



中车株洲电力机车有限公司
CRRC ZHUZHOU LOCOMOTIVE CO., LTD.

Application of lightweight acoustic materials and structures in rail vehicles

Dengke Li

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01 Motivations & Background



Dengke Li

- Technical expert and senior engineer at CRRC ZHUZHOU LOCOMOTIVE Co., Ltd. (CRRC), member of the Environmental Physics Branch of the China Environmental Science Society, and member the Vibration and Noise Control Technical Committee at CRRC

Research areas:

- Rail vehicles vibration and noise control
- Novel noise reduction materials and structures



In 2018 receive a PhD degree from Chinese Academy of Sciences



Working with Camille Perrot under support of National CSC Program



In 2018 working as an acoustic engineer in CRRC



01 Motivations & Background



Noise inside cabin



Cabin of rail vehicles



Ultra High Voltage Transformer



Automobile



Underwater vehicles



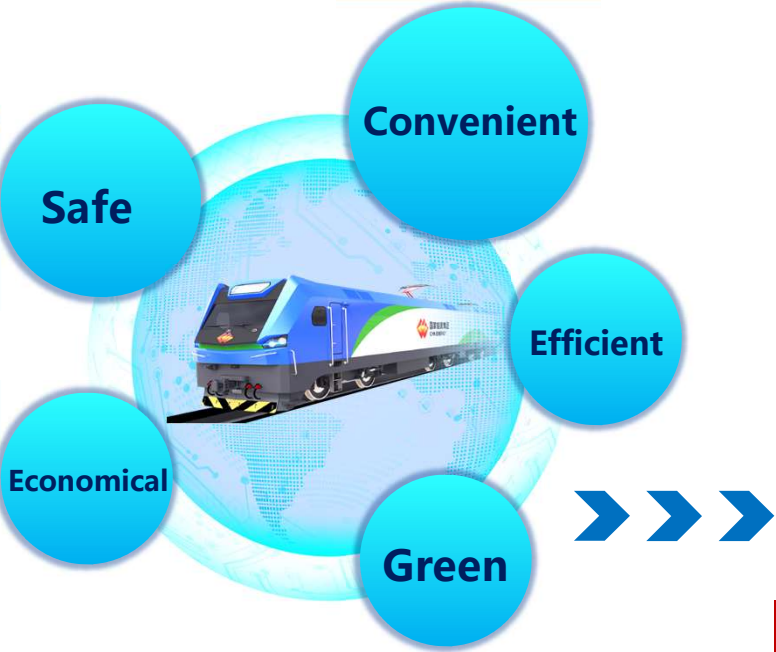
Turboprop



01 Motivations & Background

➤ Development trend of national transportation

- ❑ Building a safe, convenient, efficient, green, and economical modern integrated transportation system
- ❑ Vibration and noise in vehicles becomes increasingly prominent under high moving speeds and complex geographical and climatic conditions



High-speed & heavy loading

中华人民共和国噪声污染防治法(草案)

目 录

第一章 总 则

第二章 噪声污染防治标准与规划

第三章 噪声污染防治的监督管理

第四章 工业噪声污染防治

第五章 建筑施工噪声污染防治

第六章 交通运输噪声污染防治

第七章 社会生活噪声污染防治

第八章 法律责任

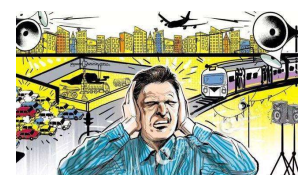
第九章 附 则

Key problem of further development of high speed transportation



High Speed

Quiet Journey



Ensuring acoustic comfort!!!



01 Motivations & Background

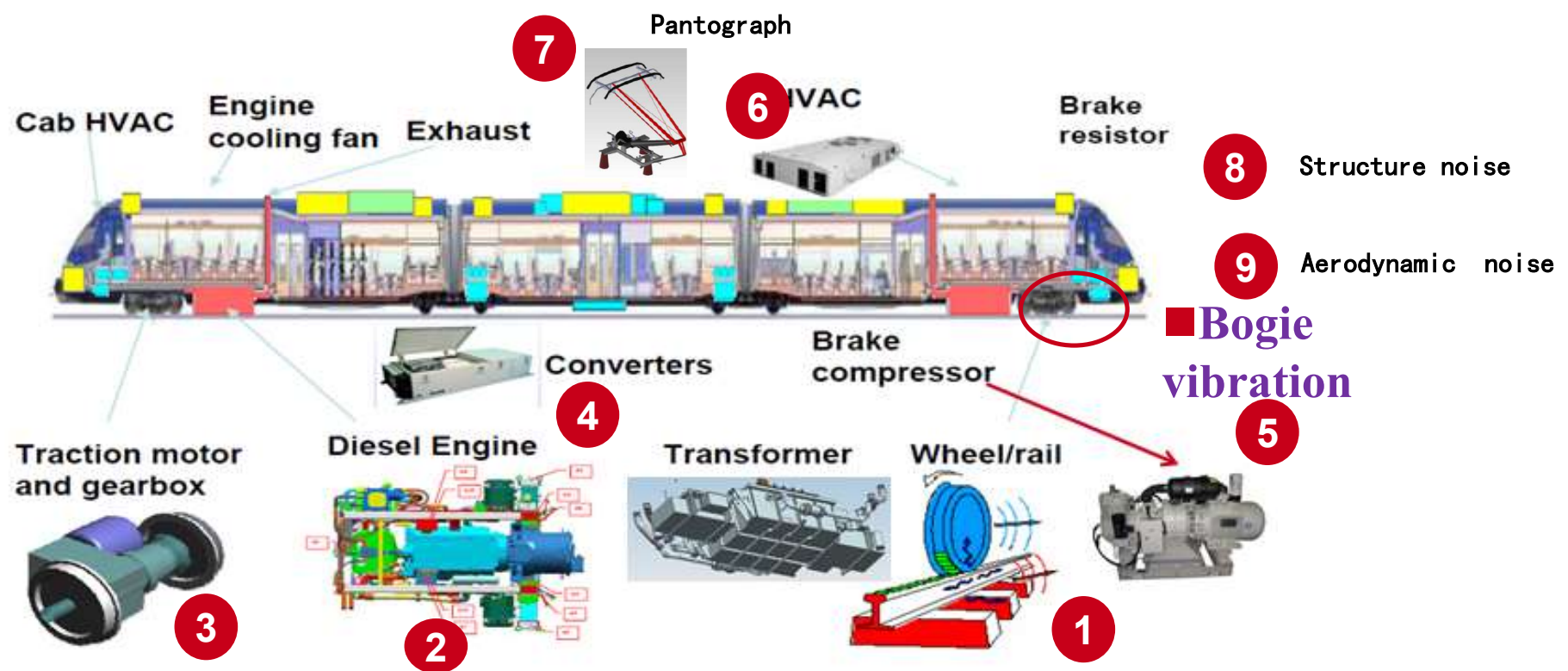
1 Where noise come from ?

2 What should do?



01 Motivations & Background

1.1 Main noise sources



Sources : **Noise** + **Vibration**



01 Motivations & Background

1.2 Main vibration paths

Excitation sources - structure (path) - response

•Sources

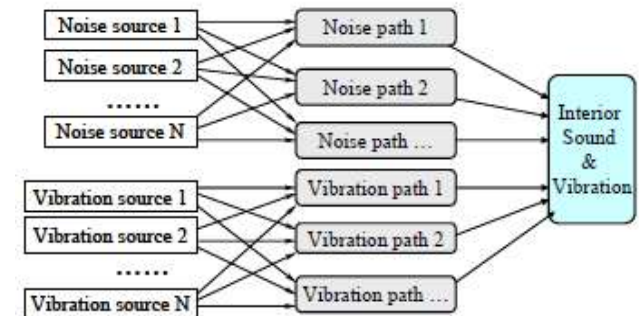
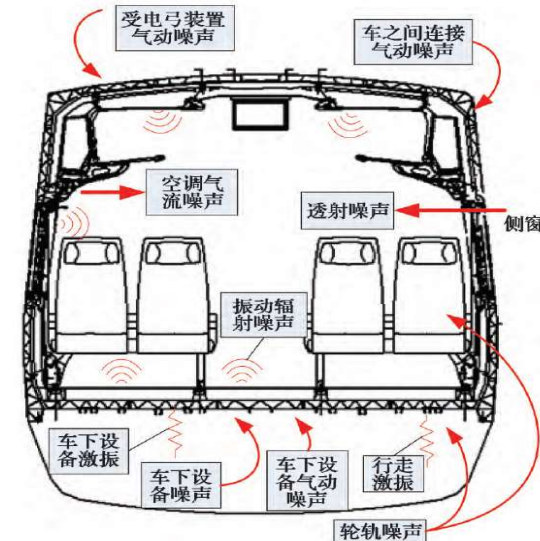
- Suspension vibration transmission
- Primary suspension excitation (wheelset to bogie)
- Secondary suspension (Bogie to car body)
- Wheel/rail interaction system
- Suspended equipment (with excitation source)
- Air dynamic load

•Transmission Paths(Structure-borne and airborne)

- Suspension
- connection points between structures
- Car Body structure
- Interior

•Response

- Each part of car body
- Test points for ride quality index (steering wheel)
- Driver' s and passenger's (seats)





01 Motivations & Background

■ Sources properties



Sound power
of all noise sources



System design



■ Body design



Transmission loss
and absorption



Air-borne sound



■ Interior design



Transmission and
reverberation



Air-borne sound



■ Vibration design



Vibration
isolation



Structure-borne sound

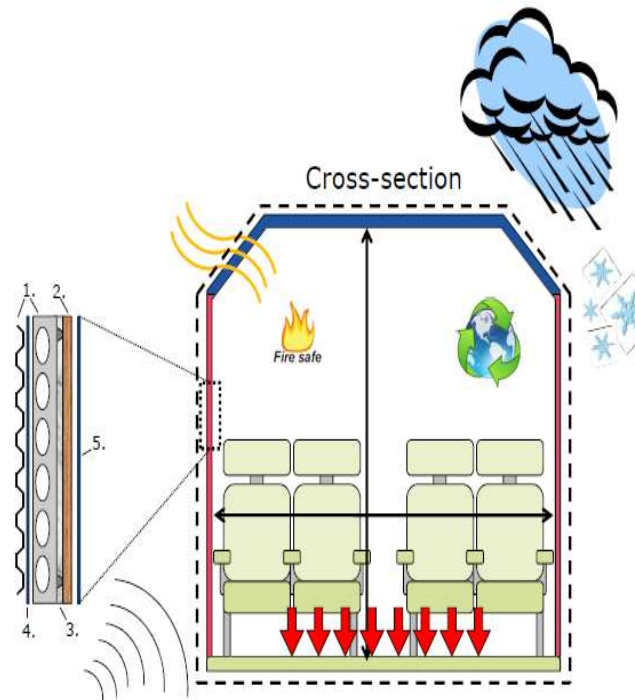


01 Motivations & Background

■ Key requirement of acoustic materials

Considering multiple comprehensive performance factors

- ✓ Load-bearing capacity
- ✓ Vibration damping
- ✓ Noise reduction
- ✓ Fire resistance
- ✓ Thermal insulation
- ✓ Weather resistance



Fireproof
heat-resistant

sound insulation,
vibration reduction

moisture resistance
damp-proofing

filtration
dust absorption

exterior
decoration

Finding balanced solutions for various technical performance requirements!



01 Motivations & Background

■ Damping

■ Transmission loss

■ Absorption

■ Isolation

■ Sealing



for high frequency noise and vibration

much depend on mass density

for middle and high frequency noise

for low frequency vibration

for high frequency noise



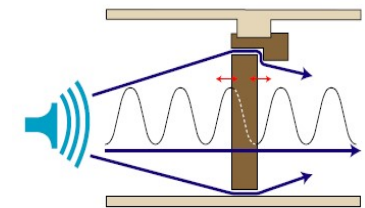
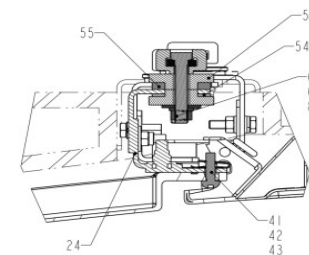
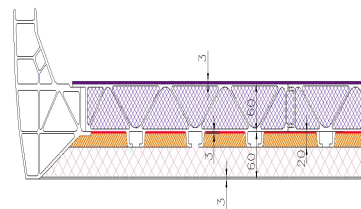
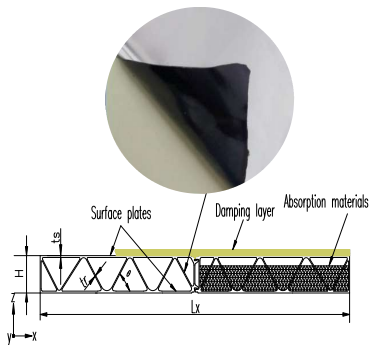
thin panel structure

whole vehicle body areas

interior porous materials and structures

bogie area
Air conditioning compressor

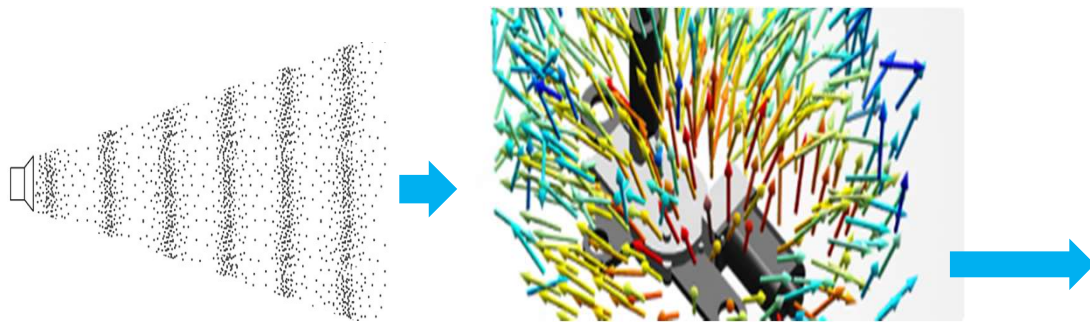
door and gangway



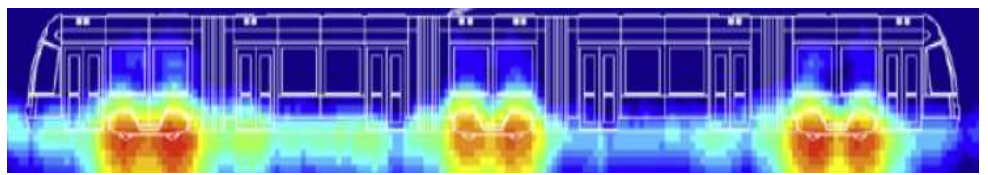


1.3 Noise identification

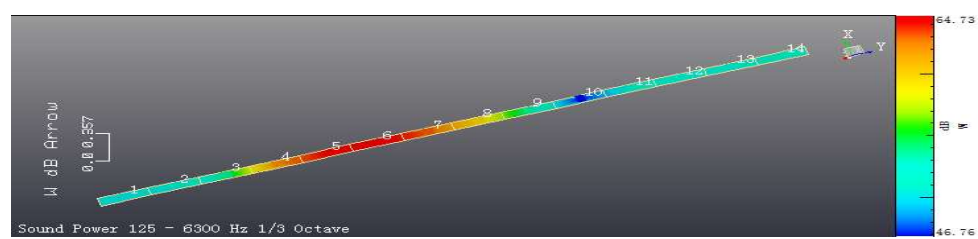
Noise source identification system by vector acoustic sensors



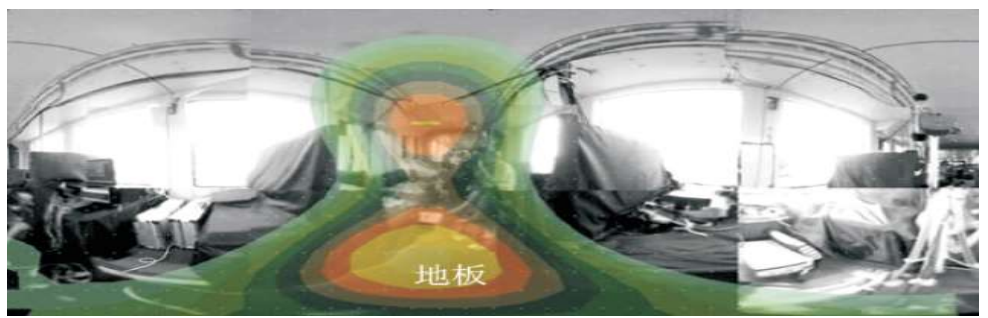
Noise source identification and transmission characteristics test



Exterior noise source identification



Airconditioning duct noise distribution



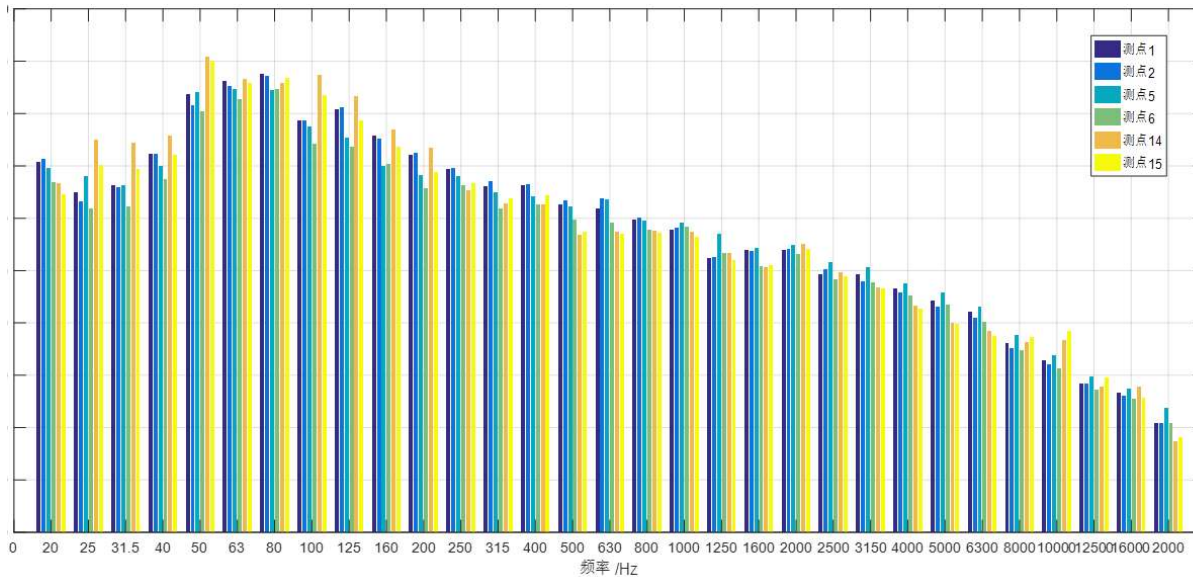
Interior noise source identification



01 Motivations & Background

1.4

Noise spectrum



- 50-2000Hz dominates

Challenges:

- Improve low frequency sound insulation and absorption

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Motivations & background



Research progress



Engineering application view

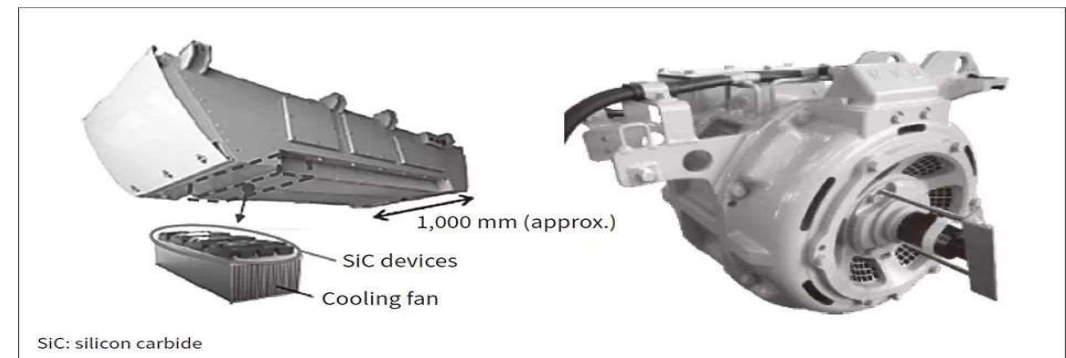


Challenges & opportunities

02 Research Progress

2.1 Japan_N700S

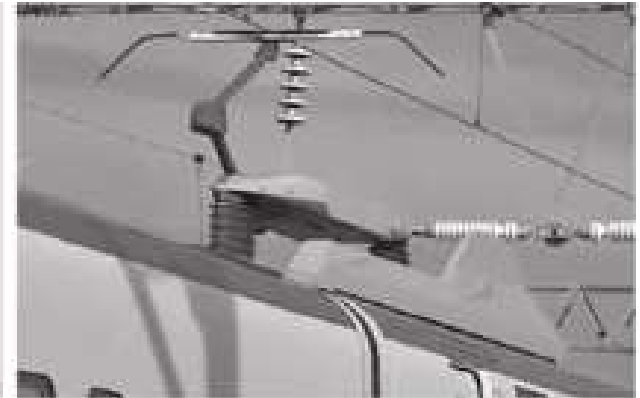
- ✓ a "super double wing" streamlined nose, which optimizes the aerodynamic performance of the high speed train
- ✓ minimizing the pressure wave into the tunnel, thus reducing the noise into the tunnel and improving the comfort of the train
- ✓ SiC device and high efficient induction motor is used to reduce the noise of transformer and motor



2.1 Japan_N700S

N700S

- ✓ Noise reduction material is used to reduce the noise from the bottom of the train
- ✓ Sound insulation barrier to reduce the radiation noise of the pantograph.
- ✓ High-performance sound absorption materials in cabin





02 Research Progress



2.2 Shift2 rail

Recent progress from Pro. David J. Thompson

- Mic array for beamforming
- Near-field array for WSE
- Static and dynamic vibration and noise for ATPA (and MISO)

Field test to gather validation data

- One week in June 2016
- High speed track near Munich
- DB Schallmesswagen
- Wheel and rail roughness
- Modal analysis of wheel
- Track decay rate
- Wheel / rail vibration and noise
- Mic array for beamforming
- Near-field array for WSE
- Static and dynamic vibration and noise for ATPA (and MISO)

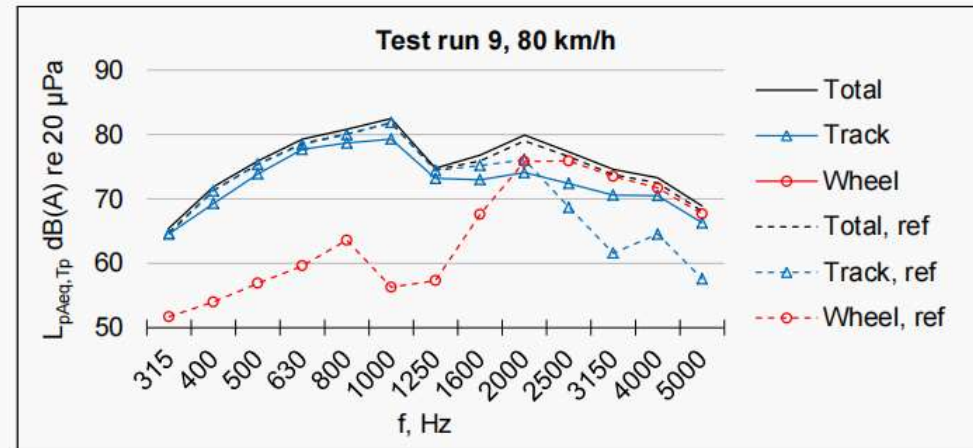


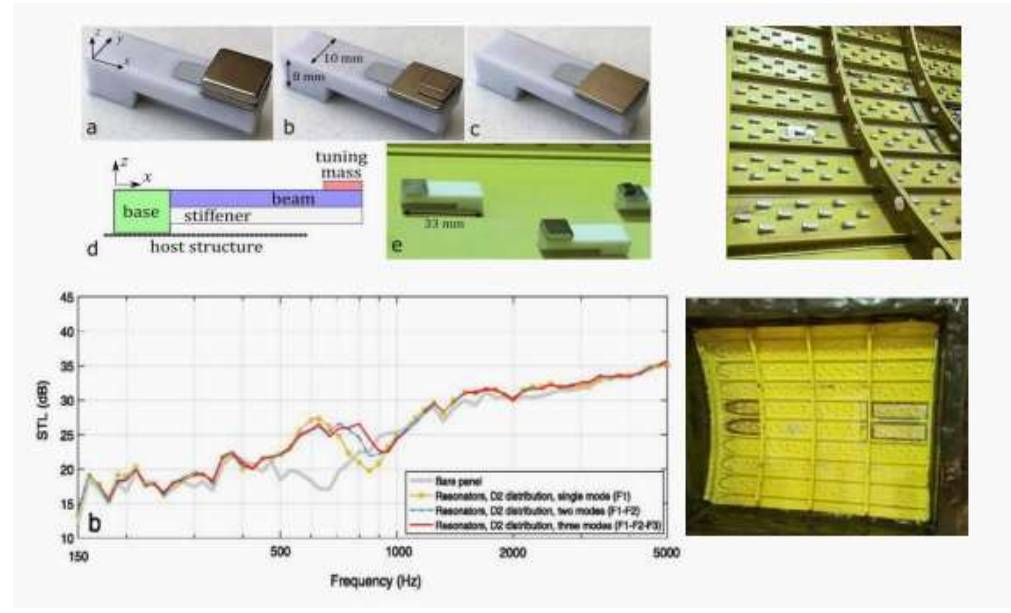
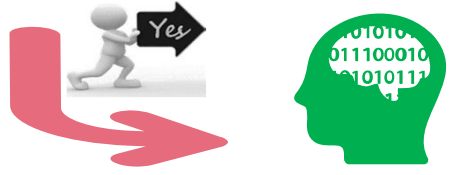
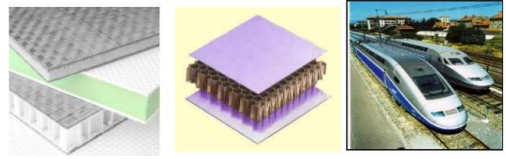
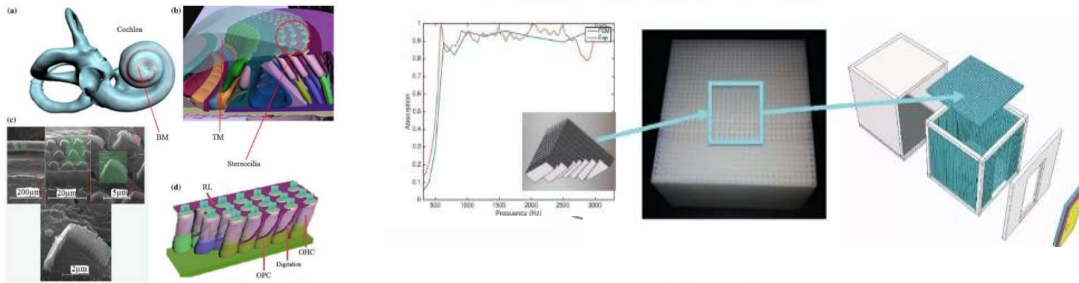
Figure 124. Noise separation result obtained with MISO method compared with reference result, Test run 9 at 80 km/h, Mic 3



02 Research Progress

2.3 Canada

- New acoustic insulation materials in aircraft cabin



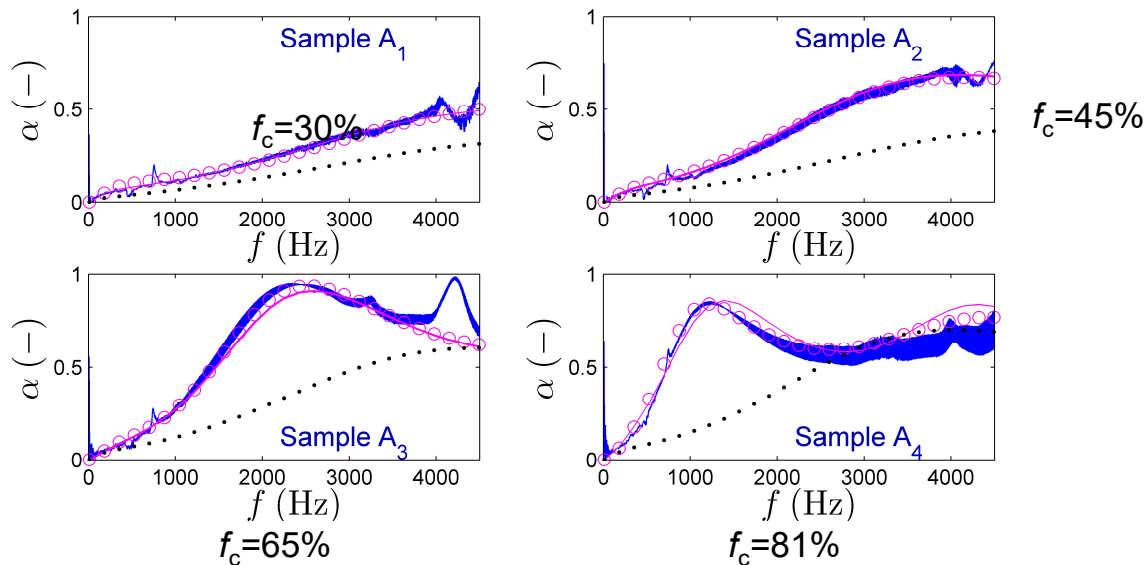
Large aircraft plate for improving TL at ring frequency range , total mass added from 5%-8.5% (Christophe Droz et al, jasa,2019)



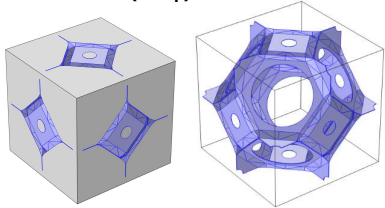
2.4 France

- New acoustic absorptive materials for low frequency noise control

Effects of membranes



Increasing of the membrane level f_c \nearrow from 29%(A₁) to 81 % (A₄) has a strong influence on sound absorption.



By Van Hai Trinh, Camille Perrot;

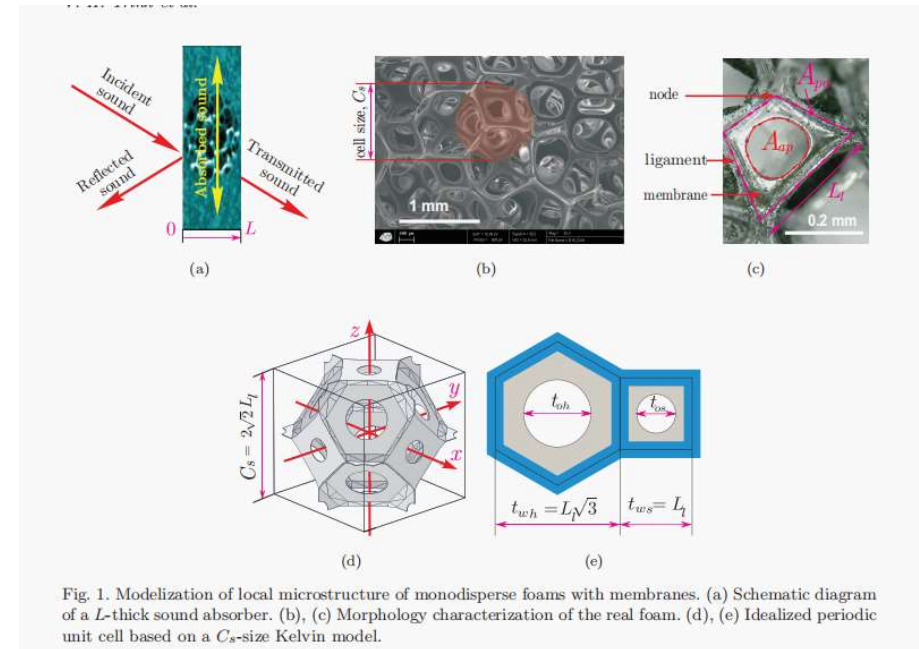


Fig. 1. Modelization of local microstructure of monodisperse foams with membranes. (a) Schematic diagram of a L -thick sound absorber. (b), (c) Morphology characterization of the real foam. (d), (e) Idealized periodic unit cell based on a C_s -size Kelvin model.

- Vanhai Trinh, Dengke Li, Mu He, Xin Li, Modeling sound absorption of graded foam absorbers via polynomial surrogate technique, Journal of Theoretical and Computational Acoustics, 2021.

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Motivations & background



Research progress



Engineering application view



Challenges & opportunities



3.1 Sound absorption

➤ Concept of sound absorption

$$W_i = W_r + W_\alpha + W_t$$

Reflection coefficient $r = \frac{W_r}{W_i}$

Transmission coefficient $\tau = \frac{W_t}{W_i}$

- Sound absorption coefficient is defined as

$$\alpha = 1 - r = 1 - \frac{W_r}{W_i} = \frac{W_\alpha + W_t}{W_i}, (0 \leq \alpha \leq 1)$$



3.1 Sound absorption

➤ Concept of sound absorption

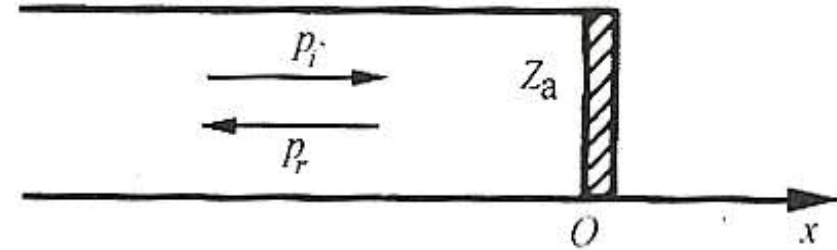
$$p_i = p_{ai} e^{j(\omega t - kx)}$$

$$p_r = p_{ar} e^{j(\omega t + kx)}$$

$$r_p = \frac{p_{ar}}{p_{ai}} = |r_p| e^{j\sigma\pi}$$



$$\alpha = \frac{4r}{(1+r)^2 + x^2}, \quad r = \frac{R_s}{\rho_0 c_0}, \quad x = \frac{X_s}{\rho_0 c_0}$$



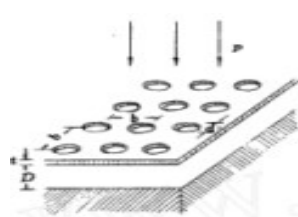
$$\alpha = 1 - r_I = 1 - r_p^2$$

- To achieve a broadband sound absorption coefficient: $r \longrightarrow 1, x \longrightarrow 0$ or $(1+r) < x$
- It is easy to increase damping to overdamping
- Difficult to minimize acoustic impedance

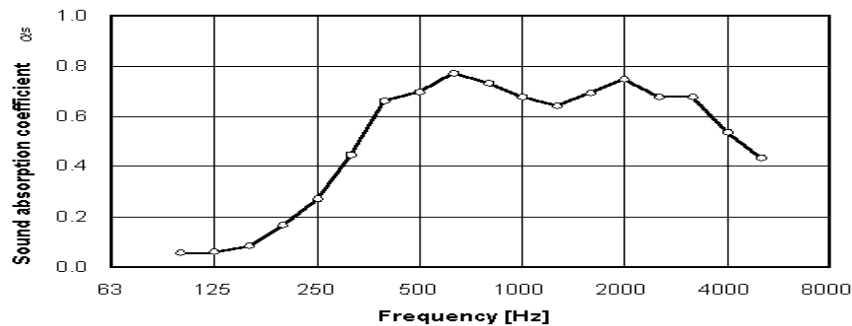


3.1 Sound absorption

● MPP structure



$d < 1\text{mm}$,
 $\phi = 1 \sim 3\%$



Maa D. Y., J. Acoust. Soc. Am. 104(5), 1998.

$$\rho \dot{u} - \frac{\eta}{r_1} \frac{\partial}{\partial r_1} \left(r_1 \frac{\partial}{\partial r_1} u \right) = \frac{\square p}{t}$$

$$Z_1 = \frac{\square p}{\bar{u}} = j\omega \rho t \left[1 - \frac{2}{x\sqrt{-j}} \frac{J_1(x\sqrt{-j})}{J_0(x\sqrt{-j})} \right]^{-1}$$

$$Z_1 = \frac{32\rho\mu t}{d^2} \sqrt{1 + \frac{x^2}{32}} + j\omega \rho t \left[1 + \frac{1}{\sqrt{3^2 + \frac{x^2}{2}}} \right]$$

$$r = \frac{32\mu}{\rho c} \frac{t}{d^2} \left[\sqrt{1 + \frac{x^2}{32}} + \frac{\sqrt{2}x}{8} \frac{d}{t} \right]$$

$$m = \frac{t}{\rho c} \left[1 + \frac{1}{\sqrt{3^2 + \frac{x^2}{2}}} + 0.85 \frac{d}{t} \right]$$

$$Z_D = -j\rho c \cot\left(\frac{\omega D}{c}\right)$$

$$\alpha = \frac{4r}{(1+r)^2 + \left(\omega m - \cot\left(\frac{\omega D}{c}\right)\right)^2}$$

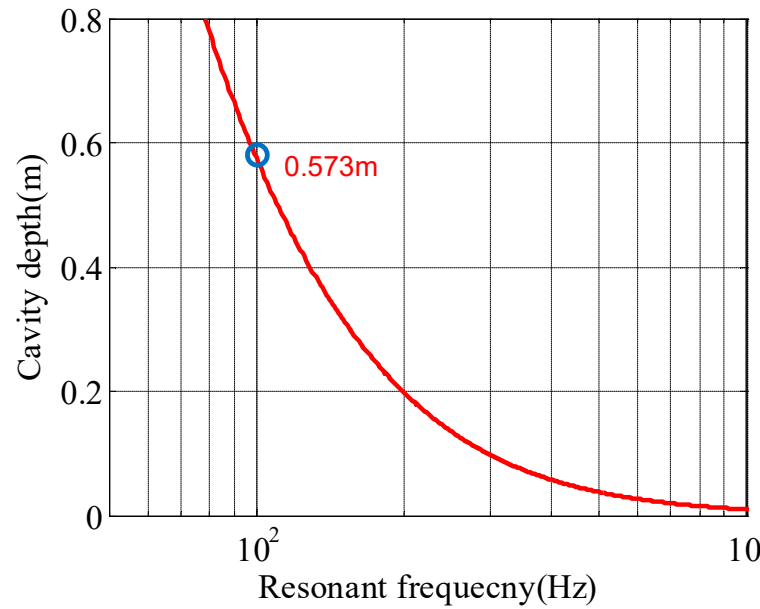
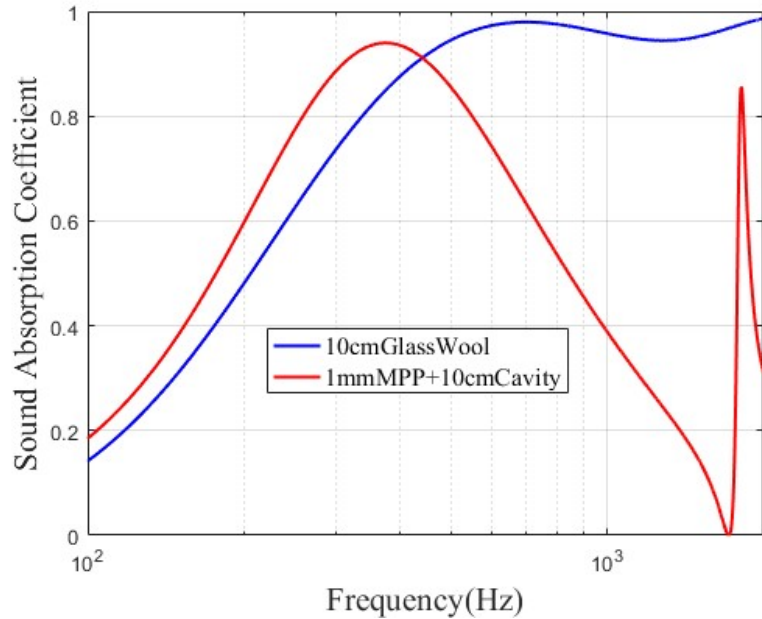
$$r \rightarrow 1, \left| \omega m - \cot\left(\frac{\omega D}{c}\right) \right| \rightarrow 0 \quad \alpha \rightarrow 1$$

$$f \uparrow \infty \quad \sqrt{\frac{p \downarrow}{tD \uparrow}}$$



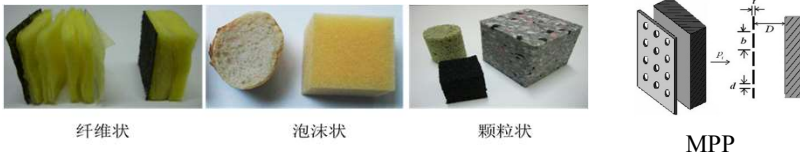
3.1 Sound absorption

● MPP structure



$$f_0 \downarrow = \frac{1}{2\pi} \frac{1}{\sqrt{\frac{D}{3c} \left(m + \frac{D}{3c} \right) \uparrow}}$$

$$\Delta f \downarrow = \frac{1}{2\pi} \frac{1+r}{\left(m + \frac{D}{3c} \right) \uparrow}$$

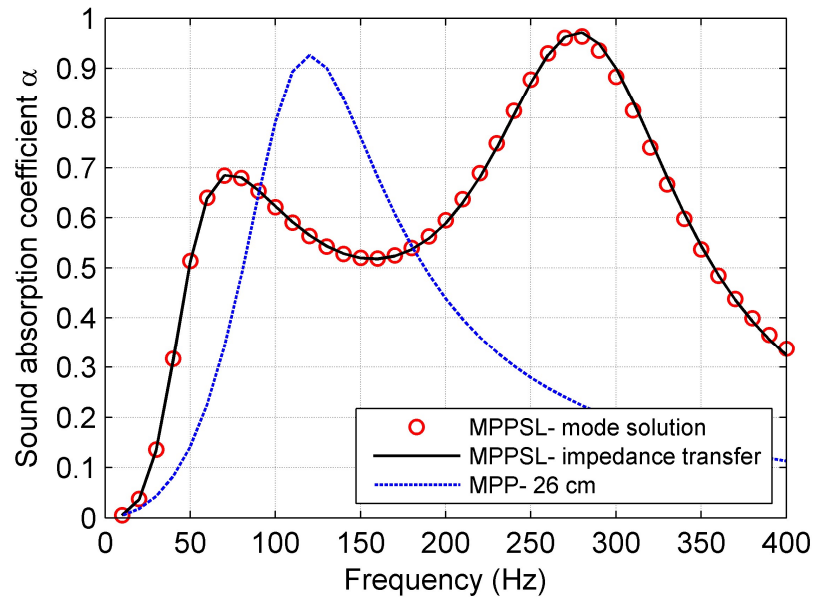


MPP requires a relative thick cavity, and the cavity depth will also narrow the absorption frequency band!

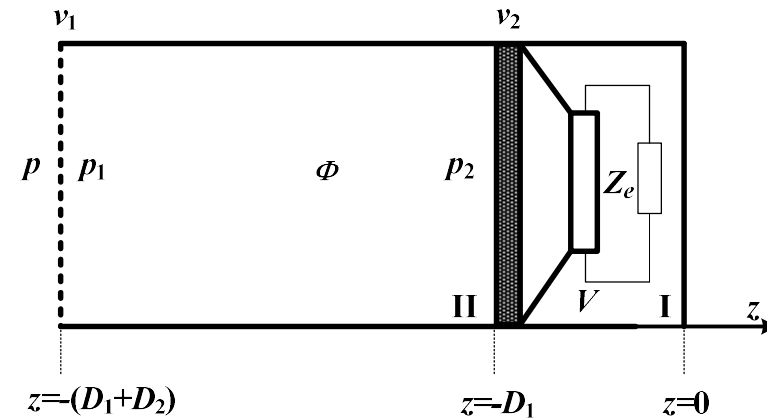


3.1 Sound absorption

● MPP combined structure



Tao JC, Jing RX, Qiu XJ. Sound absorption of a finite micro-perforated plate backed by a shunted loudspeaker. Journal of Acoustical Society of America 2013;135:231-238.

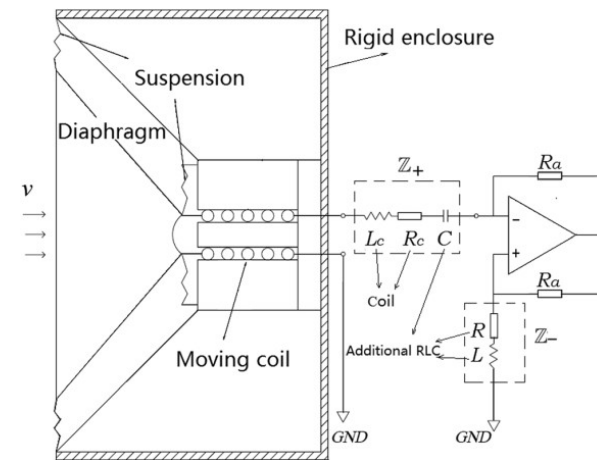
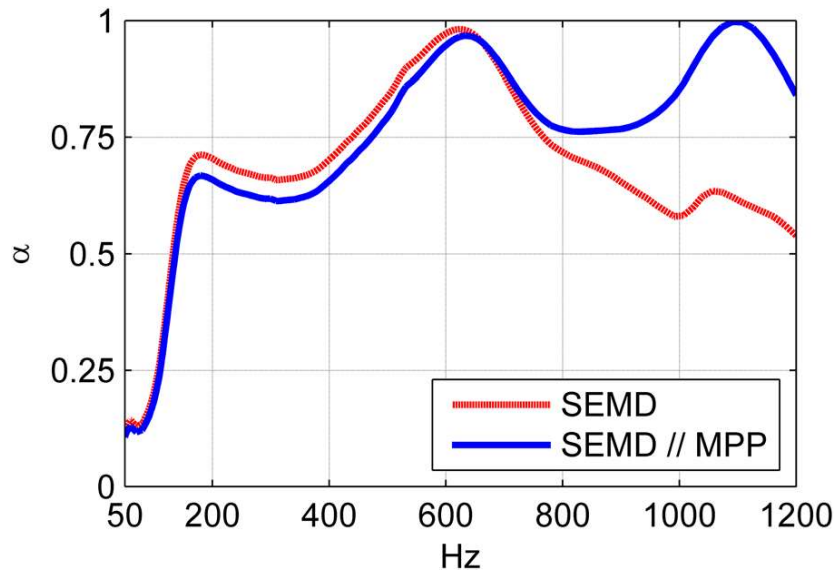


Acoustic absorption structure with microperforated panel and a bypass circuit in a speaker



3.1 Sound absorption

● MPP combined structure



MPP combining with electro-acoustical coupled speaker

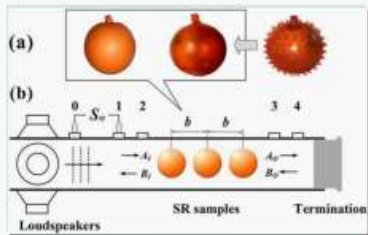
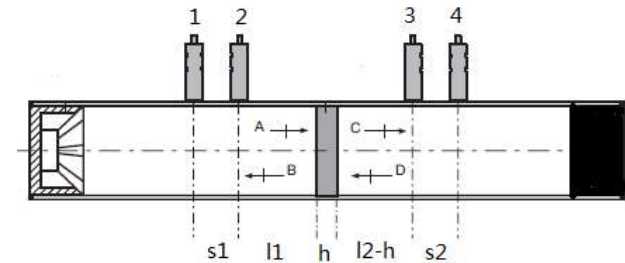
- Yumin Zhang, Yum-Ji Chan, and Lixi Huang, Thin broadband noise absorption through acoustic reactance control by electro-mechanical coupling without sensor. *J Acoust Soc Am* 2014;135(5):2738–2745.



3.1 Sound absorption

● Sonic crystals

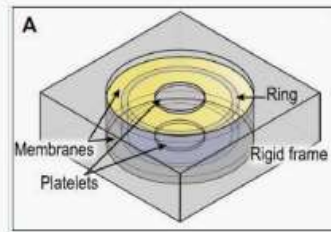
- A. Using 'elastic/soft ball' to realize resonances (X. Jing, et al, Scientific Reports, 2015)
- B. Using 'Helmholtz Resonator' to achieve resonances (M. Reynolds et al, ASA meeting, 2013)
- C. Using 'membrane and mass' to achieve cell resonances 2013 (P. Sheng et al, Phys. Rev. Lett. 2008)
- D. Using 'double membrane and mass' to achieve multiple resonances (P. Sheng et al, Phys. Rev. Lett. 2013).
- E. Using 'shunt circuit' to achieve mechanical-circuit resonances (Hao Zhang, et al, Phys. Rev. Lett. 2016)



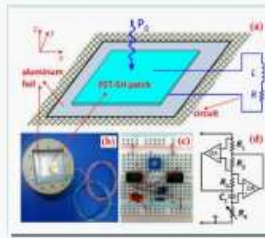
A



B



C



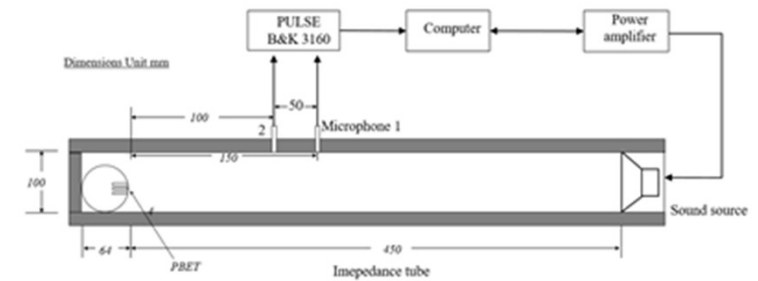
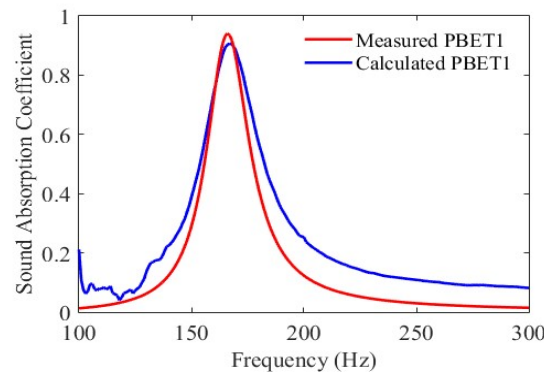
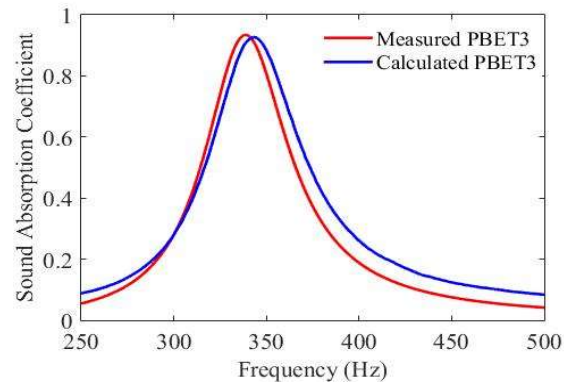
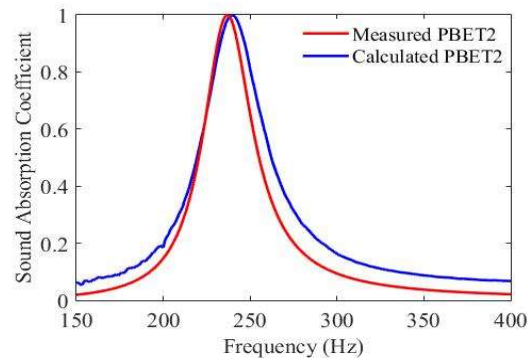
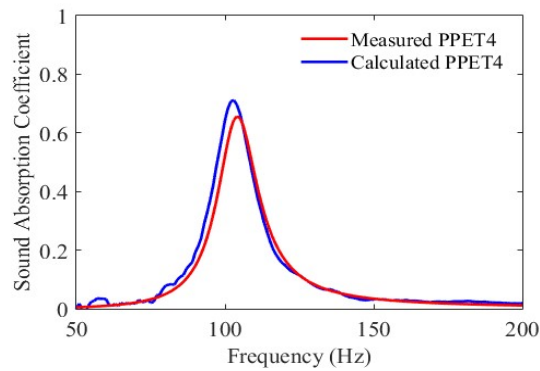
D

sound absorptive performance are tested by impedance tube



3.1 Resonant acoustic absorber

● PBET for low frequency sound absorption



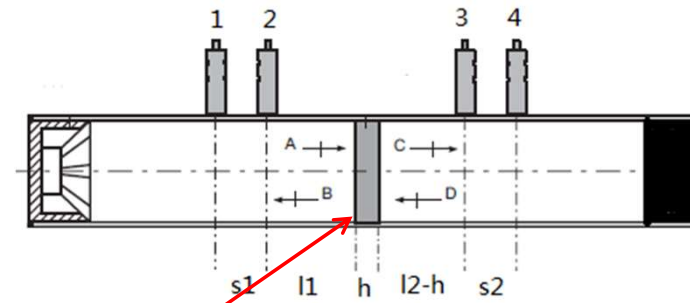
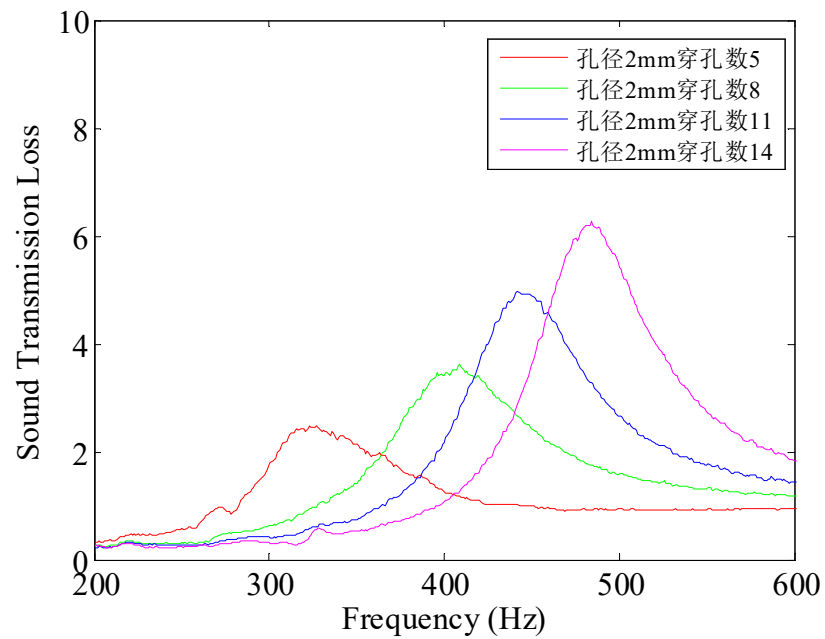
Samples



3.1 Resonant acoustic absorber

● PBET for low frequency sound transmission

ASTM standard E2611-09: Standard test method for measurement of normal incidence sound transmission of acoustical materials based on the transfer matrix method



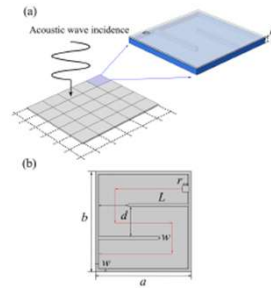


03 Engineering Application

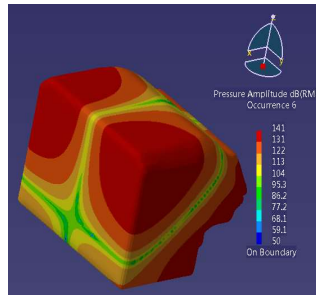


3.1 Resonant acoustic absorber——PBET

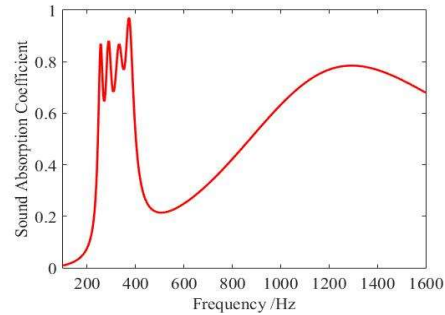
- A thin layer of low frequency noise reduction material
- Wideband noise reduction is achieved by multiple resonant element



Coupling element



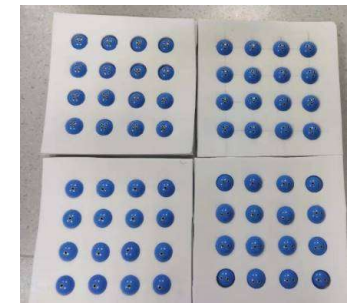
Low frequency mode inside cabin



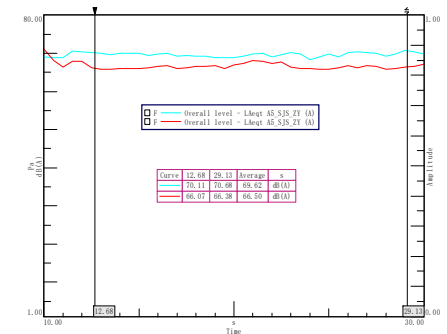
Sound absorption coefficient



Test in locomotive



Samples

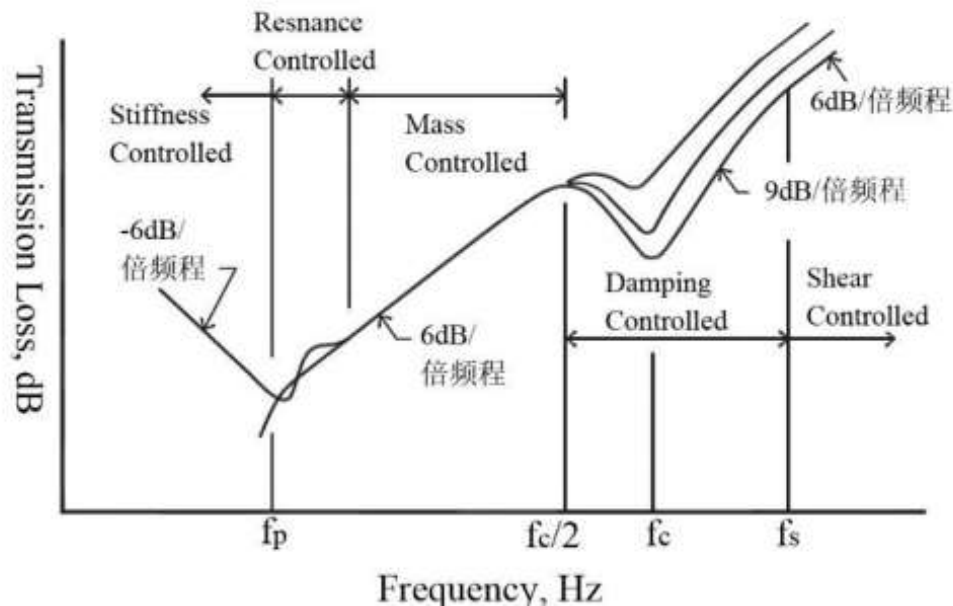


Noise reduction performance above 3dB



3.2 Sound transmission improvement of thin plate

● Transmission loss & Mass Law



$$TL = 20 \log_{10} m + 20 \log_{10} f - 20 \log_{10} (\rho_0 c / \pi) \text{ dB}$$

$$= 20 \log_{10} (mf) - 42 \text{ dB}$$

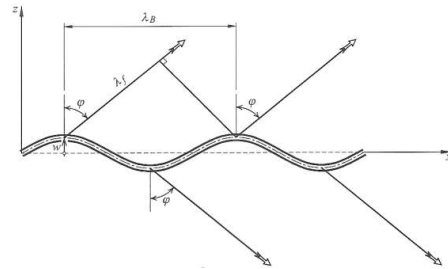
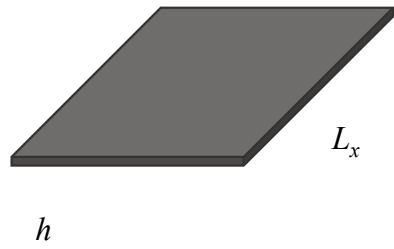
To improve the TL without increasing the weight seems an impossible task !



03 Engineering Application



3.2 Sound transmission improvement of thin plate



$$R = 10 \log \left(\frac{1}{\tau} \right) \text{ avec } \tau = \frac{W_2}{W_1}$$

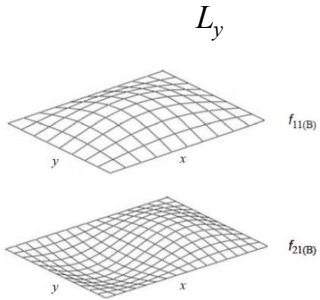
$$W_1 = I_1 S = \frac{\langle p_1^2 \rangle_{t,s} S}{4 \rho_0 c_0}$$

$$W_2 = \frac{\langle p_2^2 \rangle_{t,s} A}{4 \rho_0 c_0}$$

Ainsi $\frac{1}{\tau} = \frac{W_1}{W_2} = \frac{\langle p_1^2 \rangle_{t,s} S}{\langle p_2^2 \rangle_{t,s} A}$

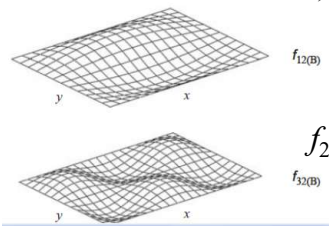
$$R = 10 \log \left(\langle p_1^2 \rangle \right) - 10 \log \left(\langle p_2^2 \rangle \right) + 10 \log \left(\frac{S}{A} \right)$$

$$R = Lp_1 - Lp_2 + \log \left(\frac{S}{A} \right)$$



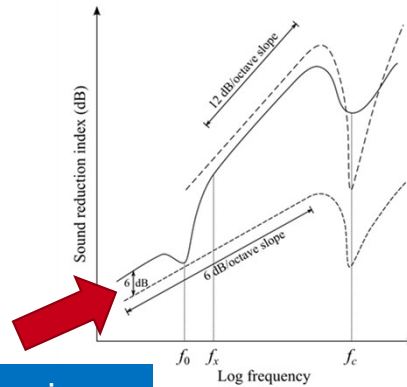
$f_{1,1}$

$f_{2,1}$



$f_{1,2}$

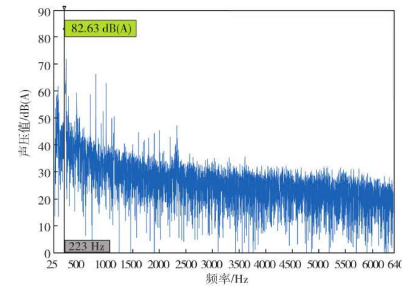
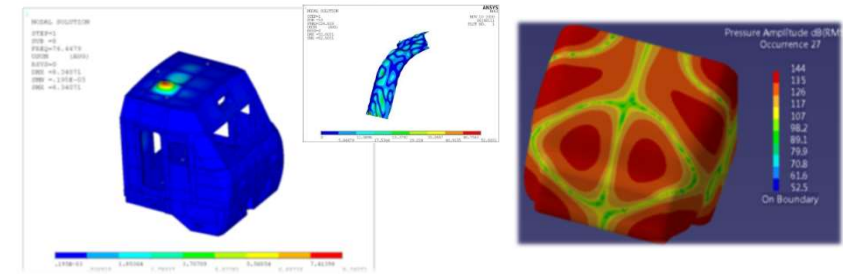
$f_{2,2}$



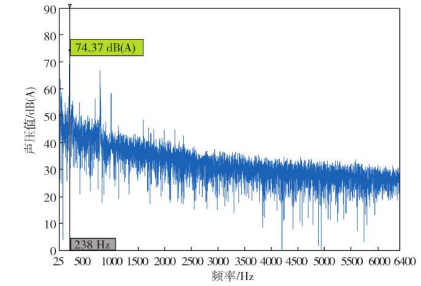
Stiffness&Damping

c: velocity of sound in the material (m / s)
Lx, Ly: plate dimensions (m)
m, n: order of the eigen modes

$$f_{m,n} = \frac{c}{2} \sqrt{\left(\frac{m}{L_x} \right)^2 + \left(\frac{n}{L_y} \right)^2}$$



Before

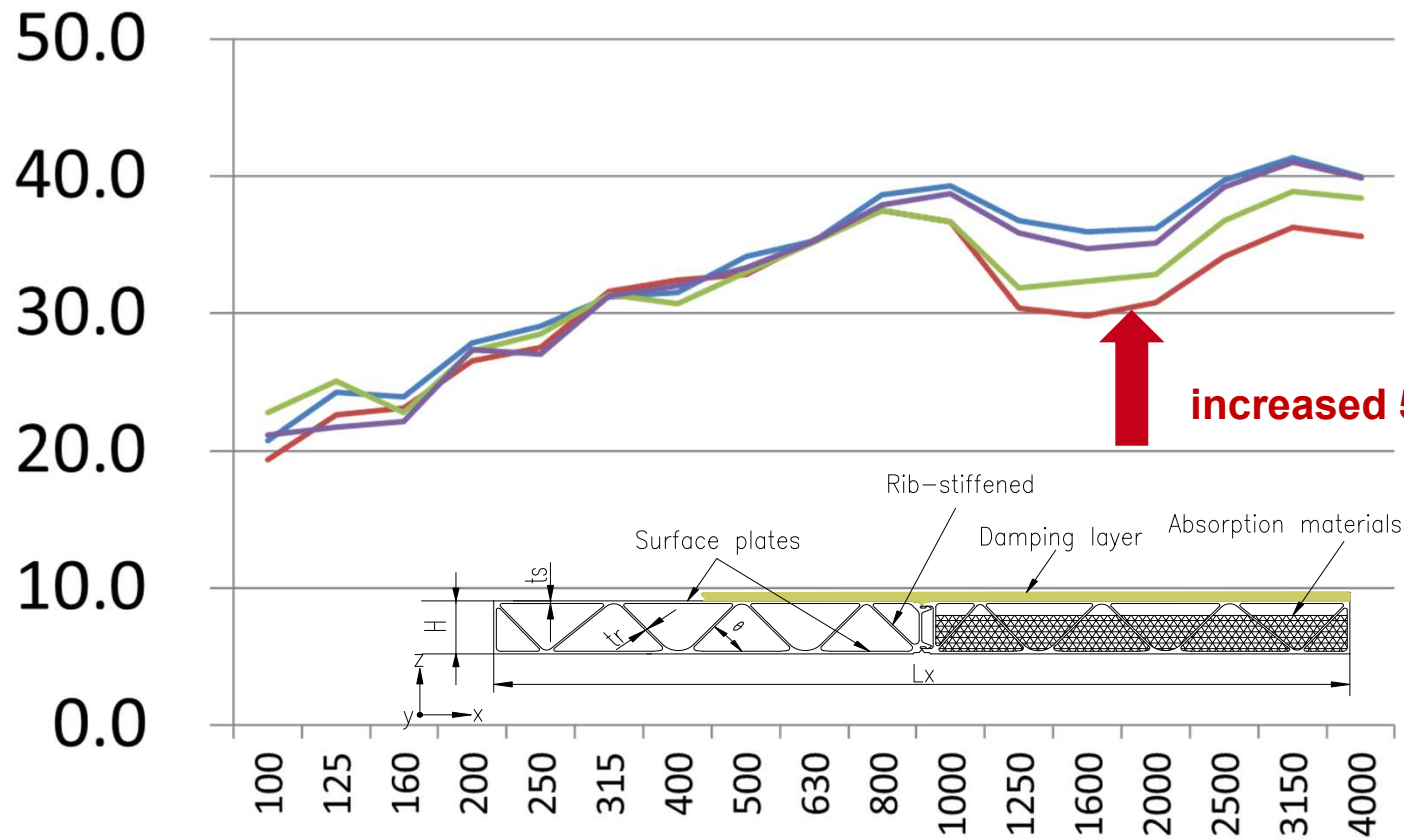


Add damping and stiffener plate

- Stiffness and damping factors are considered to enhance low frequency transmission
- Multi Mode-frequency coupling response is also studied



3.3 Sound absorbing materials



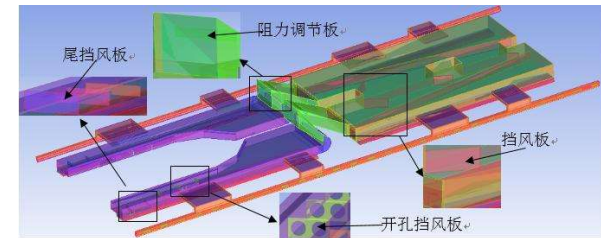
- ✓ Design for high frequency sound reduction
- ✓ Lightweight acoustic structure design with porous foam material
- ✓ The weight of the composite panel increases by approximately 0.2-0.3kg per square meter



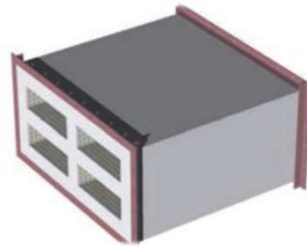


03 Engineering Application

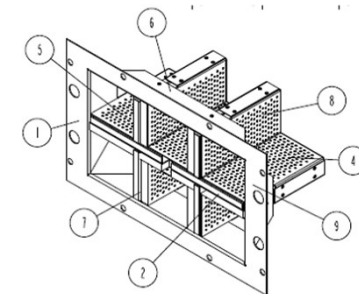
3.4 Acoustic mulffer



Supply airduct



Return airduct



MPP with sound absorbing materials

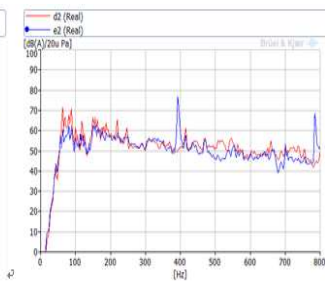
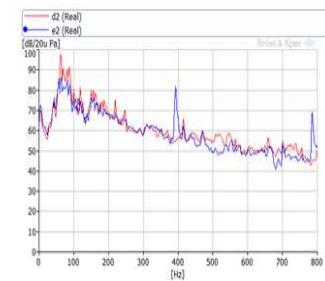
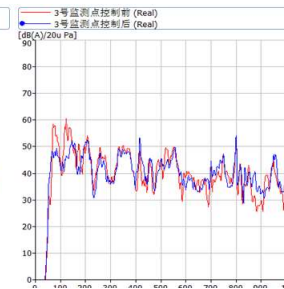
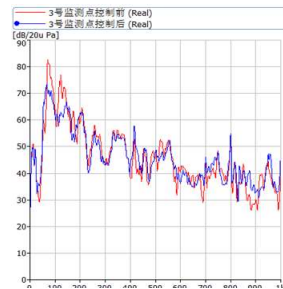
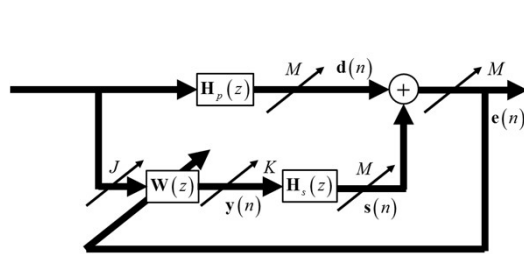
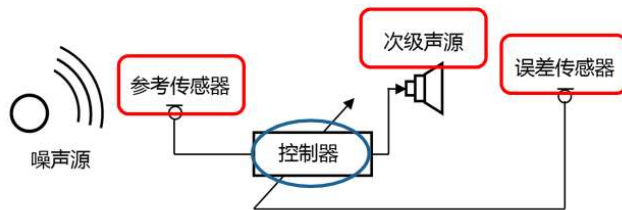
- Sound absorbing structures is both designed for supply and return airduct
- Noise control performance above 3 dB



03 Engineering Application

3.5 Active noise control

➤ Active noise reduction in locomotive cabin



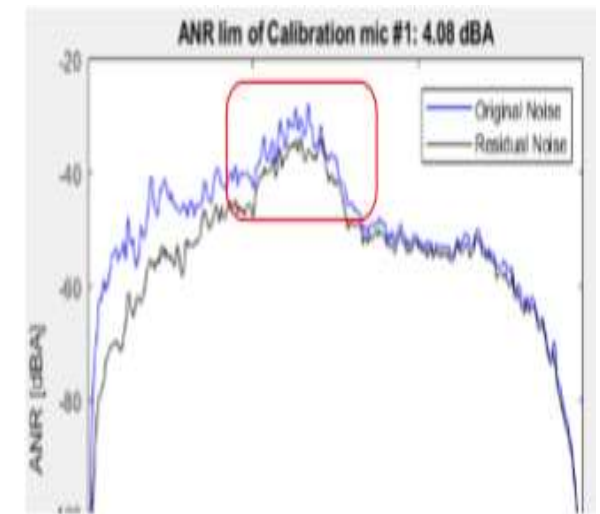
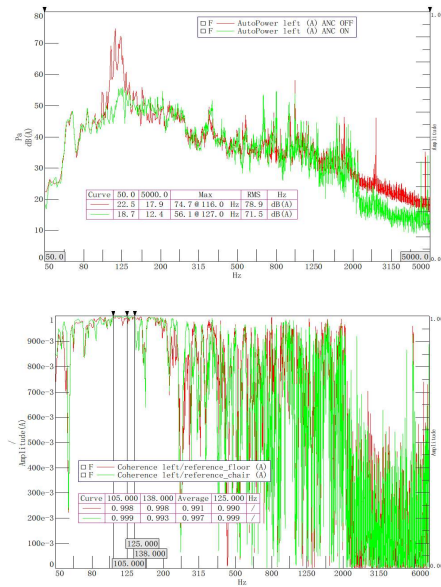
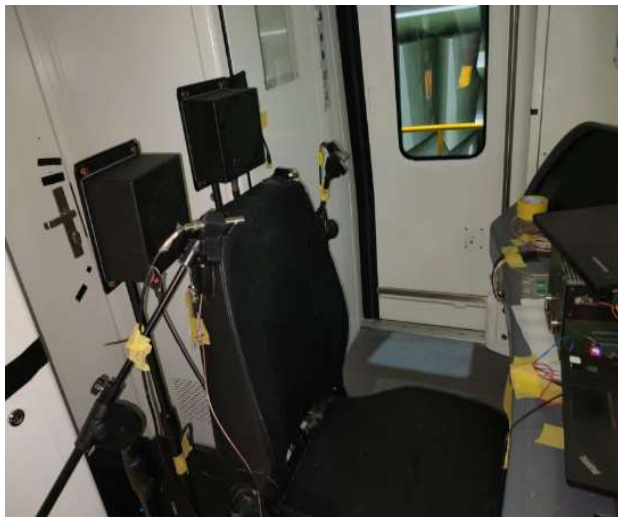
- Both the driver's ear and standing area are considered
- Noise control performance above 3 dB



03 Engineering Application

3.5 Active noise control

➤ Active noise reduction in metro cabin



- the near-field active noise reduction reaches 7.6dB (A)
- the far-field active (0.4m) noise reduction reaches 6.0dB (A)

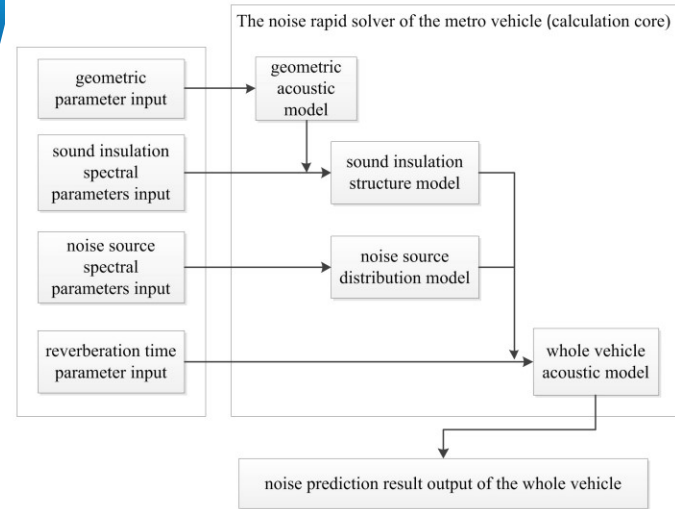
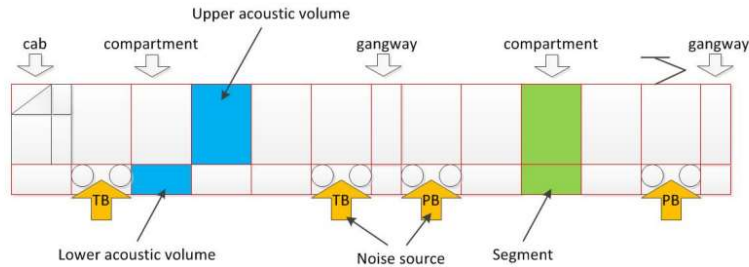


03 Engineering Application

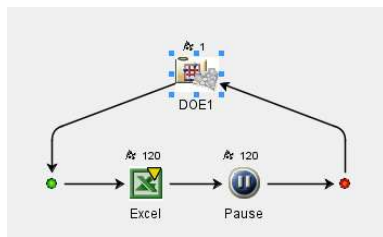


3.6 Noise calculation and optimization

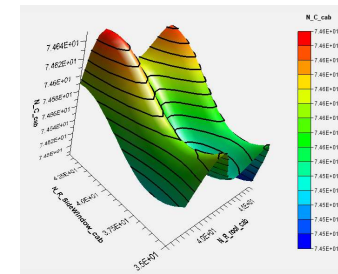
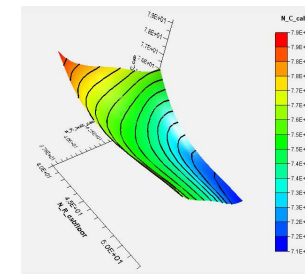
➤ Parameterized vehicle noise rapid solver



➤ Automatic optimization calculation



Run Path	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24		
1	1	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	
2	2	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
3	3	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
4	4	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
5	5	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
6	6	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
7	7	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
8	8	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
9	9	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
10	10	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
11	11	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
12	12	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
13	13	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
14	14	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
15	15	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
16	16	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
17	17	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
18	18	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
19	19	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
20	20	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
21	21	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
22	22	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
23	23	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0
24	24	48.0	41.0	38.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0	48.0



目录 Contents



Motivations & background



Research progress



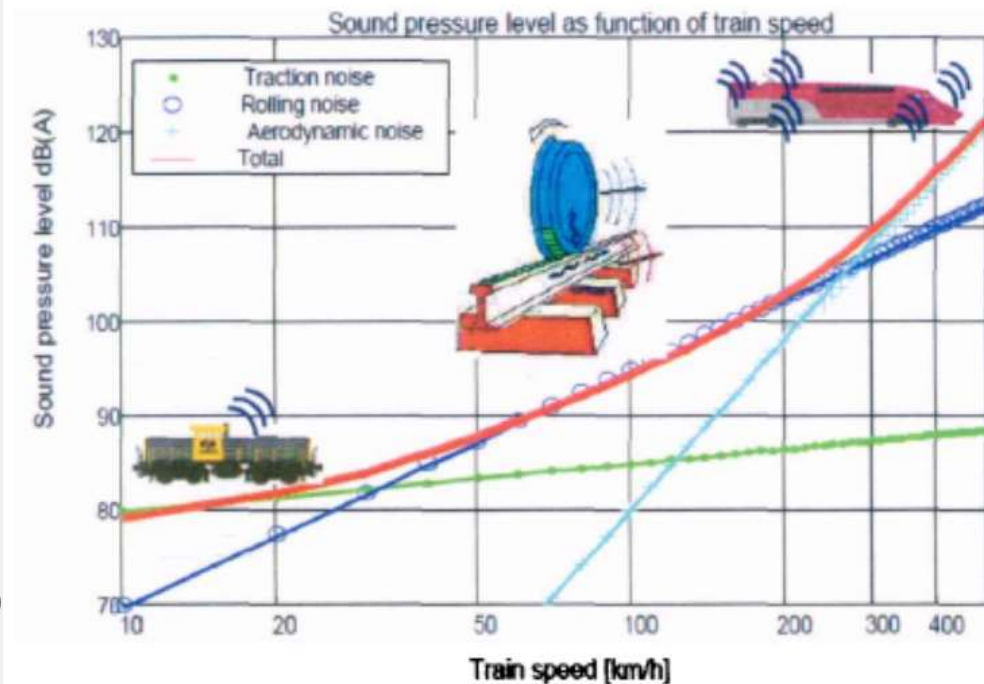
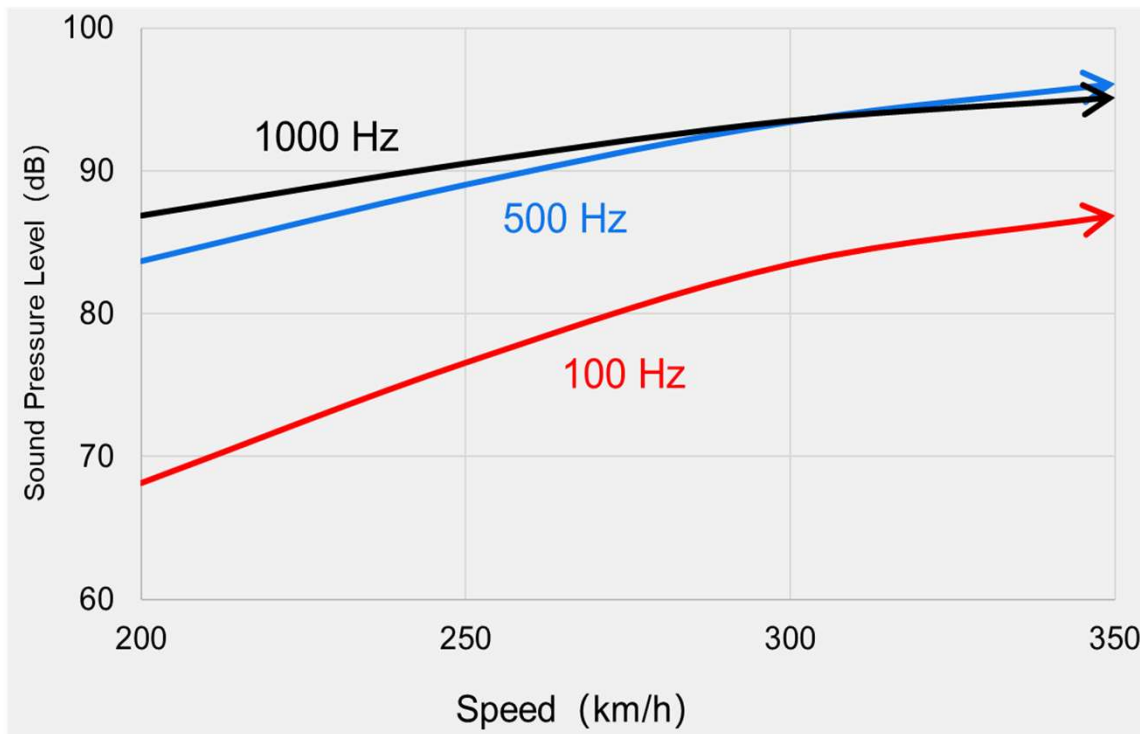
Engineering application view



Challenges & opportunities



4.1 Wheel-rail noise and aerodynamic noise

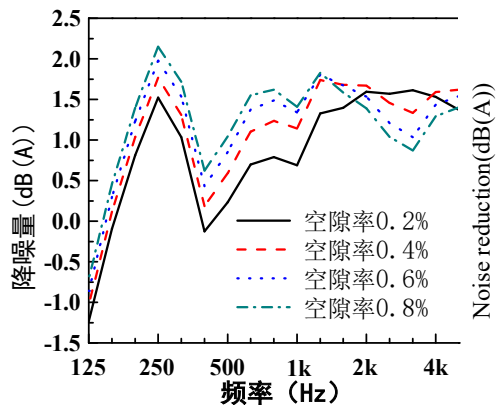


- With the increase of the running speed V , the sound pressure level of the wheel-rail noise and the running speed of the train satisfy $30\log_{10}V$;
- the sound pressure level of aerodynamic noise and the train running speed satisfy $60\log_{10}V$.

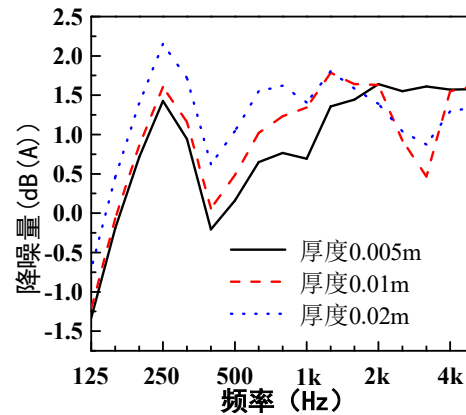


04 Challenges & Opportunities

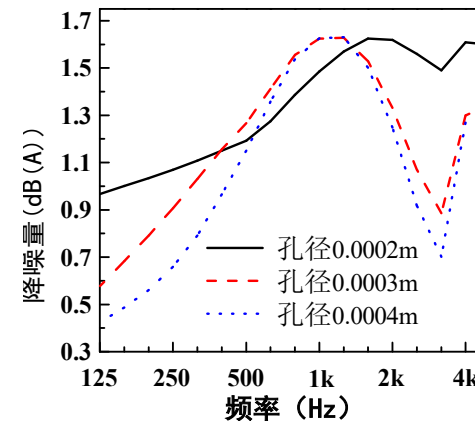
4.1 New sound absorbing materials for wheel-rail noise



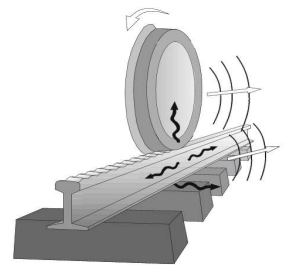
Porosity



Thickness

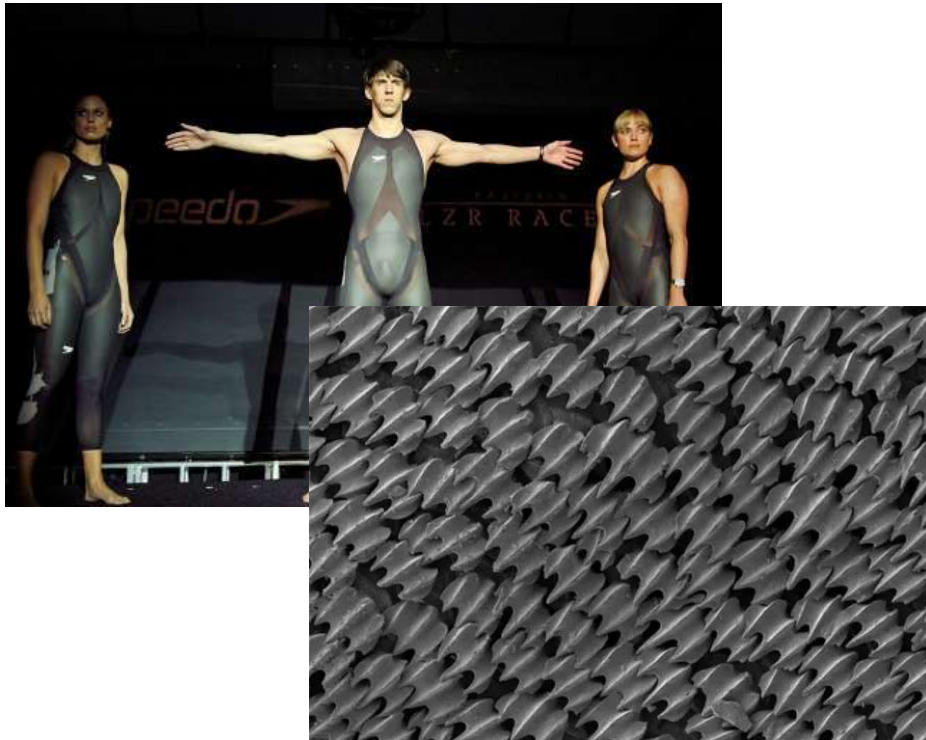


Pore diameter

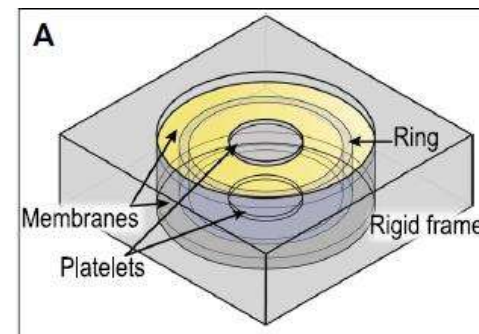
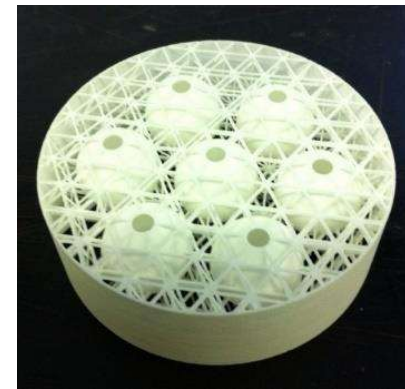


**Around 680Hz
Rail-wheel Noise**

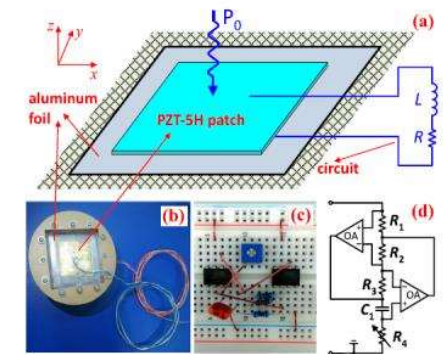
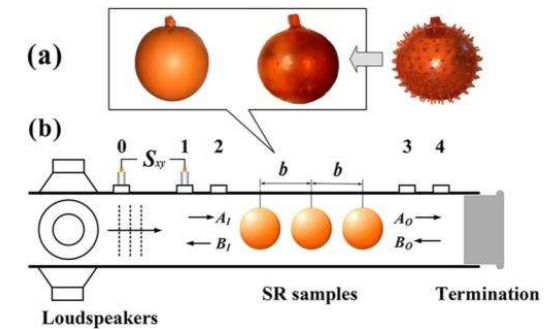
4.2 Acoustic metamaterials



Shark skin resistance reduction material



Acoustic metamaterials designed for low frequency sound absorption



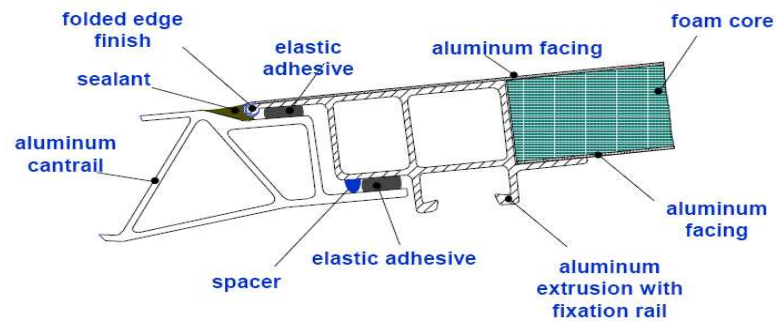


04 Challenges & Opportunities

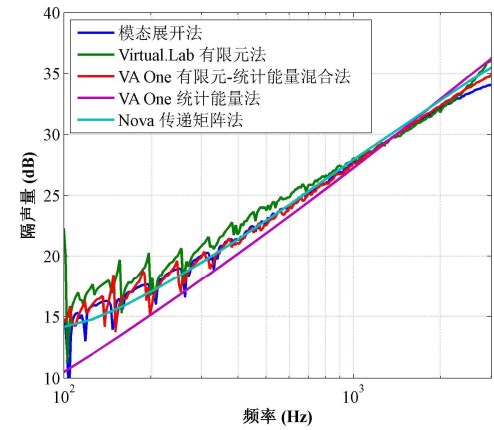
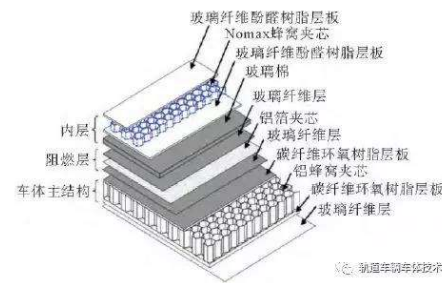
4.3 Lightweight sound insulation structure



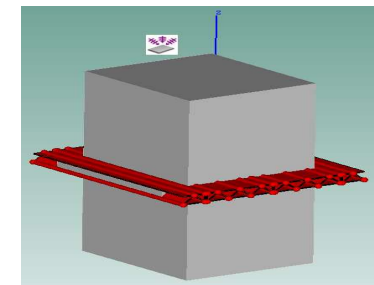
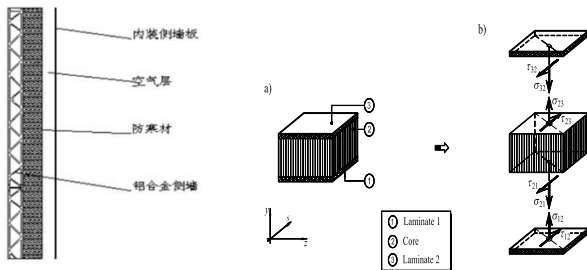
Traditional



Lightweight



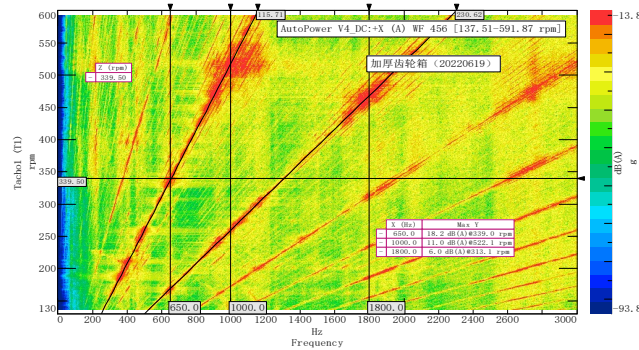
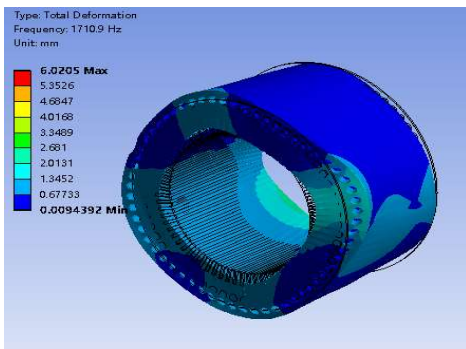
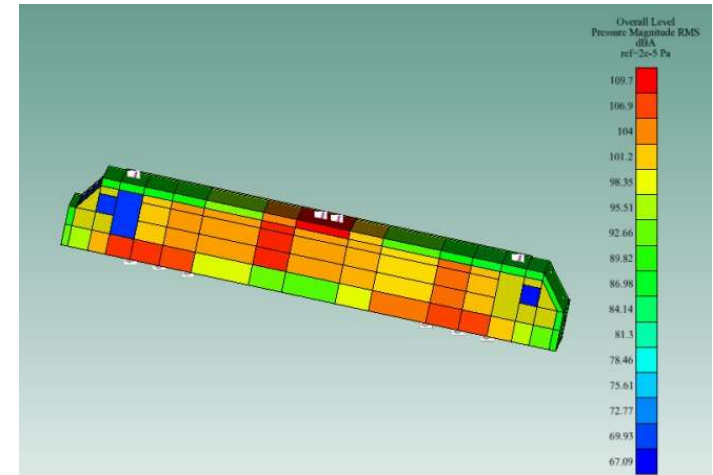
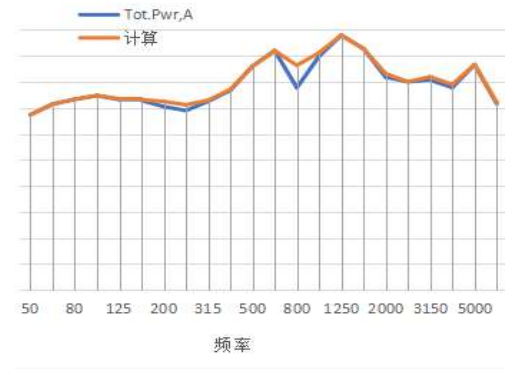
TL





04 Challenges & Opportunities

4.4 Low-noise design of gearbox and motor



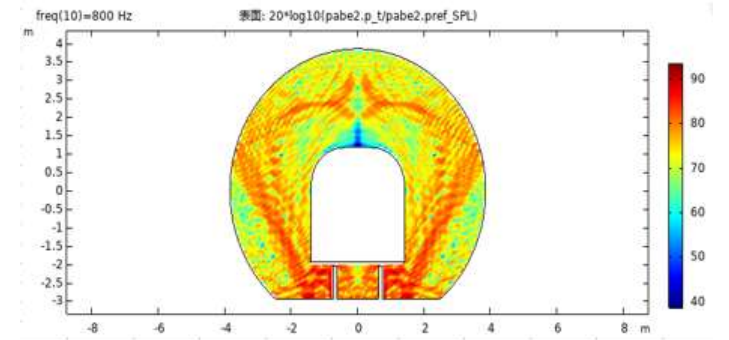
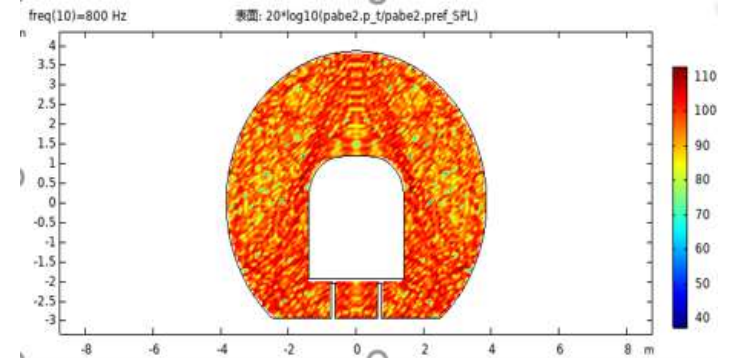
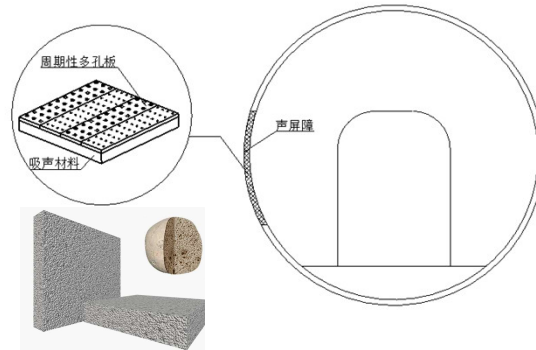
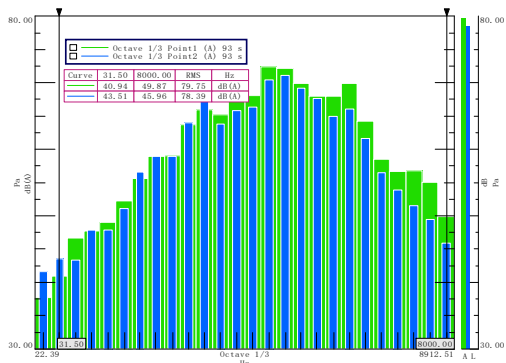
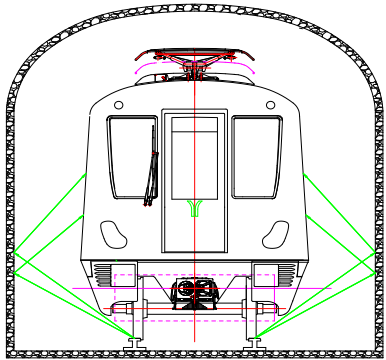
- Gearbox noise test and optimization
- Motor noise test and optimization



04 Challenges & Opportunities



4.5 Noise control in tunnel condition



- New sound absorbing materials to control reverberation time in tunnel
- Design frequency at 200-2000 Hz



[Many thanks!]

