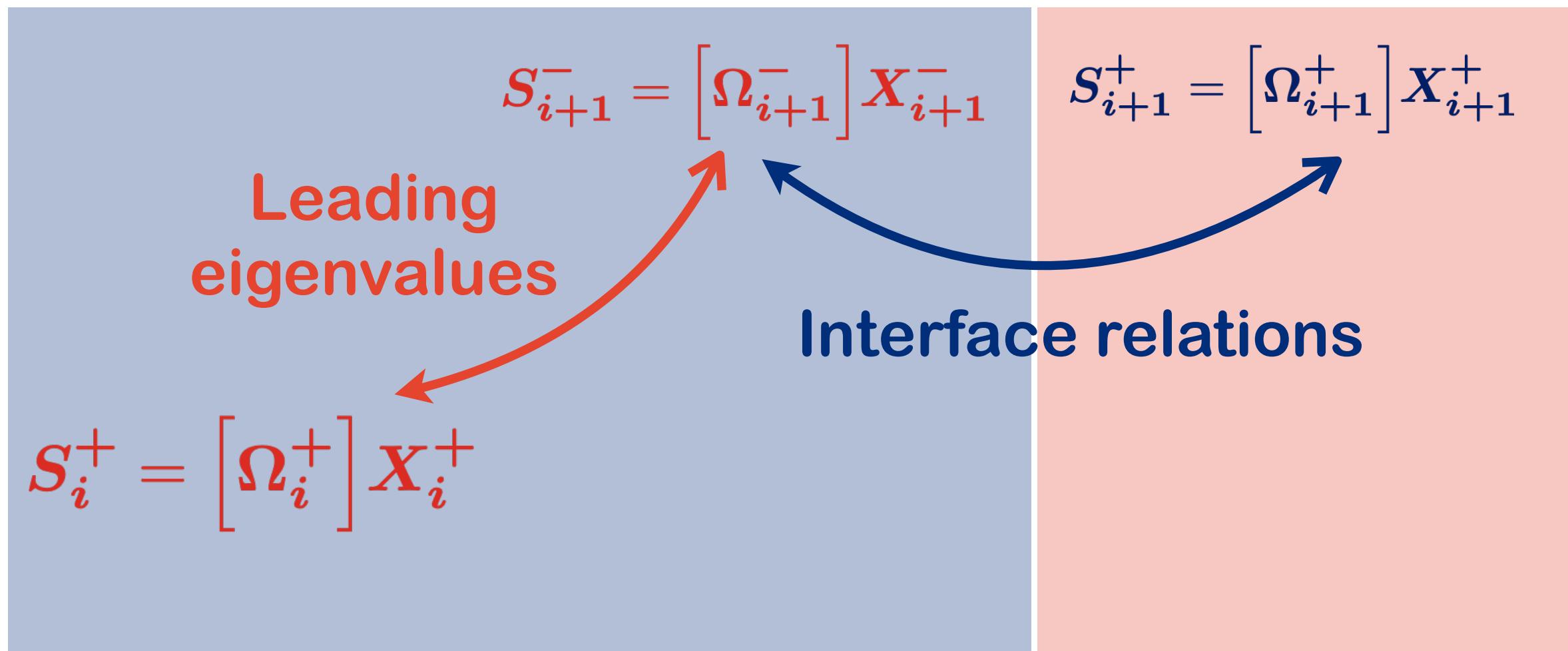
Xi = xi_prime_lambda*np.exp(lambda_[m-1]*self.d)
return Om, Xi
```



Recursive method

- Fix the stability problem of TMM
- Redaction could have been better

Dazel et al. JAP 2013



$$S_i^\pm = [\Omega_i^\pm] X_i^\pm$$

Translation matrix Information vector

- All types of physical media
- Extension to anisotropic materials Parra-Martinez et al. JAP 2016
- Code available on github <https://github.com/cpplanes/pymls>
- No global system
- Significance of the information vector ?
- A-priori in the interface relations
- Not valid at normal incidence

```

_list = [0.]*m+[1.] +[np.exp(-(lambda_[m+i]-lambda_[m-1])*self.d) for i in range(m)]
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Om = alpha_prime.dot(Om).dot(xi_prime_lambda)

Om[:,m-1] += Phi[:,m-1]
Xi = xi_prime_lambda*np.exp(lambda_[m-1]*self.d)
return Om, Xi

```

See also
Song et al. JSV 2023



Adaptation of the recursive scheme

- Characteristics stabilise FEM predictions
- Significance of the information vector ?
- A-priori in the interface relations
- Not valid at normal incidence

Adaptation of the recursive scheme

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- Significance of the information vector ?
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- Not valid at normal incidence

$$\Sigma(z) = \left\{ \begin{array}{l} \mathbf{q}^+(z) \\ \mathbf{q}^-(z) \end{array} \right\}$$

$$\left\{ \begin{array}{l} \frac{\partial p_1}{\partial n} - ikp_1 \\ \frac{\partial p_1}{\partial n} + ikp_1 \end{array} \right\}$$

Adaptation of the recursive scheme

- Characteristics stabilise FEM predictions
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$$\Sigma(z) = \begin{Bmatrix} q^+(z) \\ q^-(z) \end{Bmatrix}$$

$$\begin{Bmatrix} \frac{\partial p_1}{\partial n} - ikp_1 \\ \frac{\partial p_1}{\partial n} + ikp_1 \end{Bmatrix}$$

$$\Sigma_i^+ = \begin{Bmatrix} q_i^+ \\ q_i^- \end{Bmatrix} = \begin{bmatrix} [I_{n_i}] \\ [R_{n_i}] \end{bmatrix} q_i^+$$

- Method can be extended straightforwardly
- Just a change of variables

$$S'(z) = [\alpha]S(z) \quad S_i^- = [T]S_{i-1}^+$$

$$\Sigma'(z) = [\alpha_c]\Sigma(z) \quad \Sigma_i^- = [T_c]\Sigma_{i-1}^+$$

$$[T_c] = [P]^{-1}[T][P] \quad [\alpha_c] = [P]^{-1}[\alpha][P]$$

- Information vector = characteristics
- No a-priori in the interface relations
- Valid at normal incidence

Adaptation of the recursive scheme

- Characteristics stabilise FEM predictions
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- Method can be extended straightforwardly
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$$\Sigma'(z) = [\alpha_c] \Sigma(z)$$

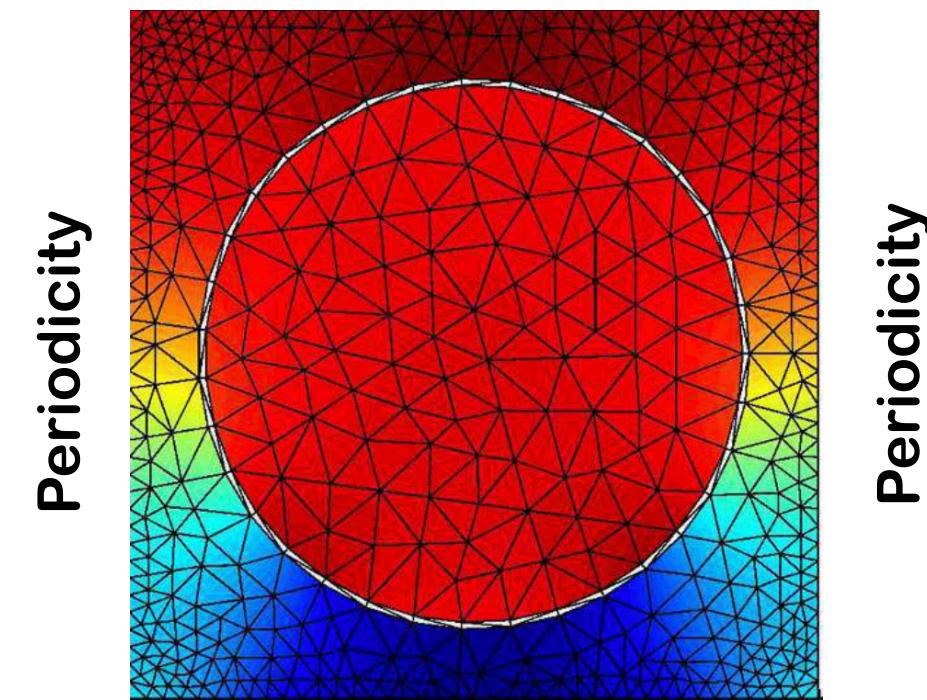
$$\Sigma_i^- = [T_c] \Sigma_{i-1}^+$$

$$[T_c] = [P]^{-1} [T] [P] \quad [\alpha_c] = [P]^{-1} [\alpha] [P]$$

- Reformulation of the TMM
- No interest if only homogeneous layers
- Transfer/State matrices diagonal at normal incidence
- Wave splitting (inhomogeneous materials)
- Childhood memories

- Information vector = characteristics
- No a-priori in the interface relations
- Valid at normal incidence

Case of the periodic structure



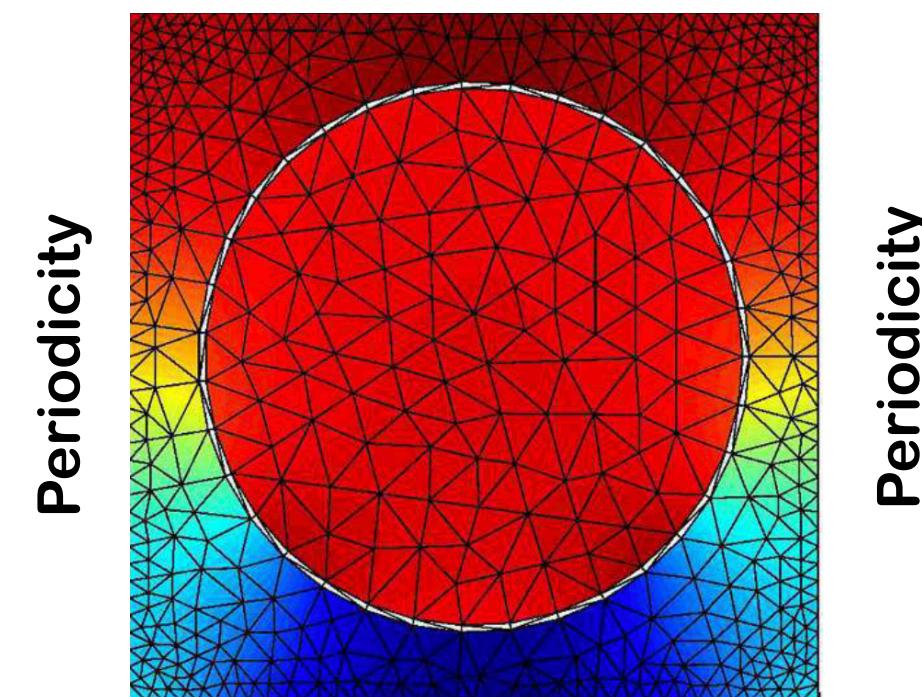
Bloch decomposition on top and bottom interfaces

$$f(x) = \sum_{l \in \mathbb{Z}} f_l e^{-i[k_x + 2\pi l/D]x}$$

Extended state vector

$$\Sigma = \left\{ \begin{array}{c} \vdots \\ q_{-1}^+ \\ q_{-1}^- \\ q_0^+ \\ q_0^- \\ q_1^+ \\ q_1^- \\ \vdots \end{array} \right\}$$

Case of the periodic structure



After truncation

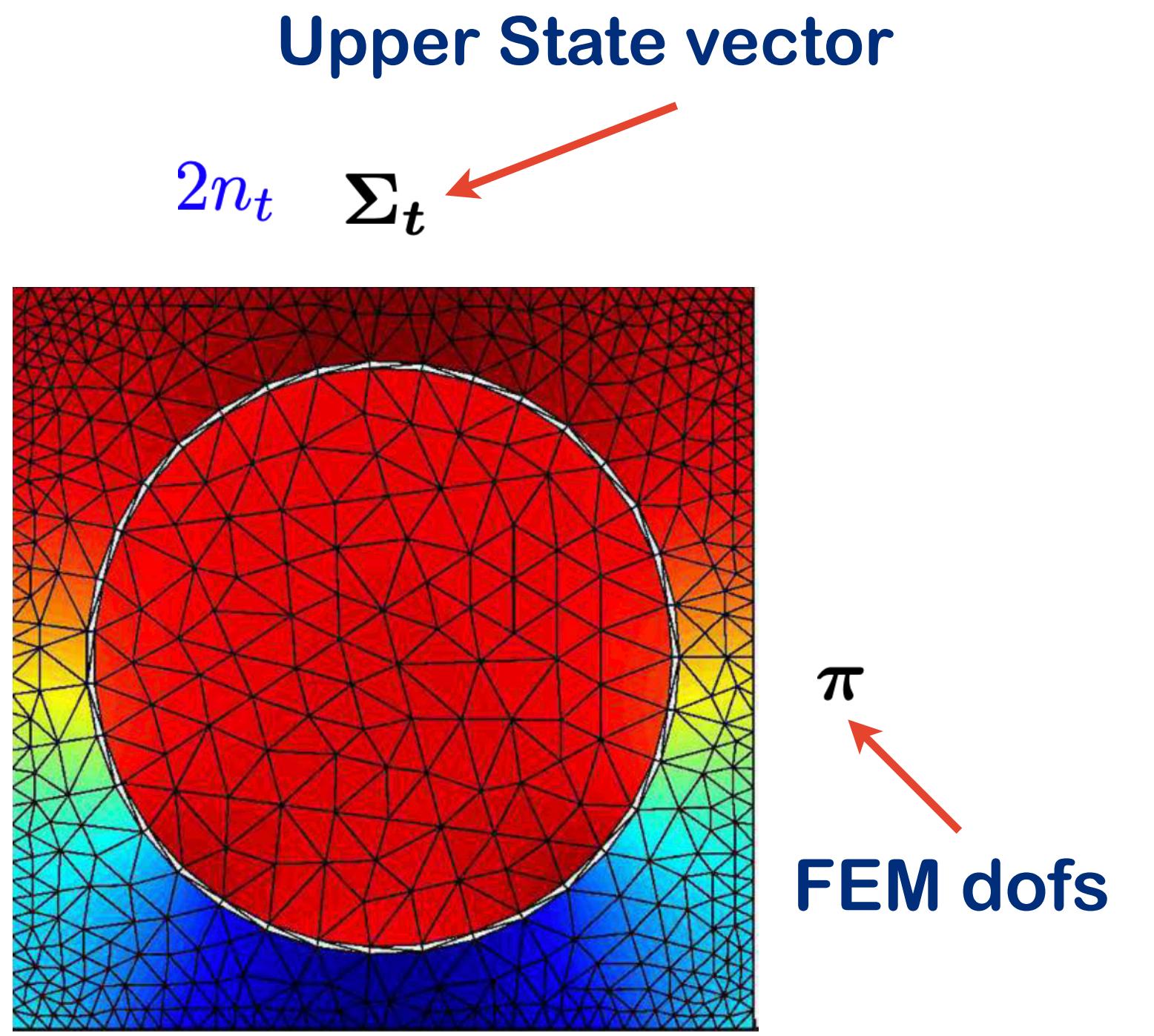
$$\begin{Bmatrix} \Sigma_{-N}^b \\ \vdots \\ \Sigma_0^b \\ \vdots \\ \Sigma_N^b \end{Bmatrix} = \begin{bmatrix} [T_{-N,-N}] & \dots & [T_{-N,0}] & \dots & [T_{-N,N}] \\ [T_{0,-N}] & \dots & [T_{0,0}] & \dots & [T_{0,N}] \\ [T_{N,-N}] & \dots & [T_{N,0}] & \dots & [T_{N,N}] \end{bmatrix} \begin{Bmatrix} \Sigma_{-N}^t \\ \vdots \\ \Sigma_0^t \\ \vdots \\ \Sigma_N^t \end{Bmatrix}$$

- Homogeneous material : diagonal by block
- Non diagonal blocks : interaction of Bloch waves

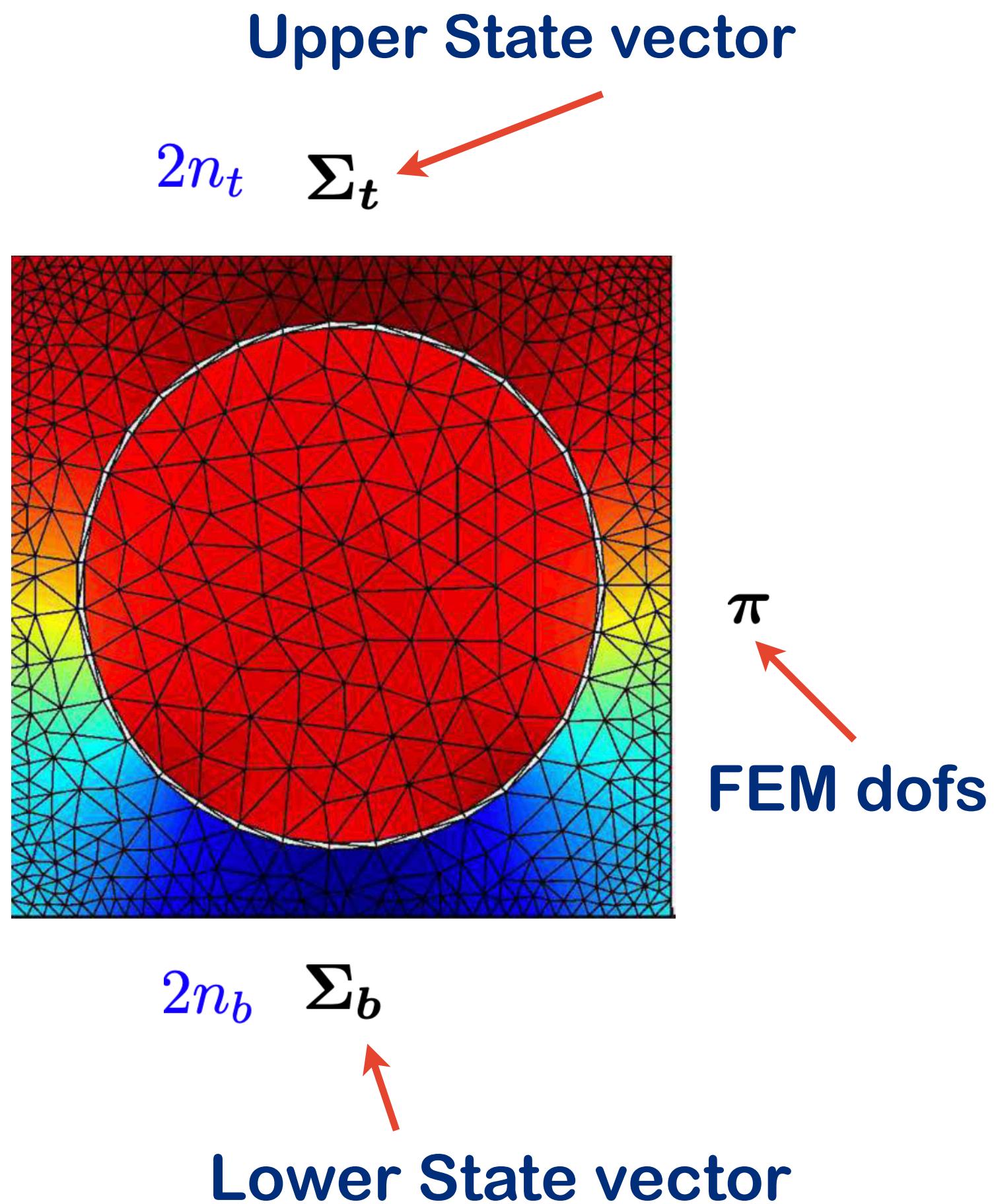
Extended state vector

$$\Sigma = \begin{Bmatrix} \vdots \\ q_{-1}^+ \\ q_{-1}^- \\ q_0^+ \\ q_0^- \\ q_1^+ \\ q_1^- \\ \vdots \end{Bmatrix}$$

Computation of the TM



Computation of the TM



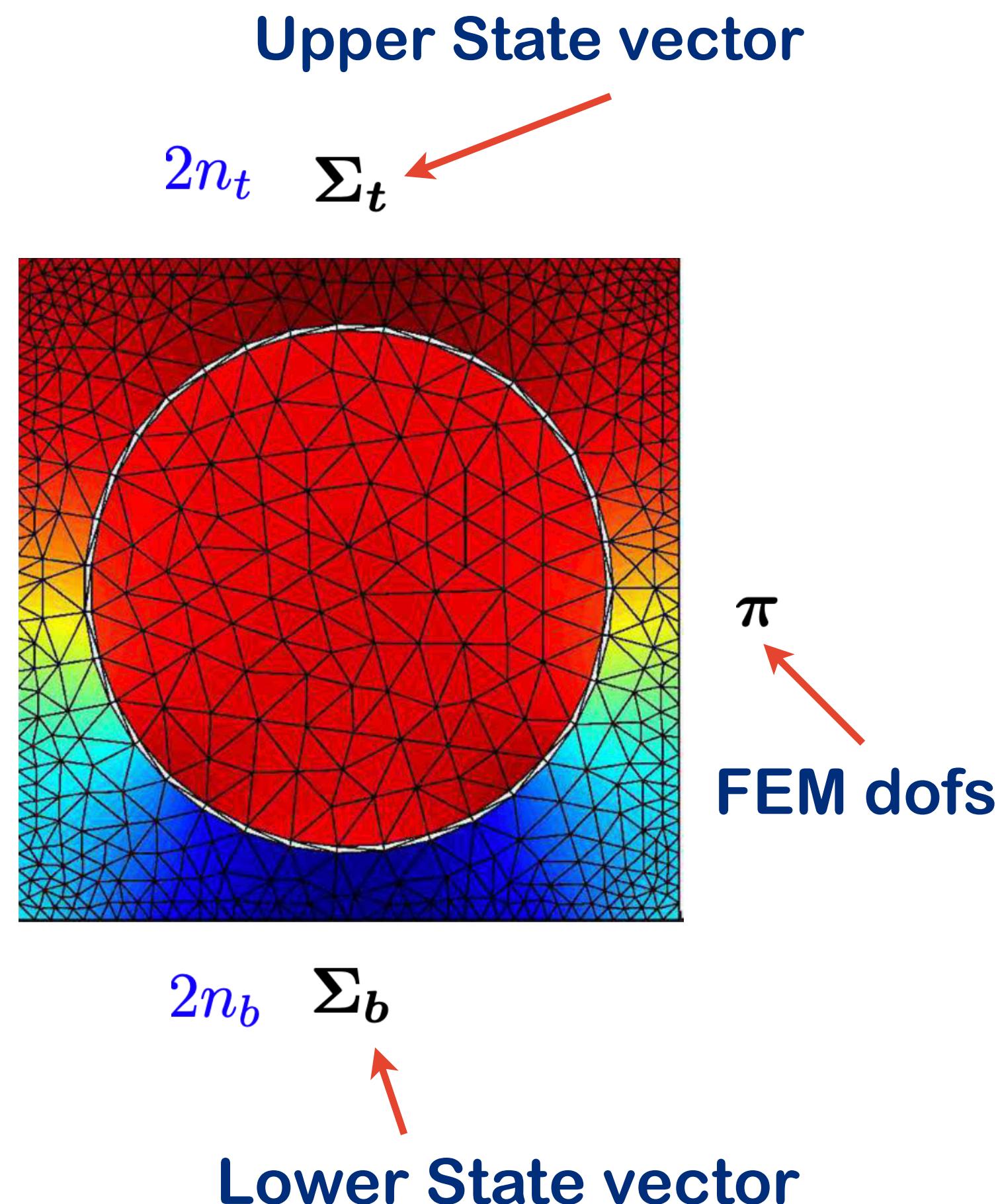
Orthogonality relations →

Stabilized weak forms →

Orthogonality relations →

$$\begin{bmatrix} [D_{tt}] & [D_{ti}] & [0] \\ [D_{it}] & [D_{ii}] & [D_{ib}] \\ [0] & [D_{bi}] & [D_{bb}] \end{bmatrix} \begin{Bmatrix} \Sigma^t \\ \pi \\ \Sigma^b \end{Bmatrix} = 0.$$

Computation of the TM



Orthogonality relations →

Stabilized weak forms →

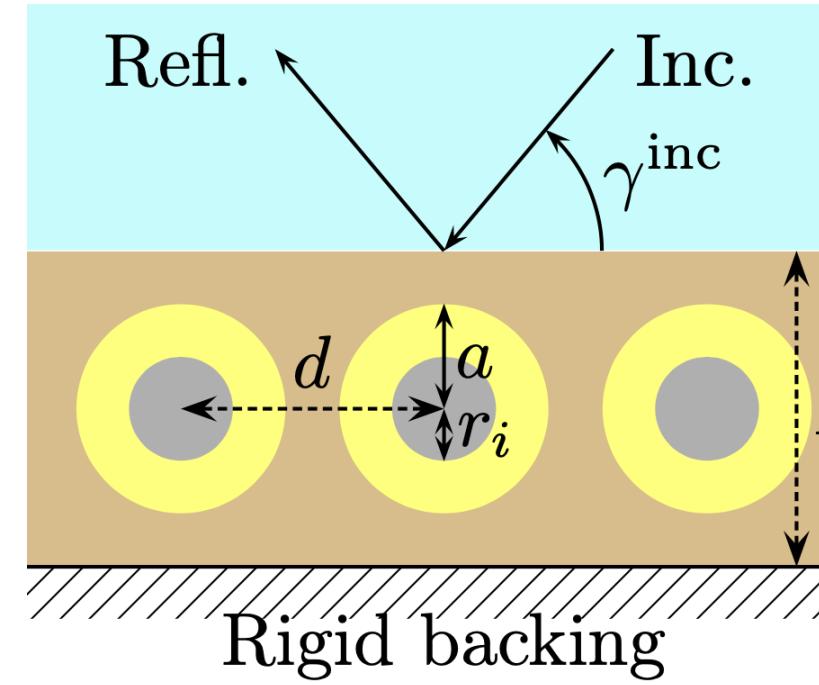
Orthogonality relations →

$$\begin{bmatrix} [D_{tt}] & [D_{ti}] & [0] \\ [D_{it}] & [D_{ii}] & [D_{ib}] \\ [0] & [D_{bi}] & [D_{bb}] \end{bmatrix} \begin{Bmatrix} \Sigma^t \\ \pi \\ \Sigma^b \end{Bmatrix} = 0.$$

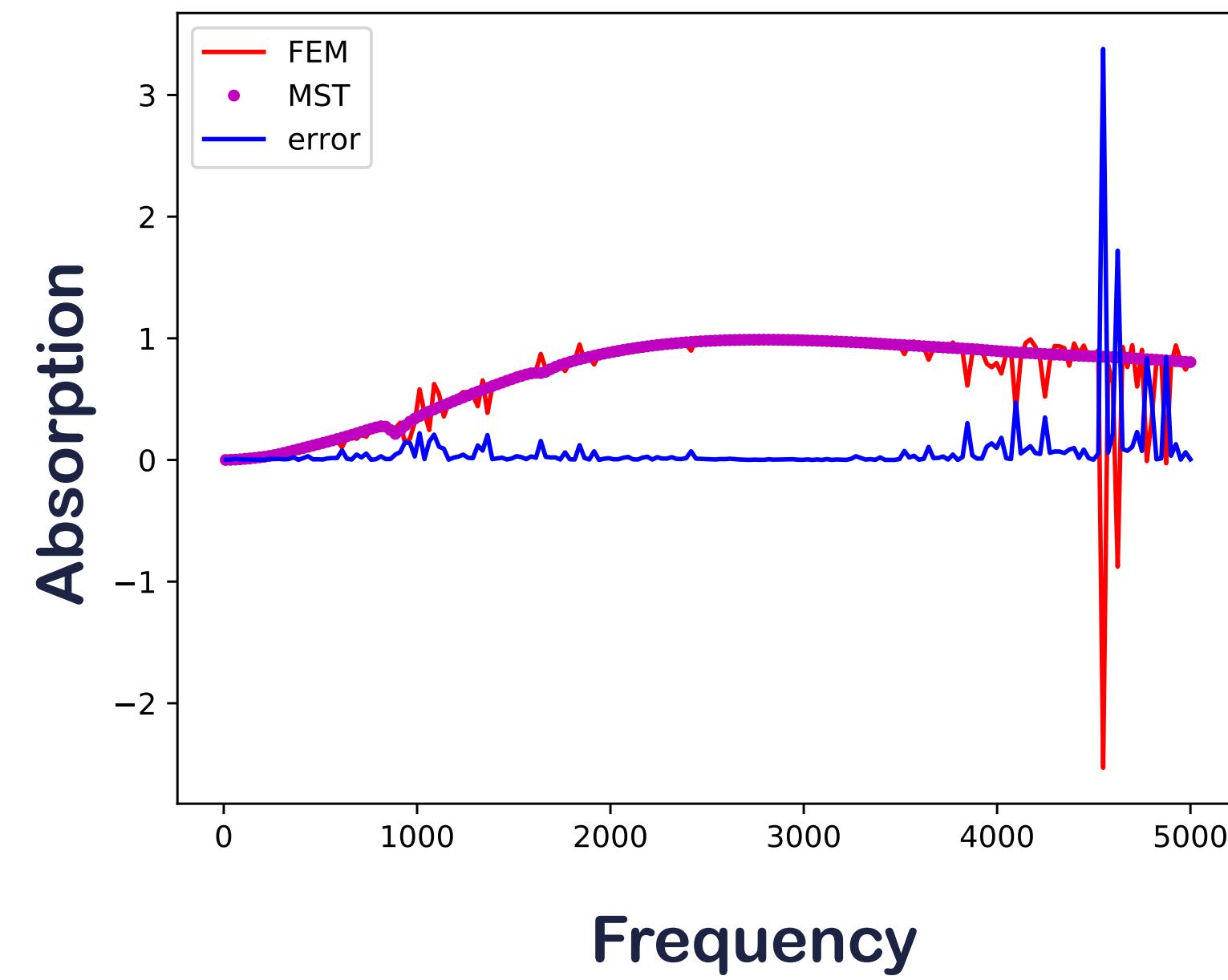
$$\Sigma^b = - \begin{bmatrix} [D_{ti}][R_b] \\ [D_{bb}] + [D_{bi}][R_b] \end{bmatrix}^{-1} \begin{bmatrix} [D_{tt}] + [D_{ti}][R_t] \\ [D_{bi}][R_t] \end{bmatrix} \Sigma^t$$

Application of the recursive approach
On the two matrices to stabilise

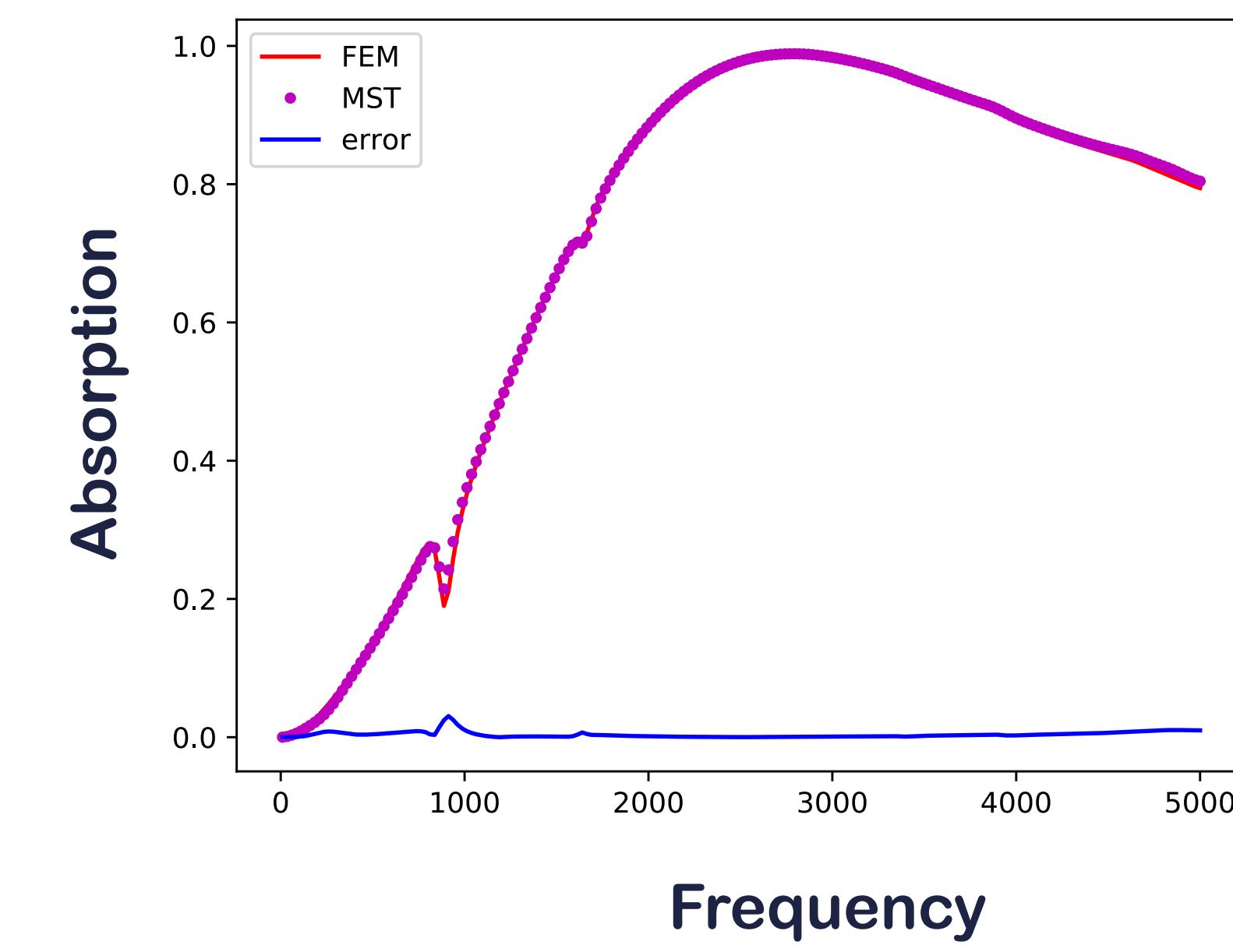
First: stability issues



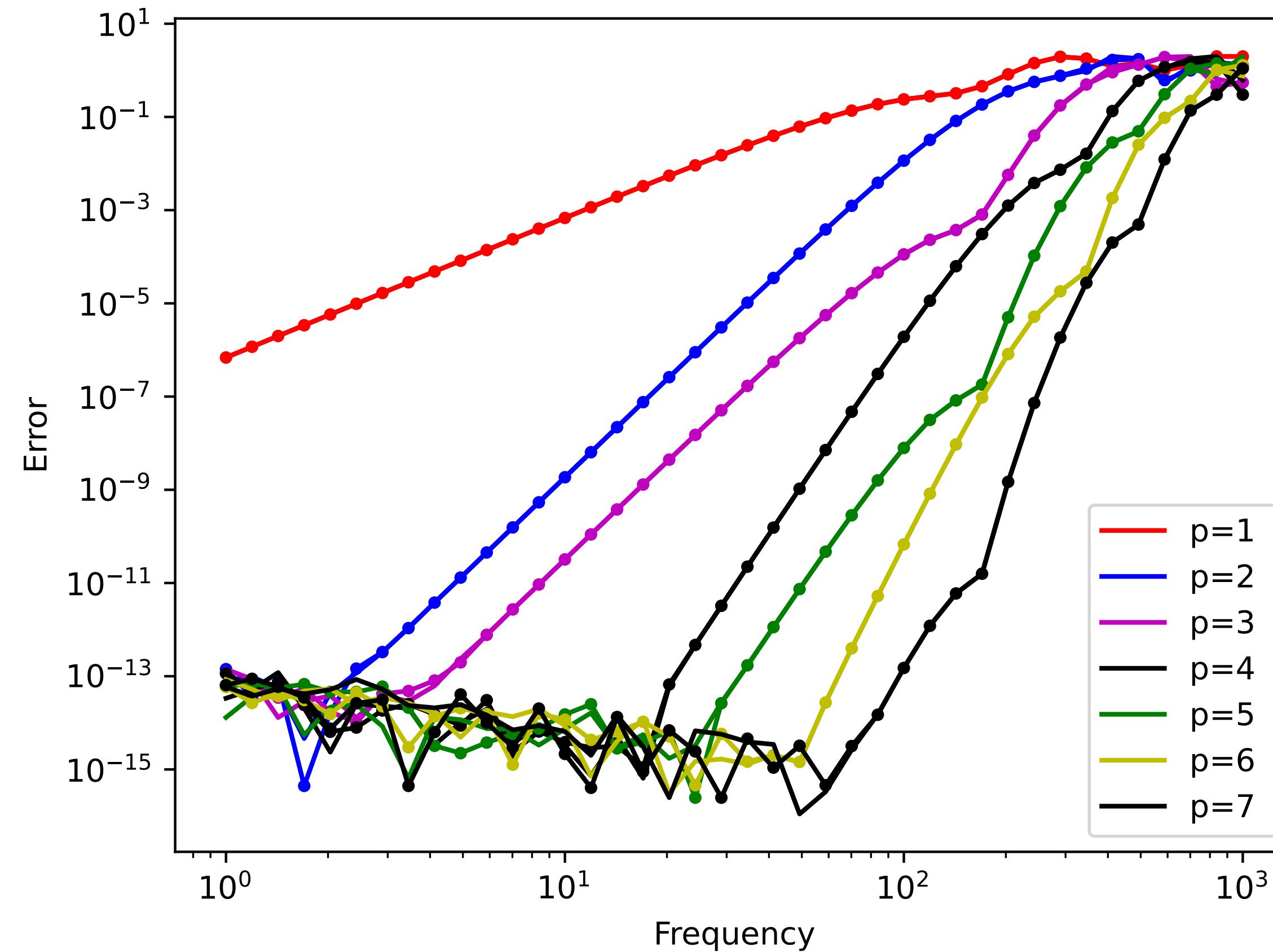
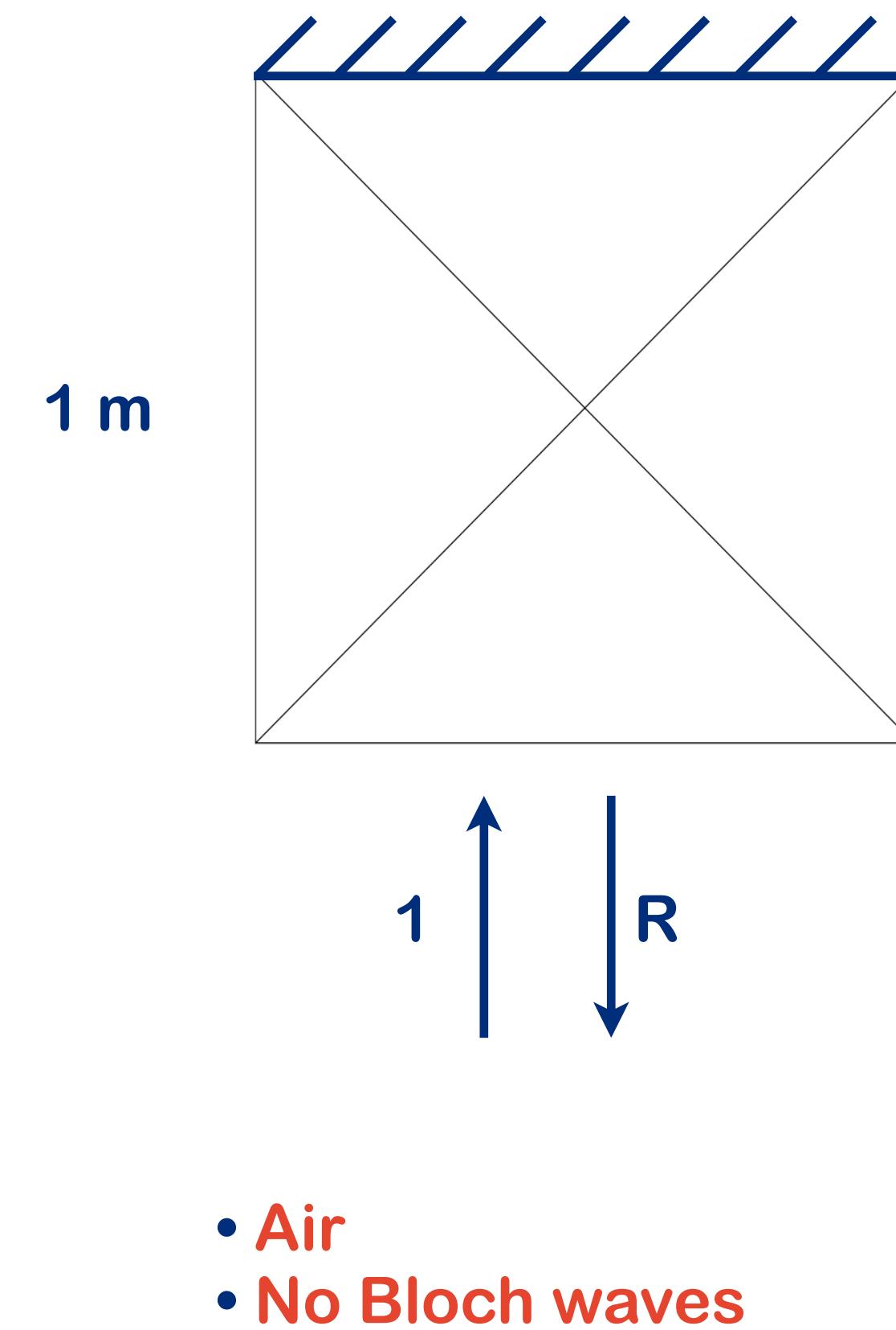
Before



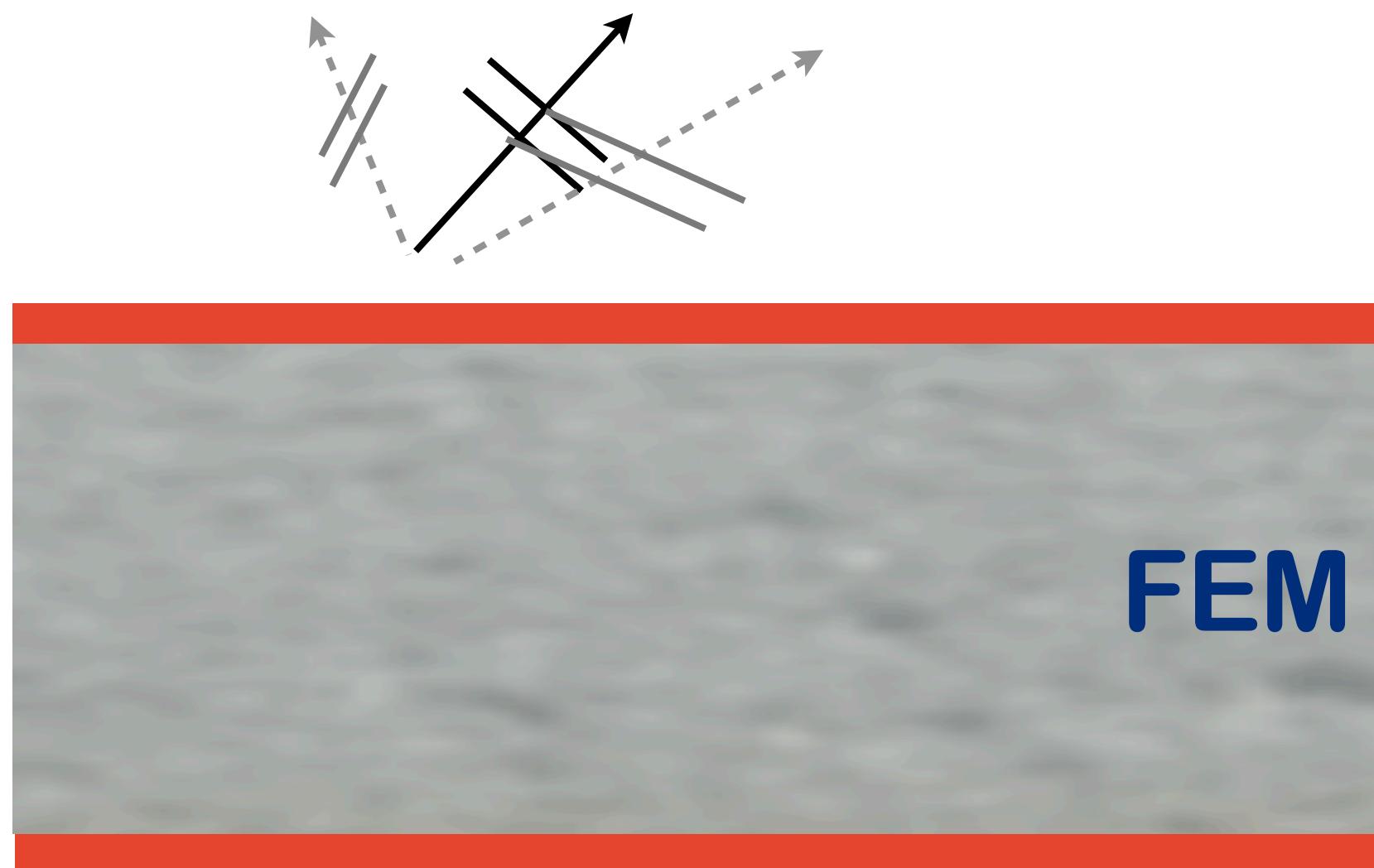
After



Performance of the method

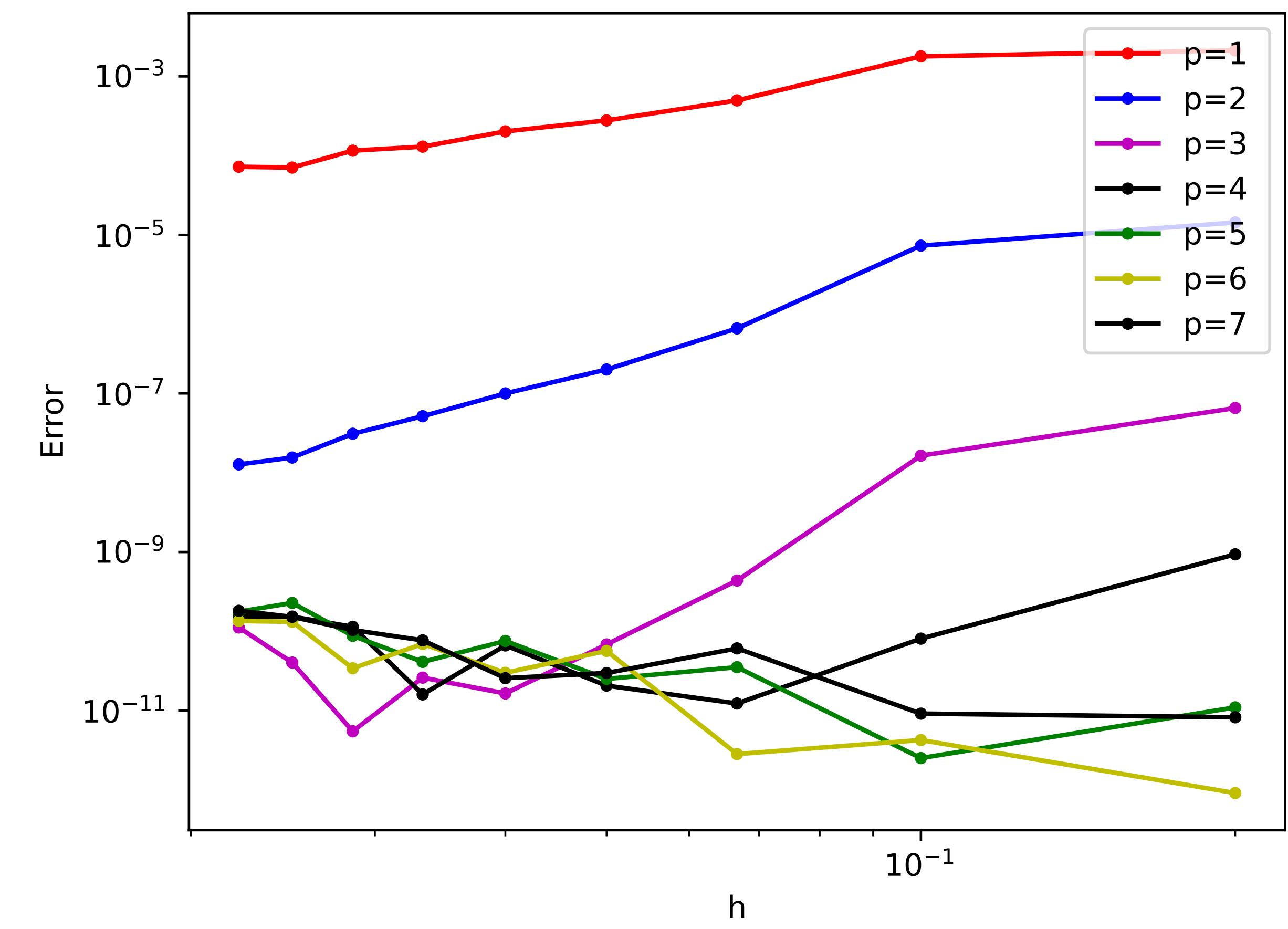


Multilayer case (sandwich panel)

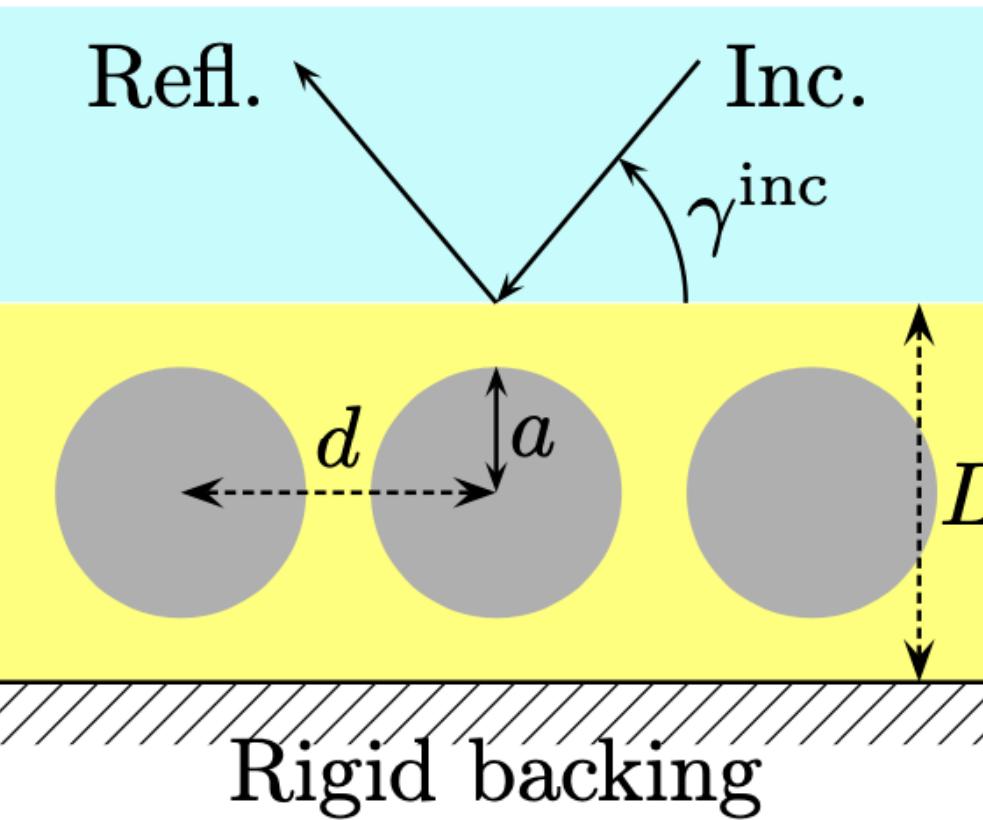


- Rubber 0.2 mm
- Melamine 2 cm
- Rubber 0.2 mm
- 45 ° incidence
- Period 20 cm

Influence of a mesh refinement

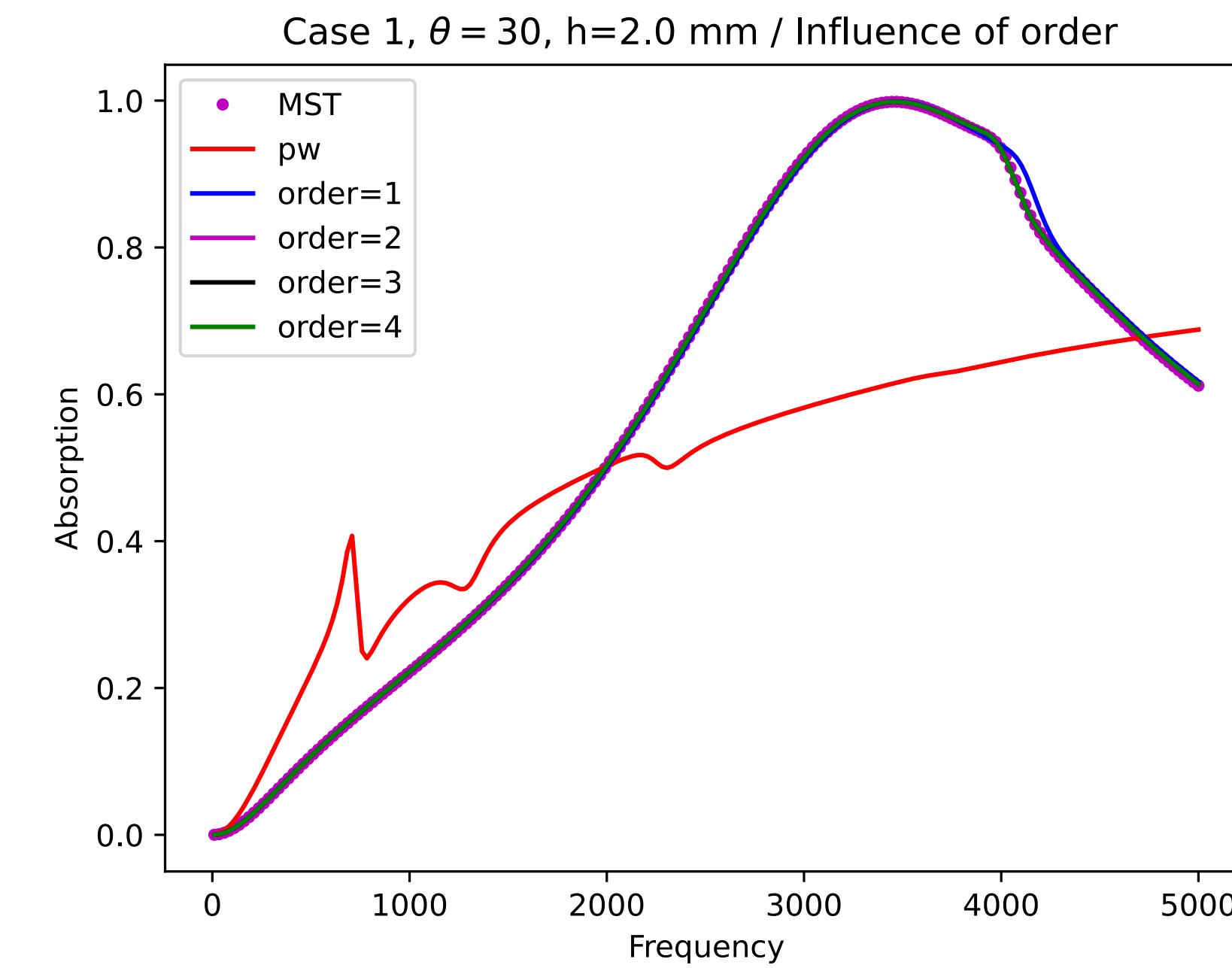
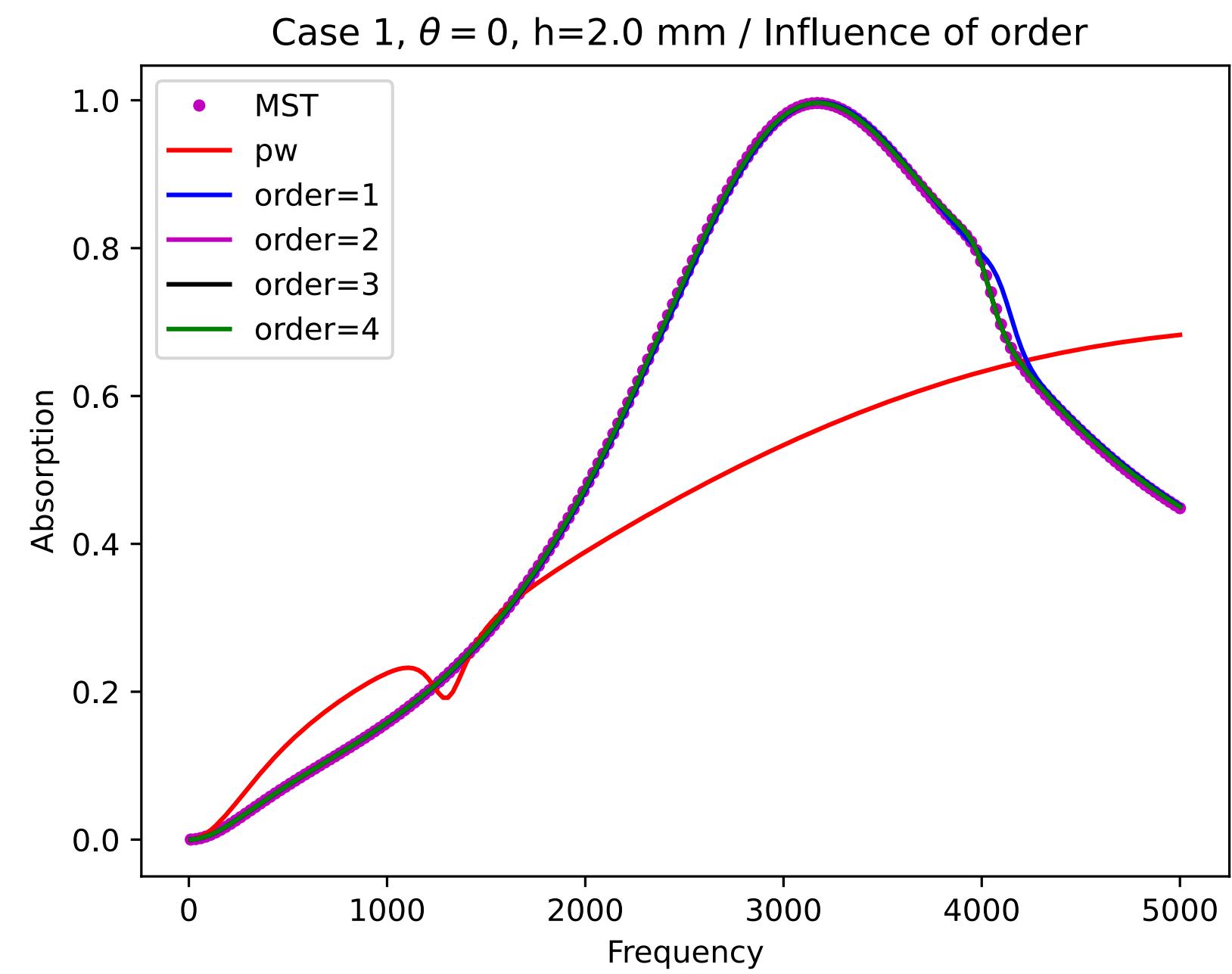


Comparaison MST



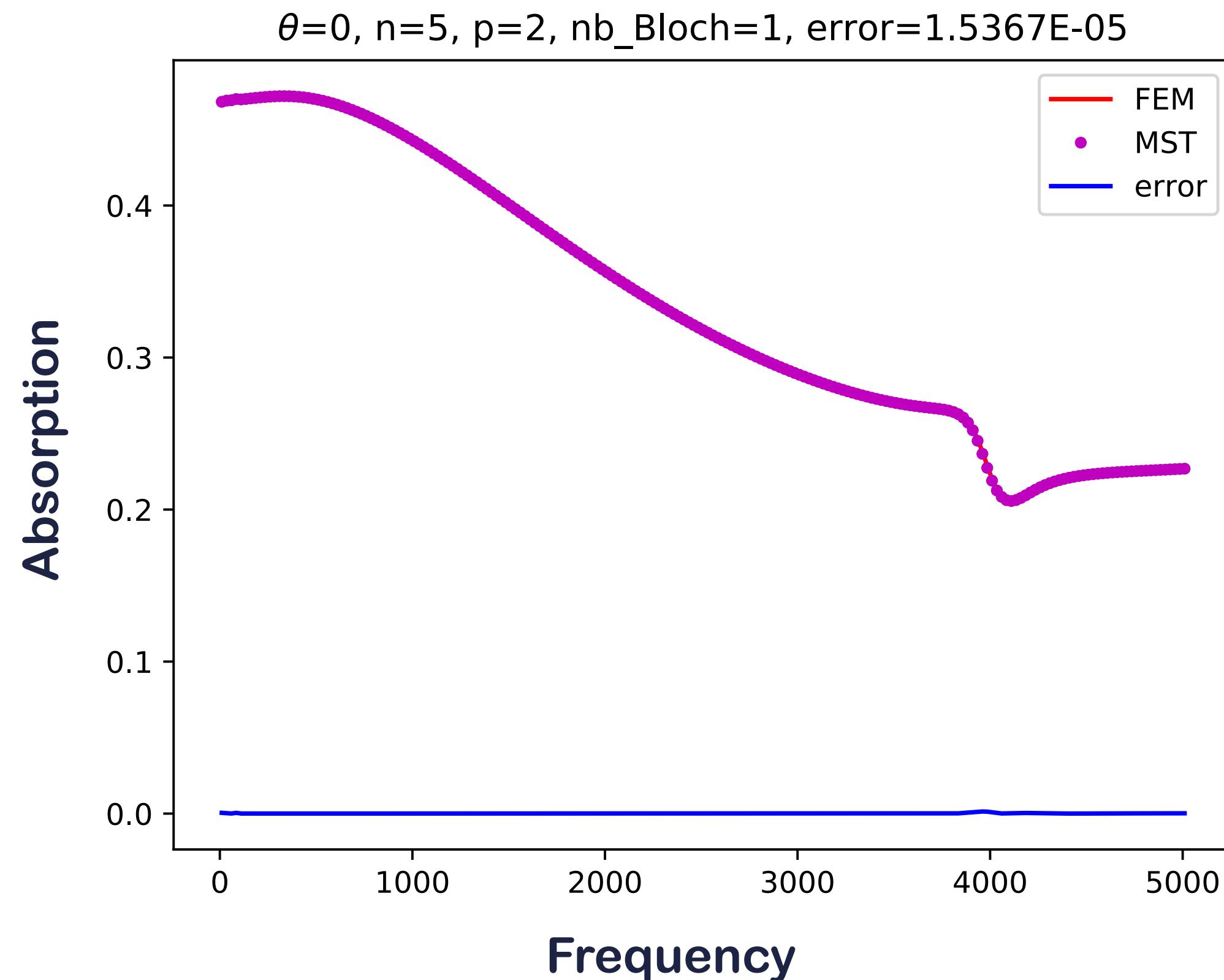
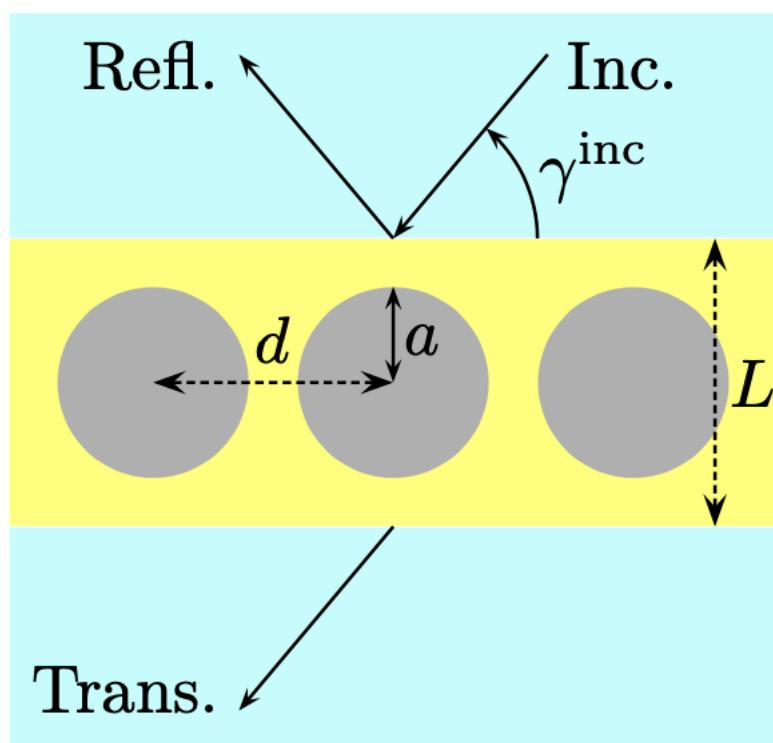
- Poroelastic core (2cm x 2cm)
- Plastic inclusion

Weisser et al. JASA (2016)

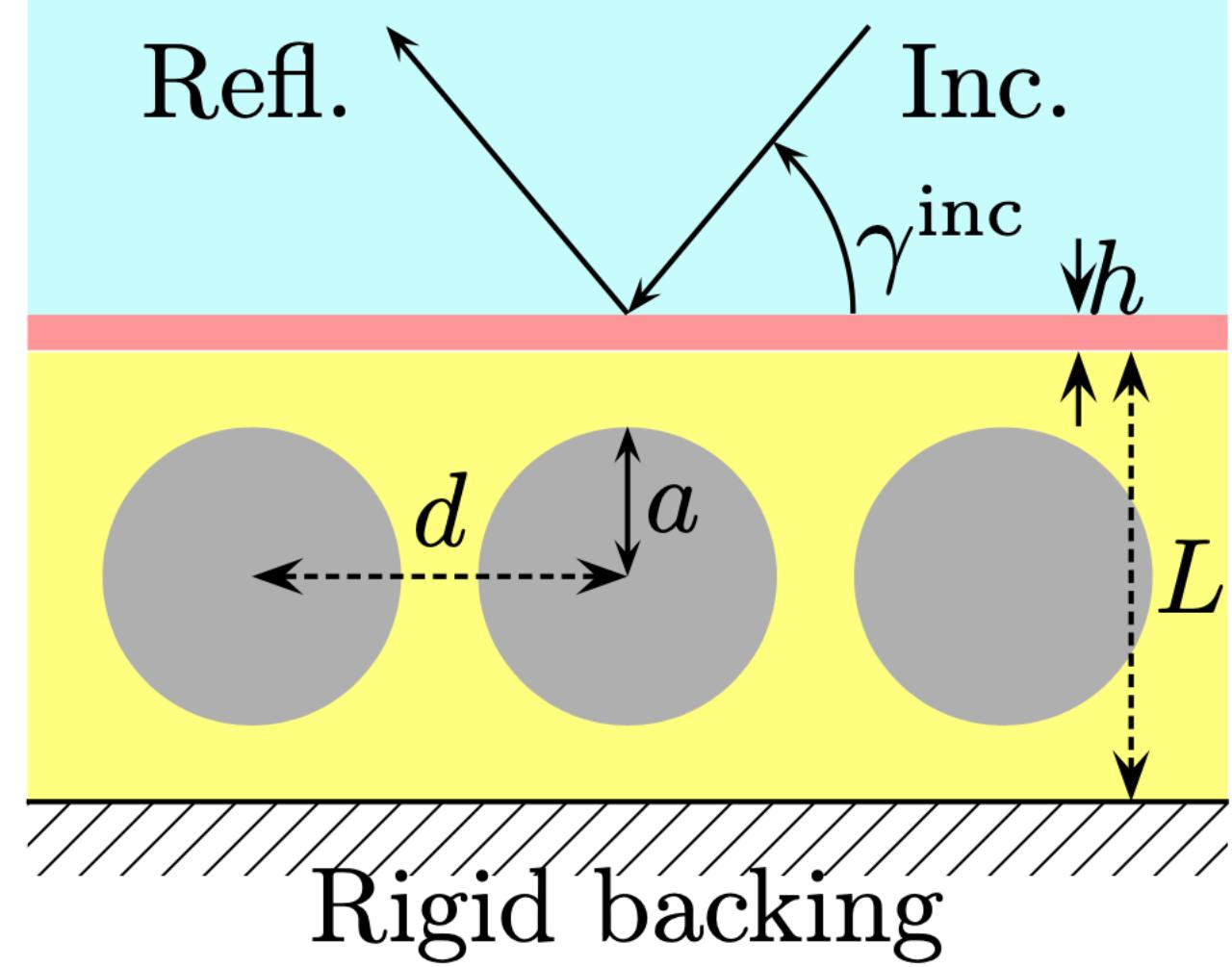


Case of transmission

- Case of transmission
- Poroelastic core ($2\text{cm} \times 2\text{cm}$)
- Plastic inclusion
- Unpublished MST (at the moment)

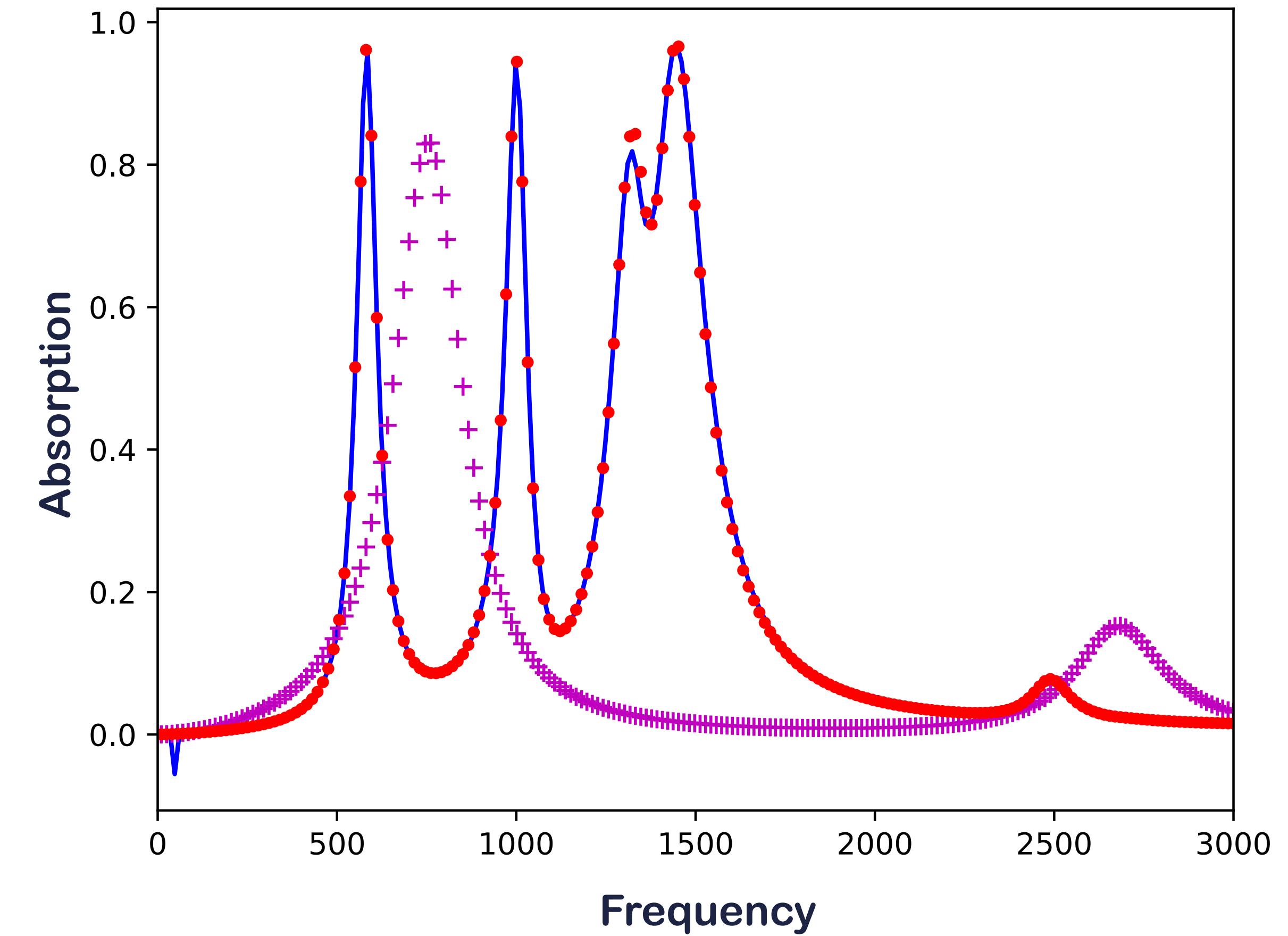


Another comparison with literature



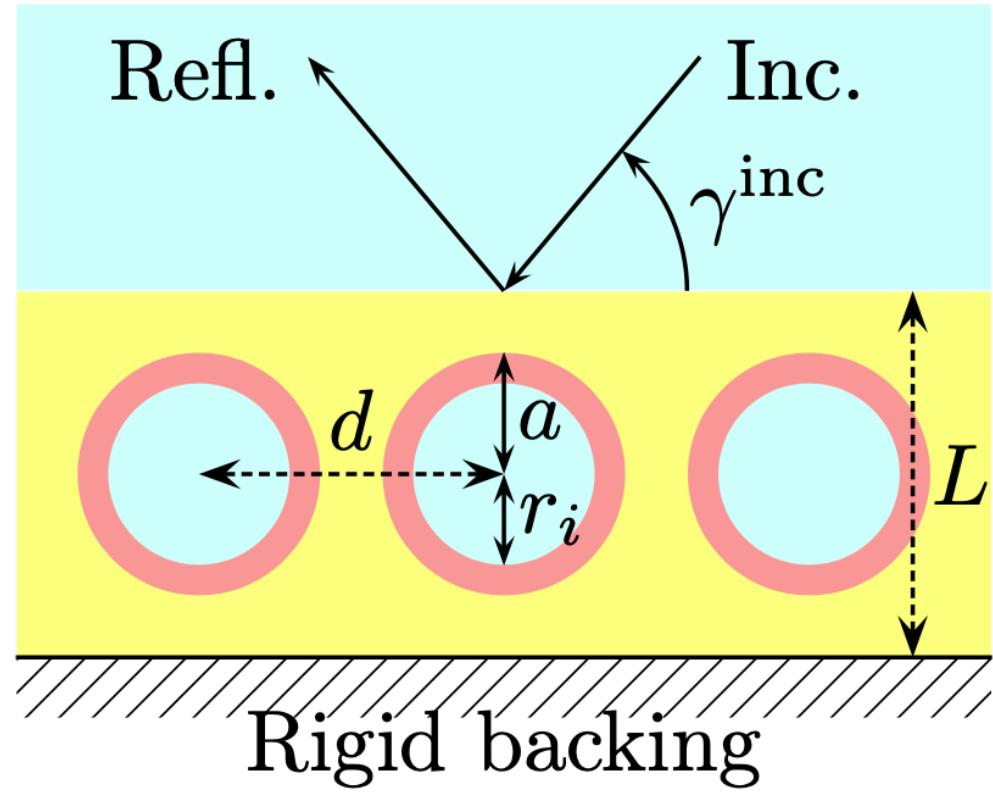
- Poroelastic core (2cm x 2cm)
- Elastic inclusion
- 0.2 mm rubber layer

Gaborit et al. AAA (2018)

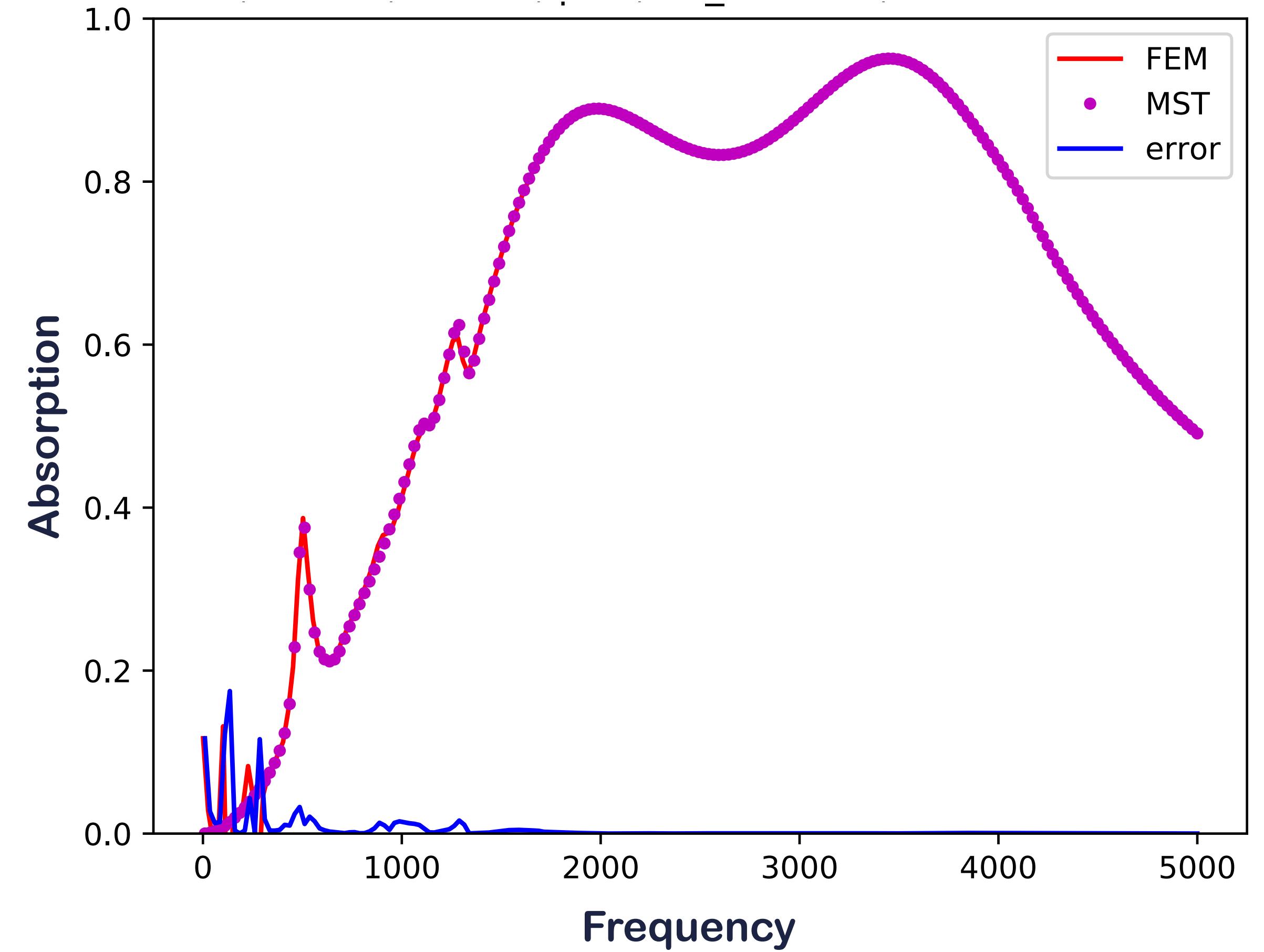


Limit of the method

Weisser et al. JASA (2016)

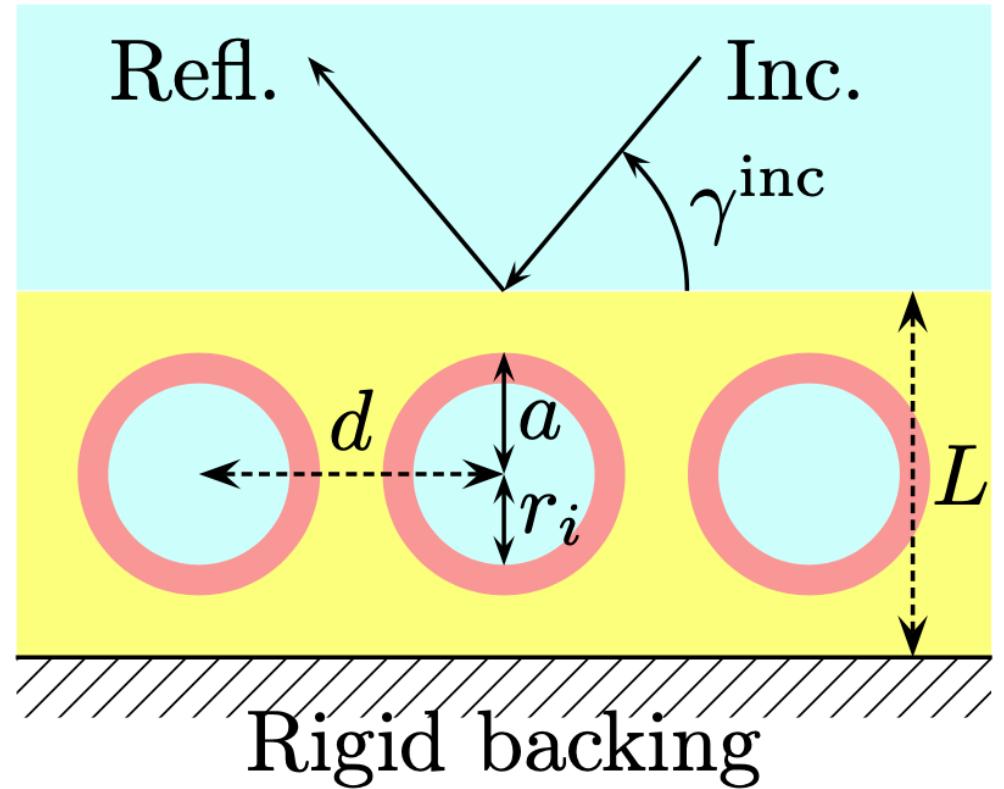


- Poroelastic core (2cm x 2cm)
- 0,2 mm rubber elastic skin
- 10 Bloch waves
- $P = 7$
- Conditioning issues at LF



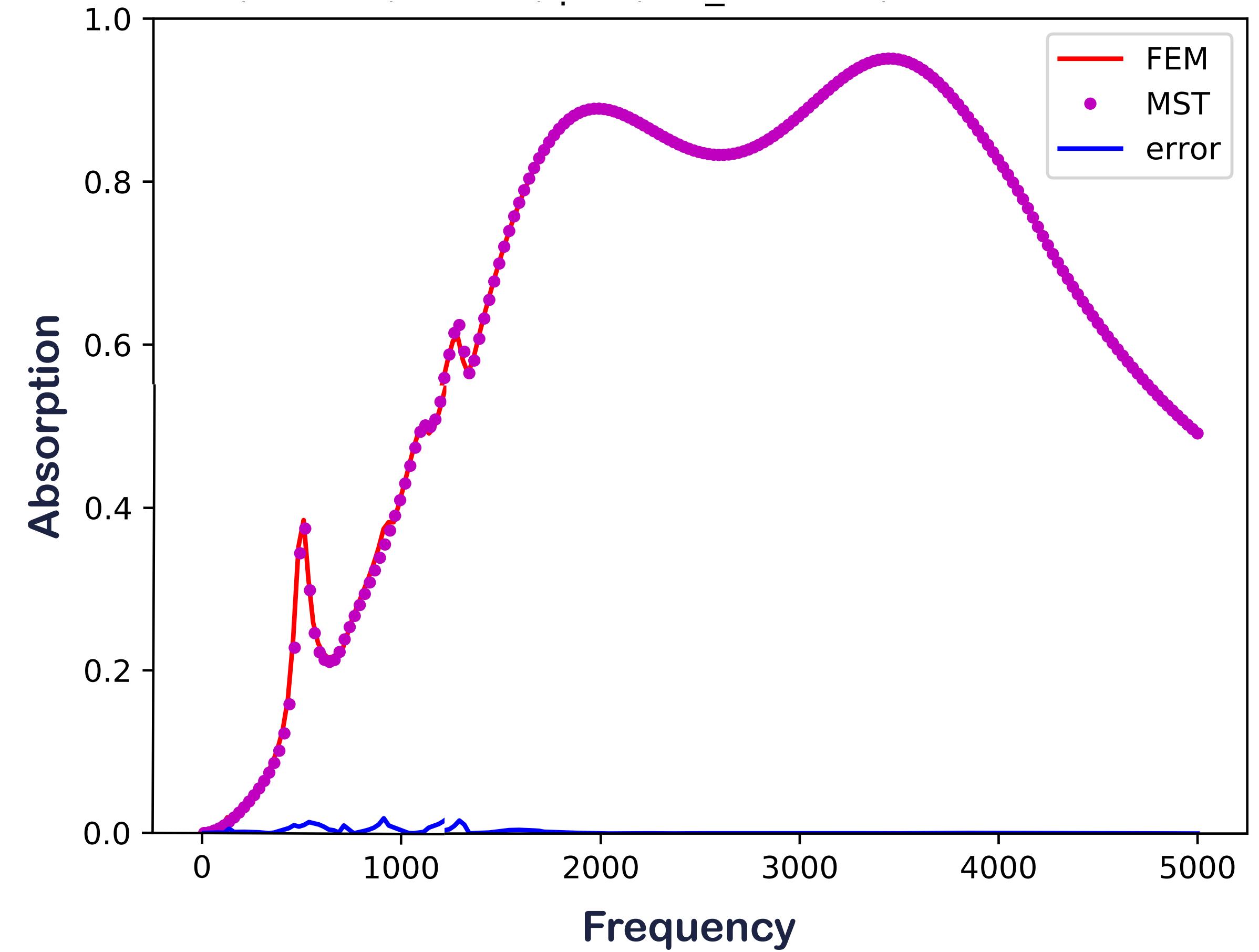
Limit of the method

Weisser et al. JASA (2016)



- Poroelastic core (2cm x 2cm)
- 0,2 mm rubber elastic skin
- 10 Bloch waves
- $P = 7$
- Conditioning issues at LF

Can be fixed by reducing the number
of Bloch waves ($p=2$)



Conclusion

- Contributions
 - Reformulation of the recursive method in terms of characteristics
 - Information vector = characteristics
 - No a-priori in the interface relations
 - Valid at normal incidence
 - Stable approach for the periodic cell
 - Valid for higher order elements
 - Both on boundary operators and propagation in layers
 - Validated on various cases
- Limits / perspectives
 - Conditioning issues when the model is too discretised
 - Empirical fixes can be used
 - Theoretical alternatives can be found
 - Dispersion analysis