

Sorrento

SAPEM' 23

常熟

Experimental study of granular activated carbon stacks' level- and time-dependent behavior



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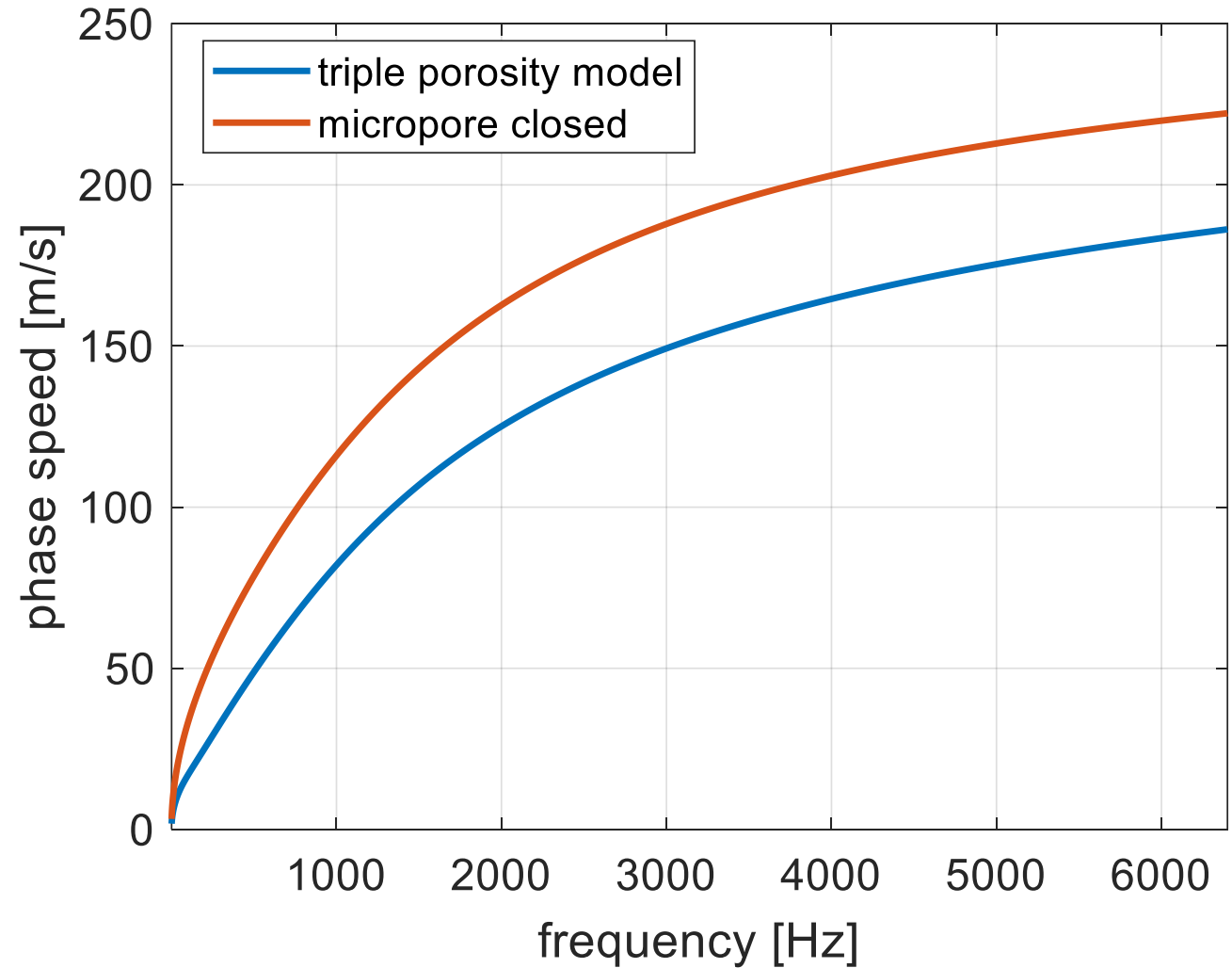
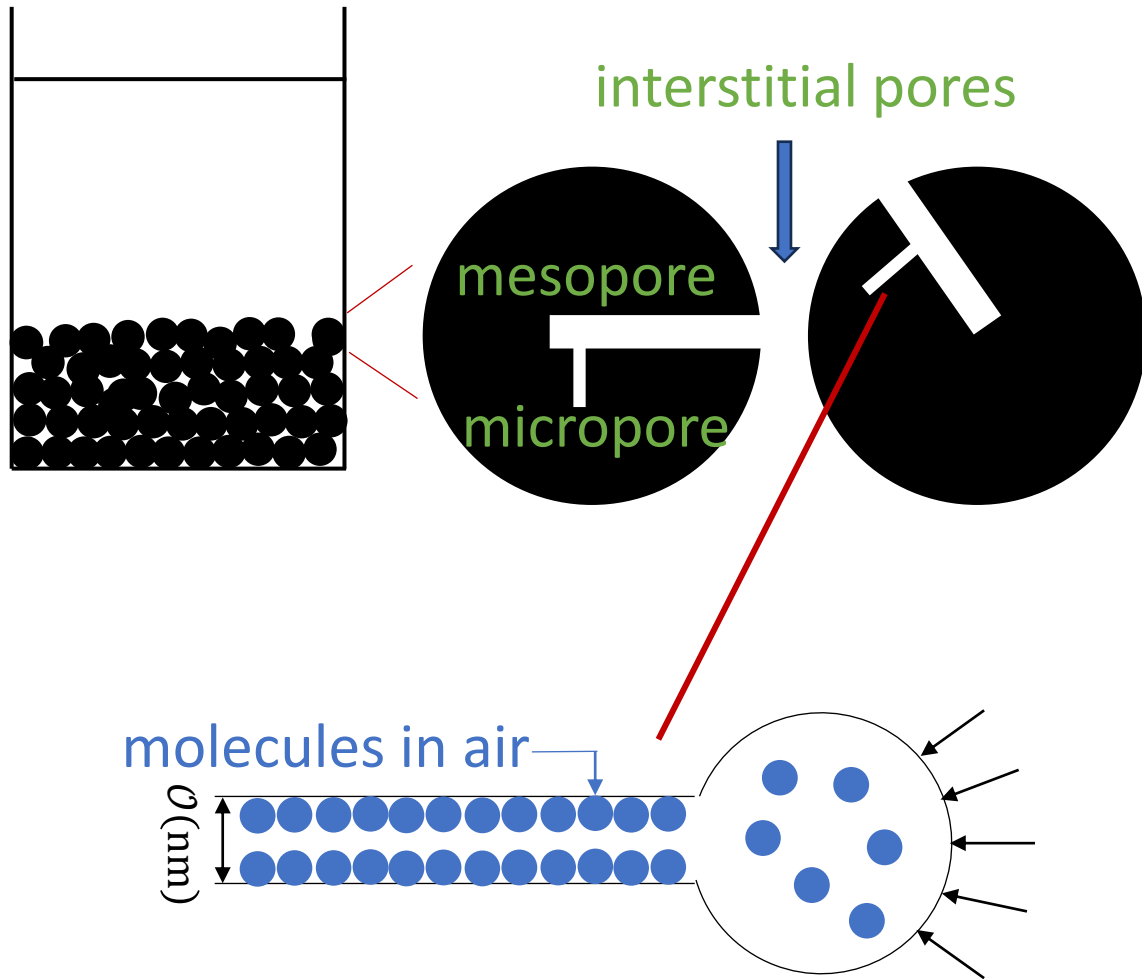
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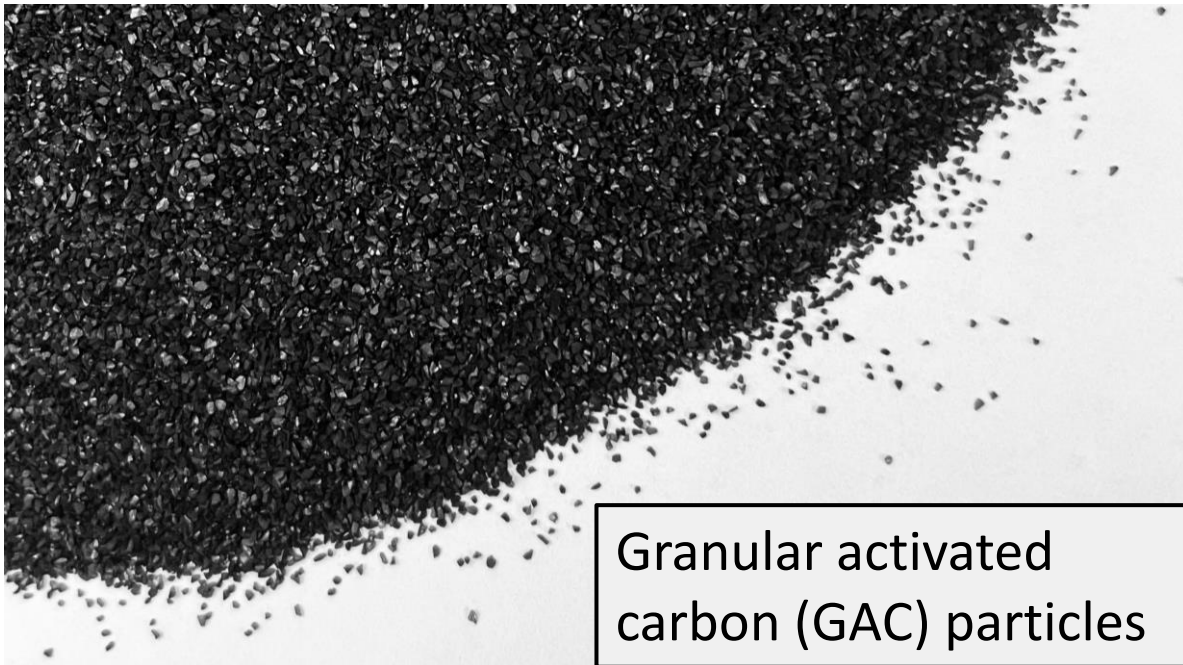
Agenda

- Motivation & test setup
- Circumferential edge-constraint effect
- Level-dependent behavior
- Time-dependent behavior
- Conclusions

Motivation (1/3): hierarchical porosity of the activated carbon particles



Motivation (2/3): particle stacks' benefits & applications



Granular activated carbon (GAC) particles



3M™ Flexile Acoustic Material

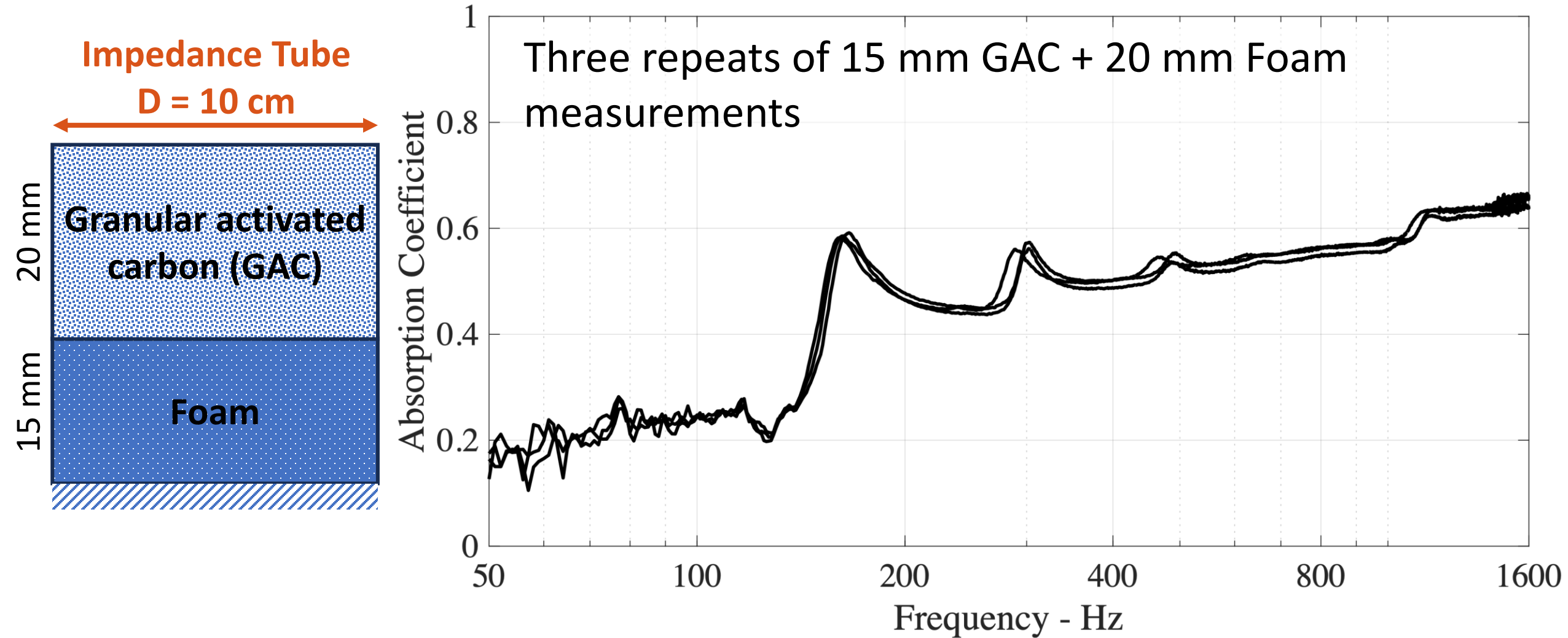
Benefits of high surface area particles:

1. Remarkable sorption characteristics
2. Better low frequency sound absorption

Applications:

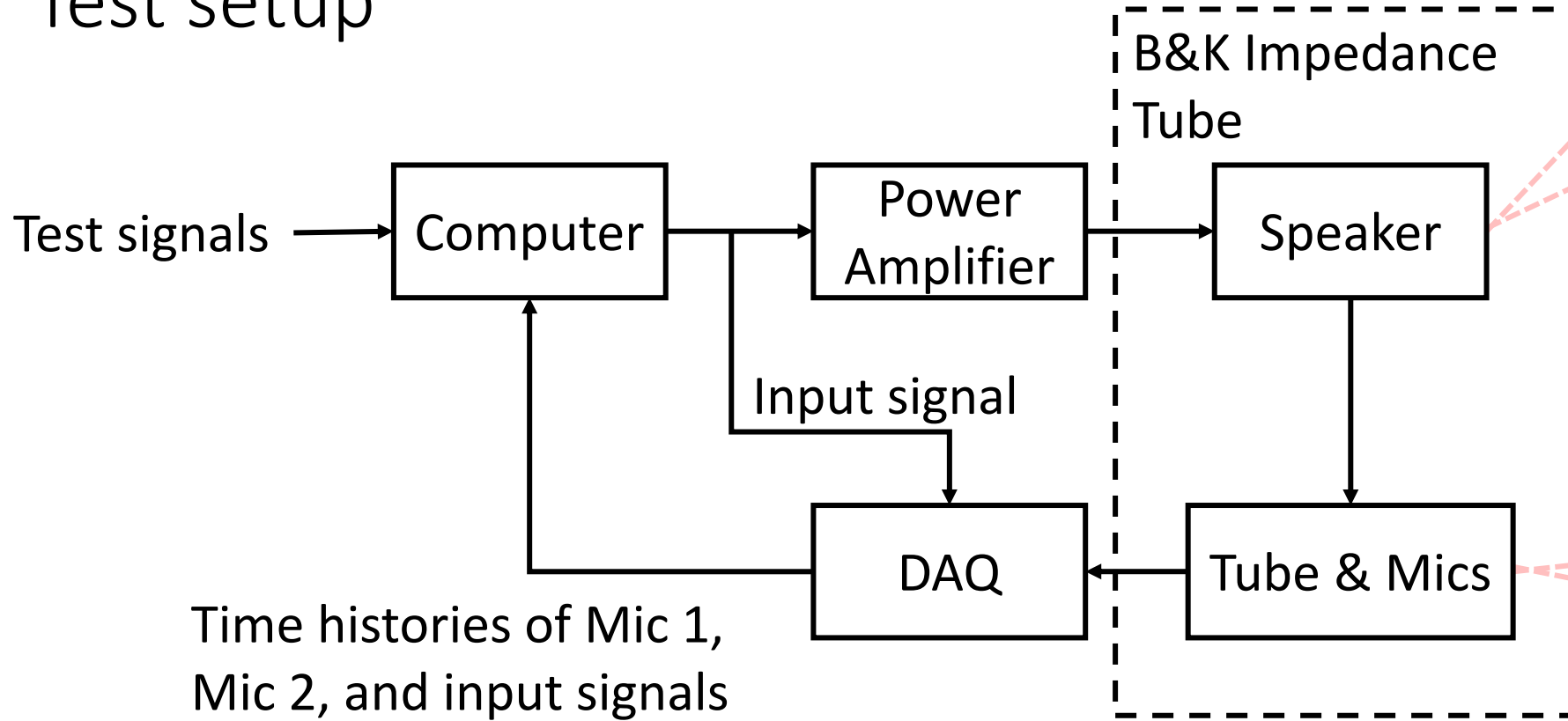
1. when the space to apply the acoustical treatment is limited (e.g., micro-speakers)
2. when one wants to enhance the low-frequency performance of the acoustical treatment (embed particles within the matrix)
3. when the granular particle has already been adopted in various fields, e.g., for thermal insulation (extend it also as an acoustic treatment)

Motivation (3/3): one more thing...

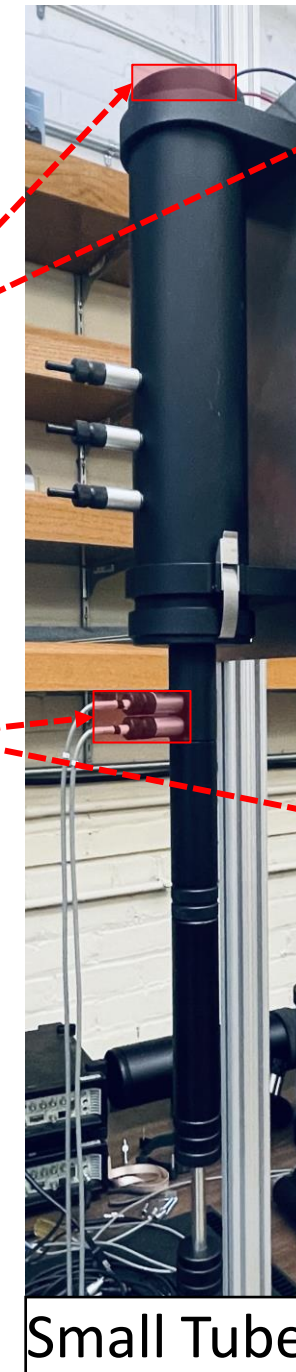


- Need to develop accurate models to allow treatment optimization.
- Must allow for unique behavior of particle stacks: edge effect, level- and time-dependence

Test setup



Granular material	GAC [Type A]	GAC [Type B]	GAC [Type C]	GAC [Type D]
Particle diameter [μm]	250-500	150-300	250-500	150-300
Bulk density [kg/m^3]	520	530	440	410

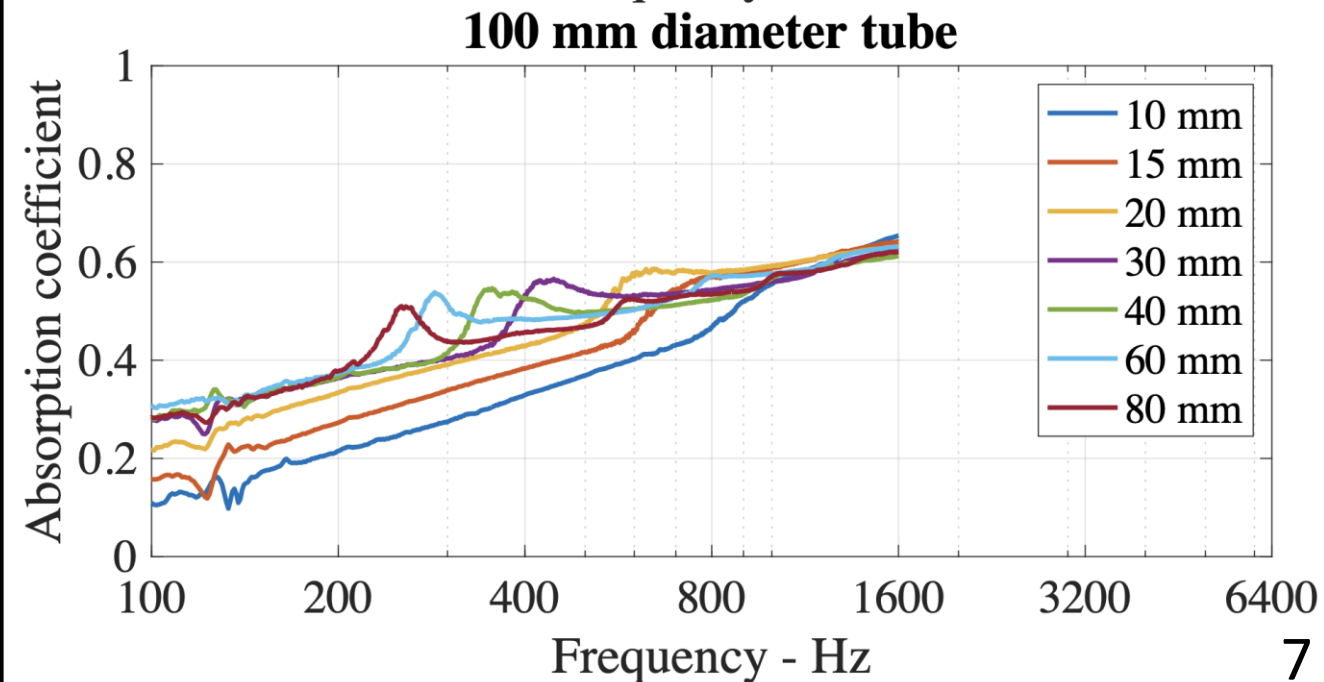
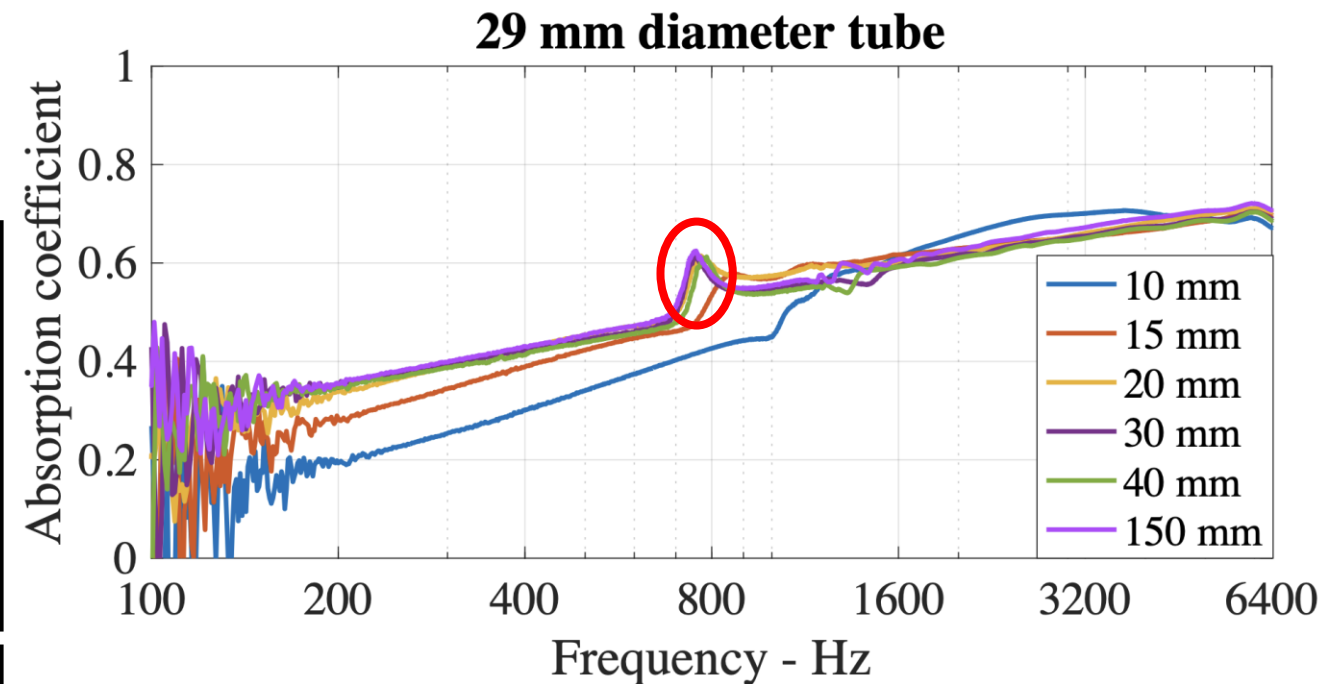
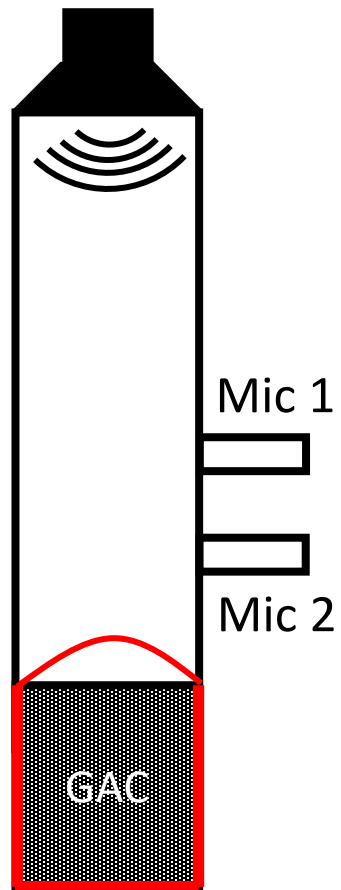


Edge-Constraint Effect

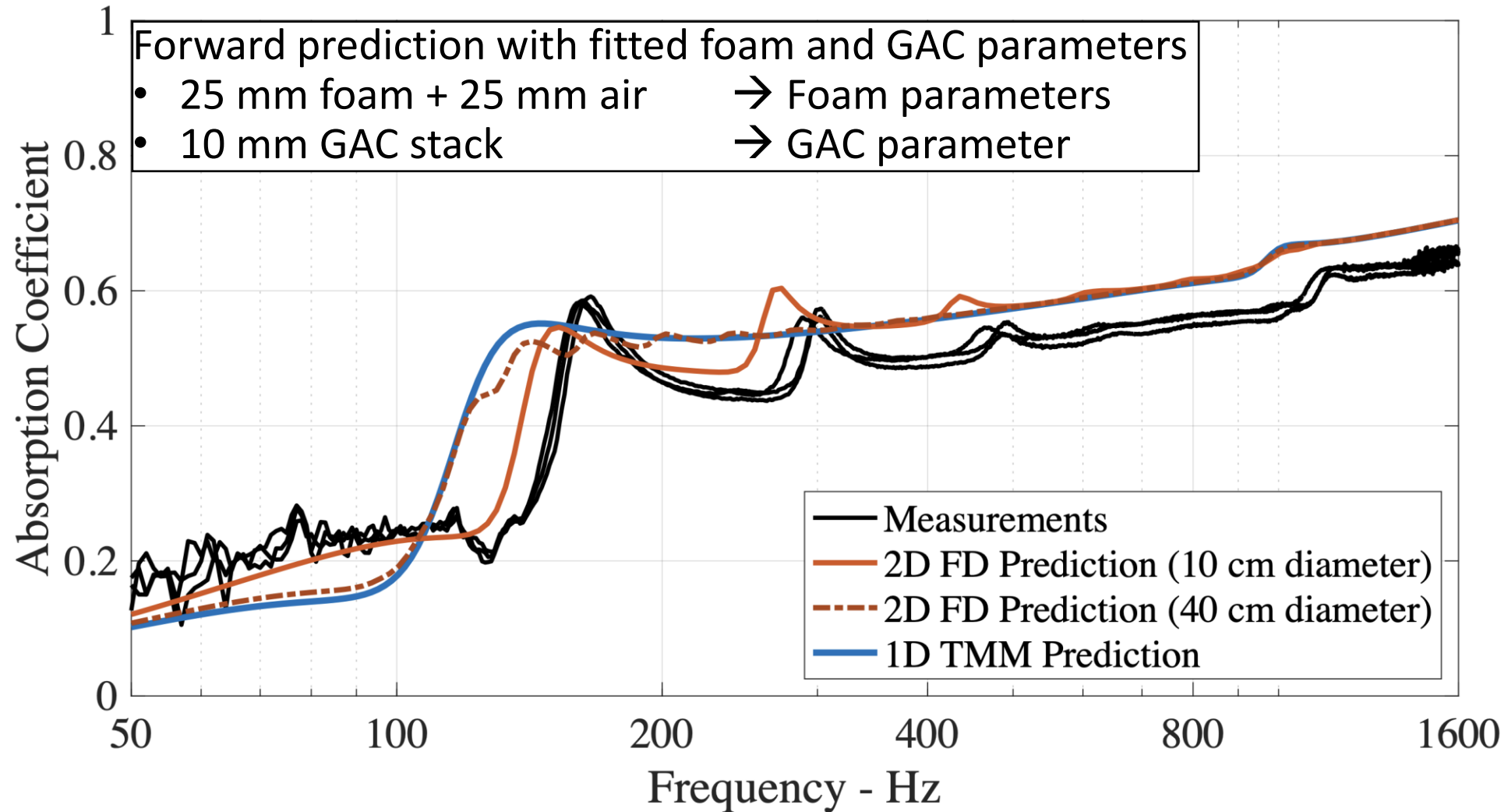
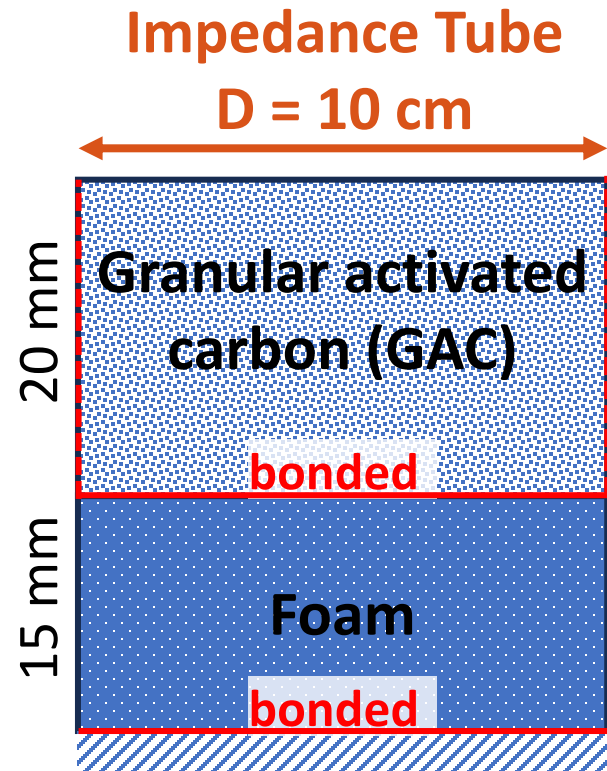
Type A GAC particle stack

- Particle stacks tend to stick to the wall.
- This edge constraint effect can affect the absorption spectrum.

- When the stack depth is greater than the tube diameter, the quarter wave resonance transitions to the first radial model.
- Conventional 1-D models only work when stack depth smaller than the tube diameter

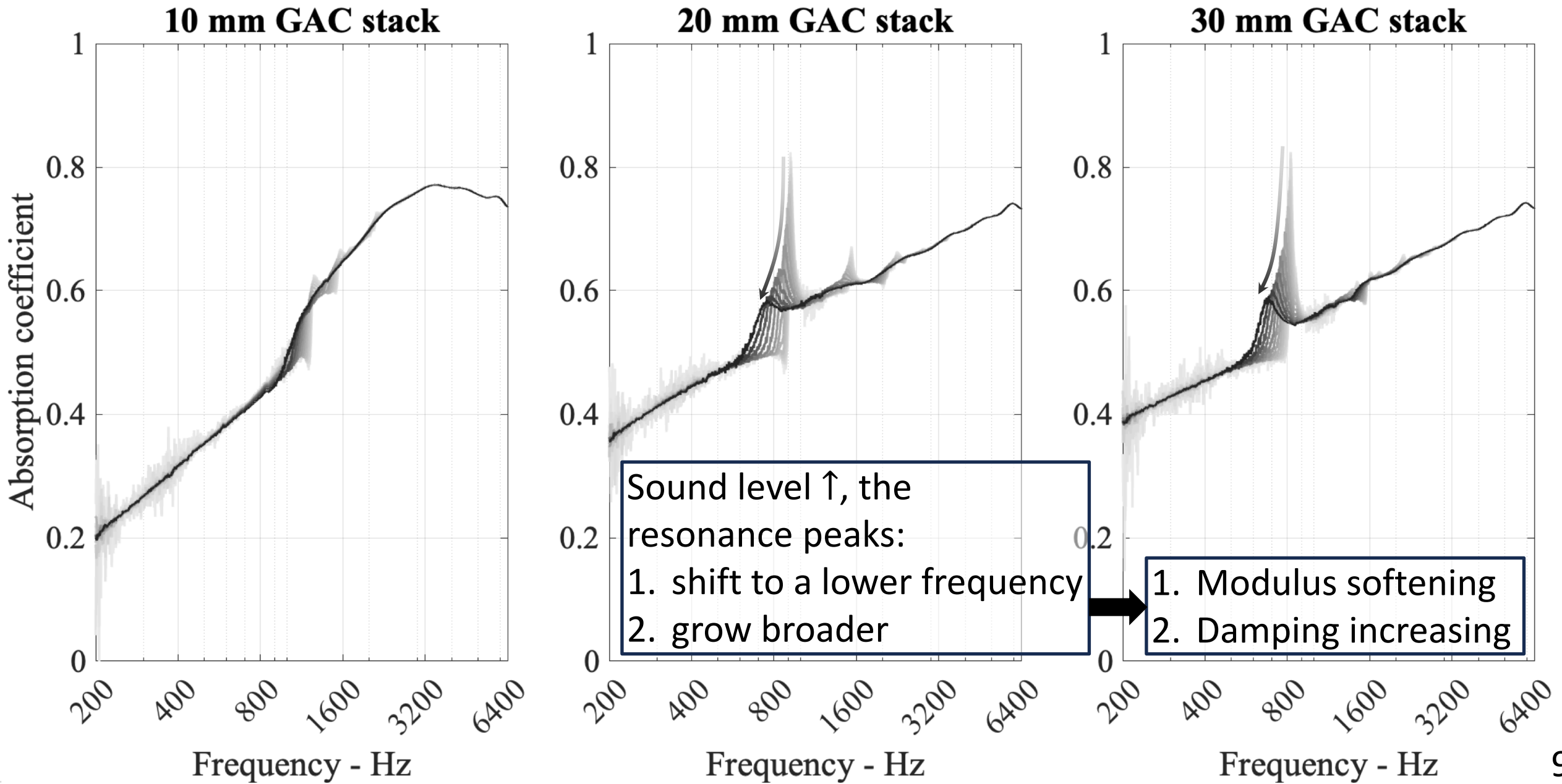


Recap on motivations

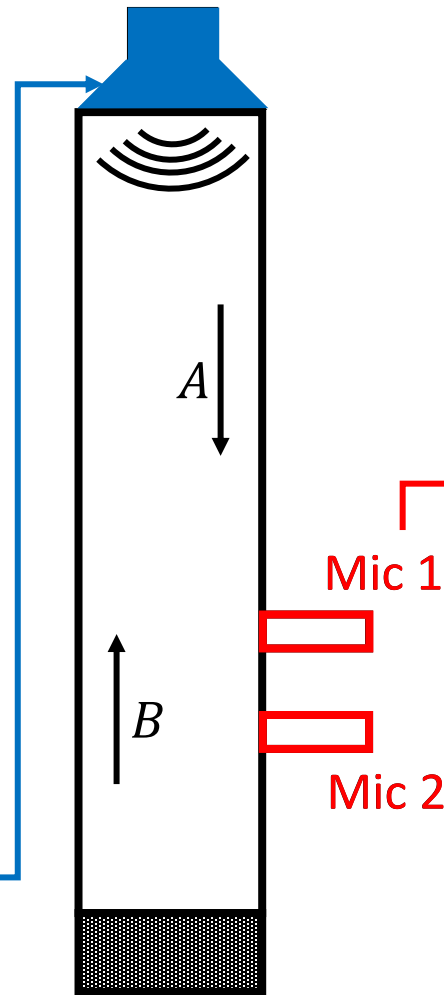
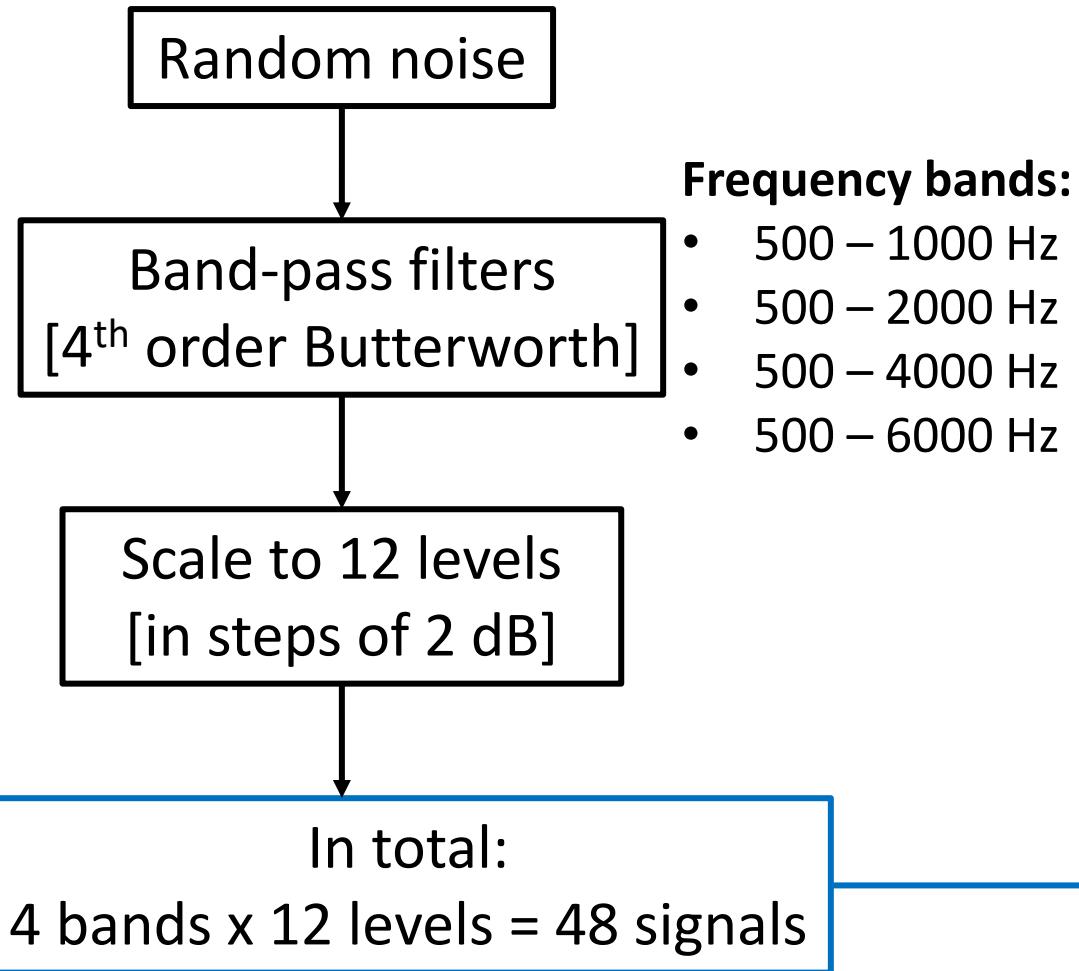


- 2D predictions converge to 1D case when sample diameter increases
- Therefore, can use 1D theory to predict and optimize large area treatments

Level-dependent absorption spectral – Type A GAC stacks



Level-dependent test setup



For each signal:

- Measure material acoustical properties following the ASTM E1050 standard
- Calculate three metrics related to the acoustic field at the surface of the particle stack
- Investigate the particle stack's change of acoustic properties when exposed to different signals

Varying level &
bandwidth

Level metrics – Integrated RMS fluid pressure, velocity, displacement

Complex pressure at Mic 1 & 2, $P_1(f)$ and $P_2(f)$

Complex fluid pressure, velocity, displacement at the of **front surface of the material:**

- $P_0 = F_{P_0}(P_1, P_2)$
- $v_0 = F_{v_0}(P_1, P_2)$
- $u_0 = F_{u_0}(P_1, P_2)$

Power spectrum of P_0, v_0, u_0 at the of **front surface of the material:**

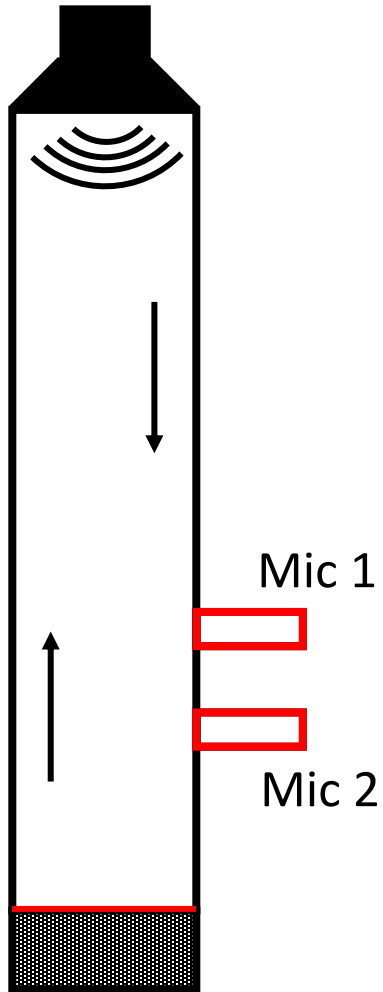
$$S_{P_0P_0} = G_{P_0}(S_{P_1P_1}, S_{P_2P_2}, S_{P_1P_2})$$

$$S_{v_0v_0} = G_{v_0}(S_{P_1P_1}, S_{P_2P_2}, S_{P_1P_2})$$

$$S_{u_0u_0} = G_{u_0}(S_{P_1P_1}, S_{P_2P_2}, S_{P_1P_2})$$

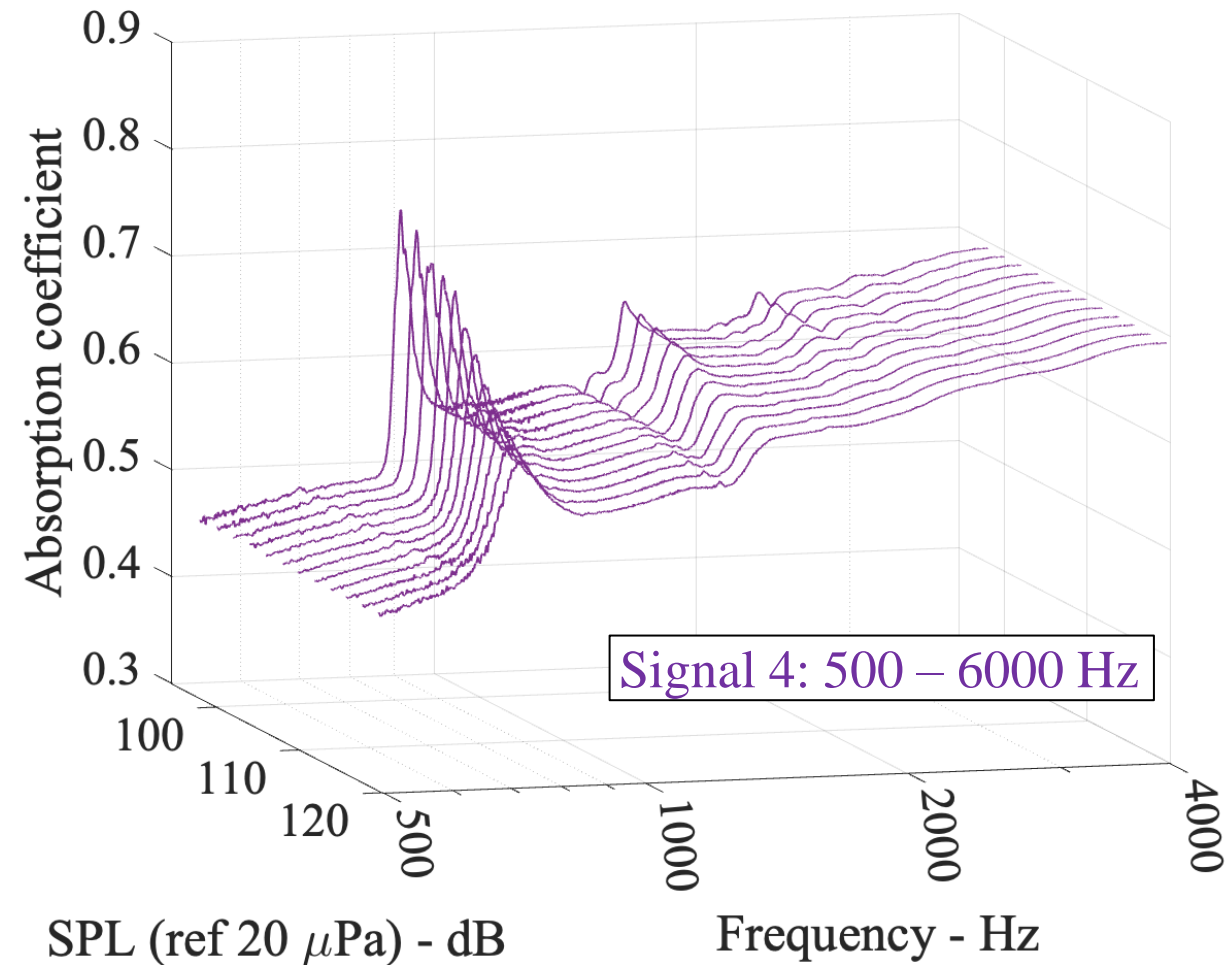
Integrate over frequency:

- $(P_0)_{rms}^2 = \int S_{P_0P_0}(f)df \rightarrow SPL$
- $(v_0)_{rms}^2 = \int S_{v_0v_0}(f)df \rightarrow \text{Integrated RMS fluid velocity}$
- $(u_0)_{rms}^2 = \int S_{u_0u_0}(f)df \rightarrow \text{Integrated RMS fluid displacement}$

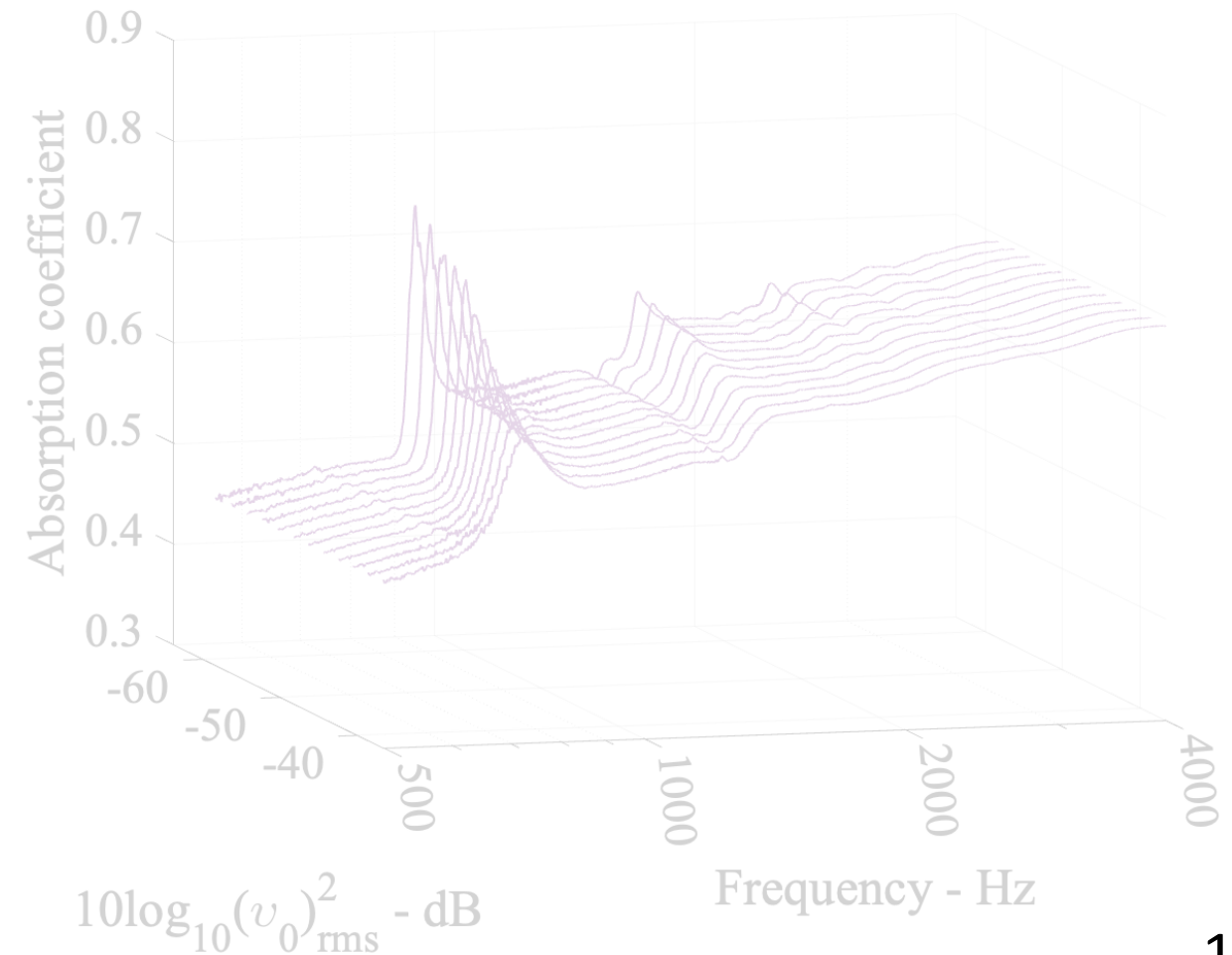


Test results: 40 mm Type A GAC stack

Sound pressure level



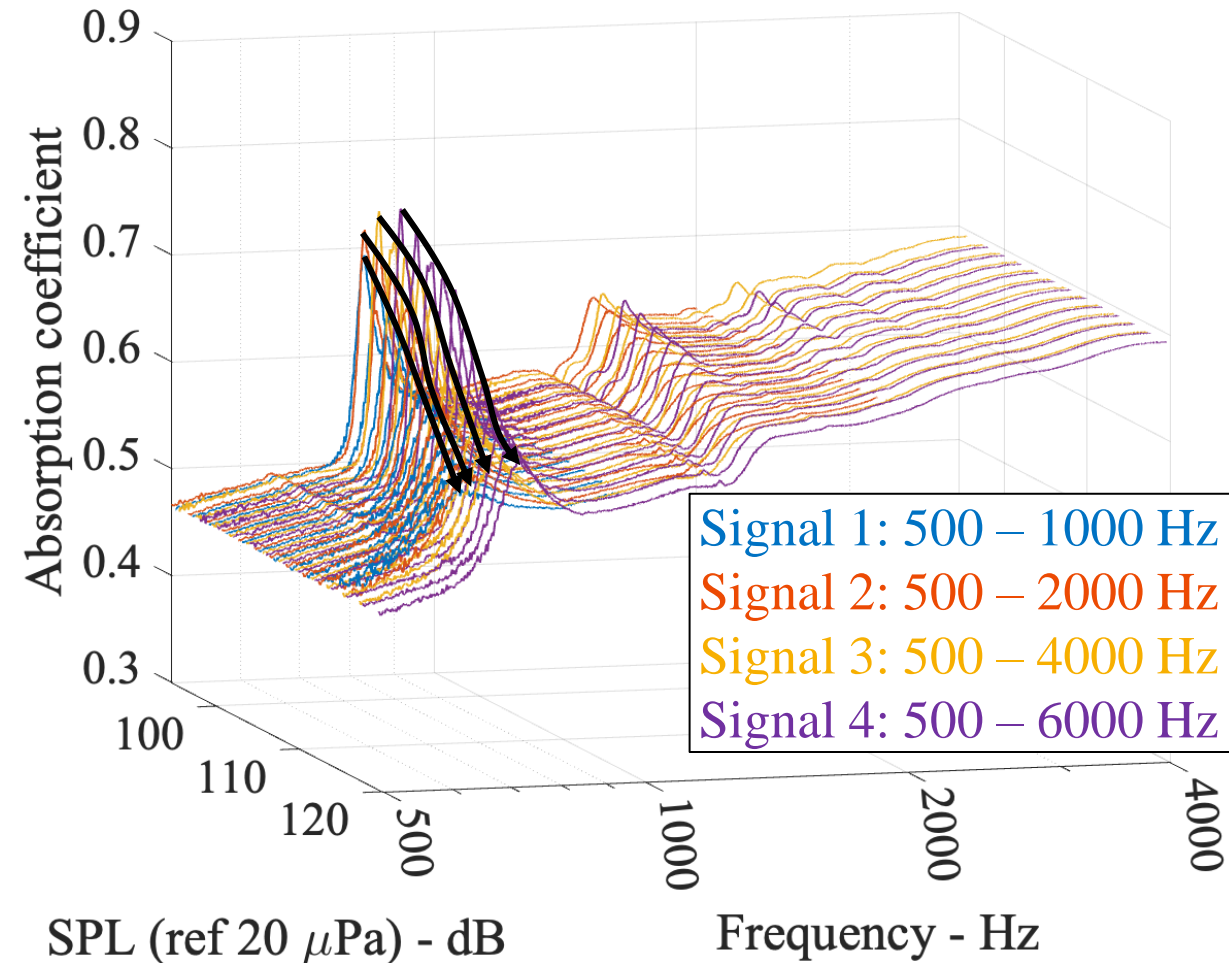
Integrated fluid RMS velocity



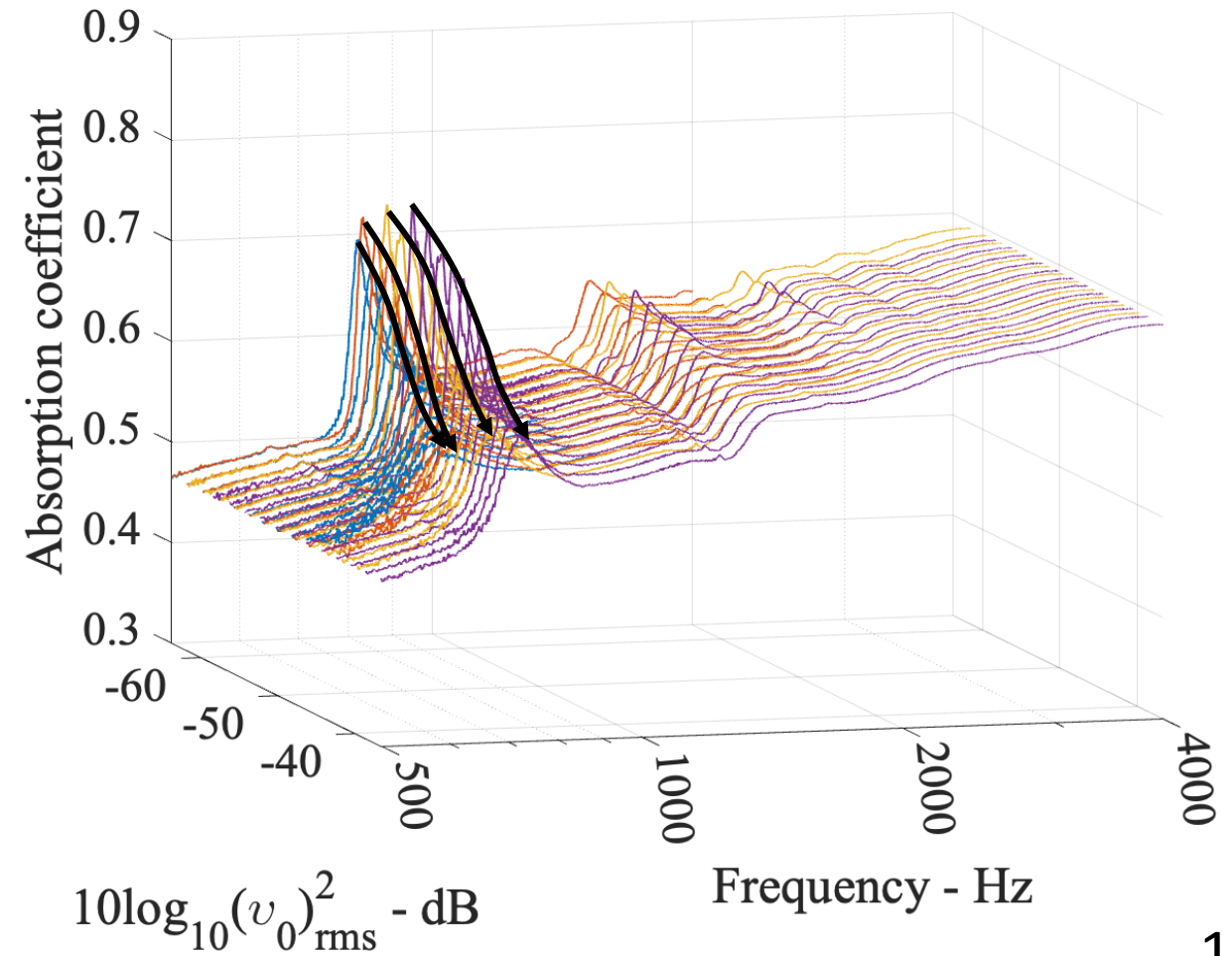
Test results: 40 mm Type A GAC stack

- Peak behavior does not scale with sound pressure level or integrated RMS velocity

Sound pressure level

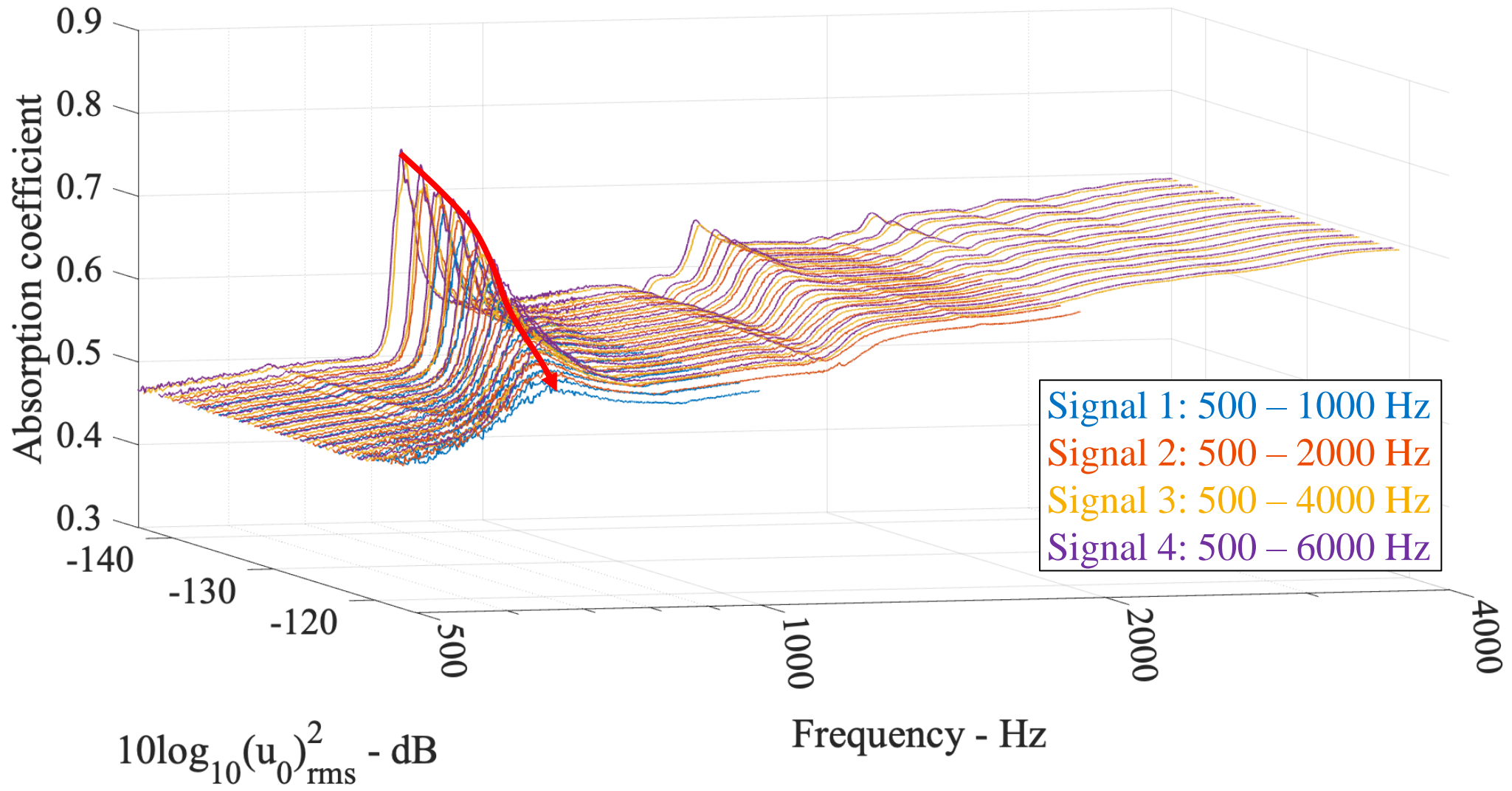


Integrated fluid RMS velocity

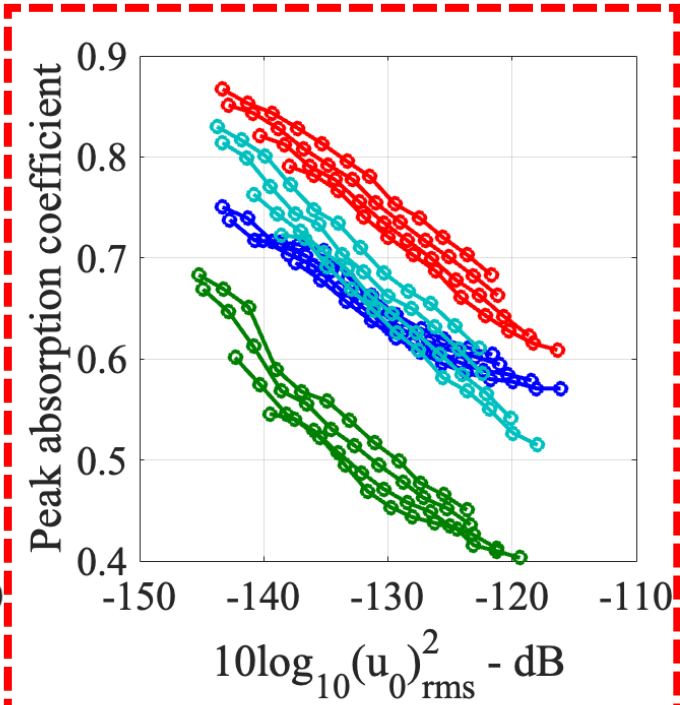
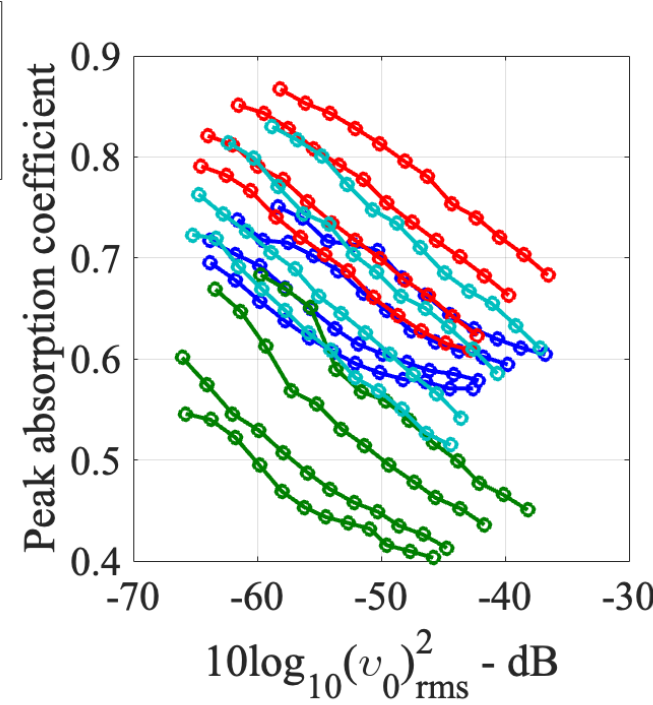
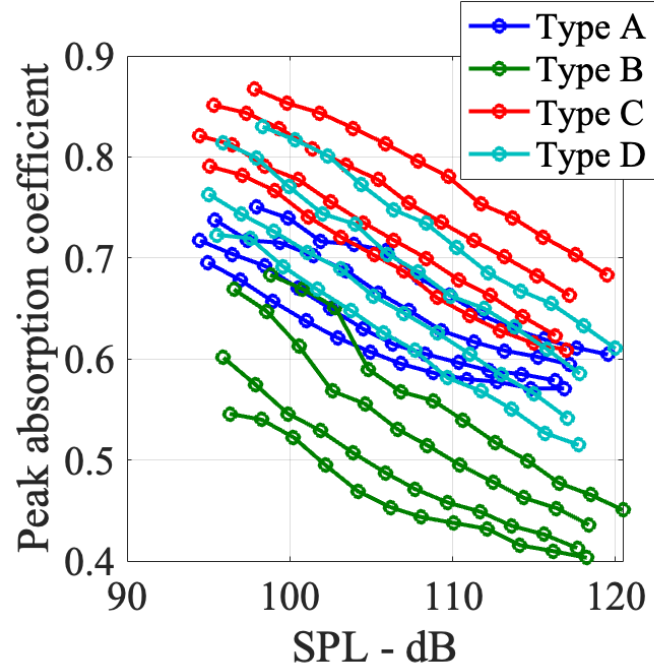


Test results: 40 mm Type A GAC stack

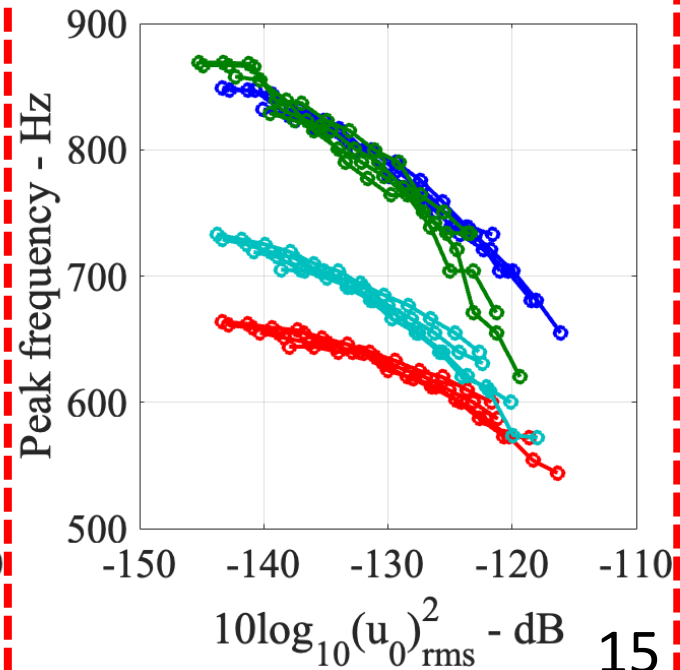
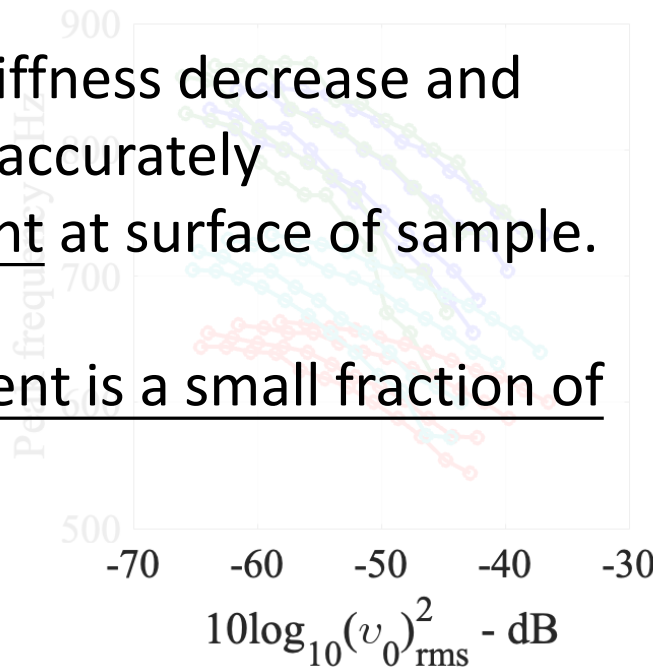
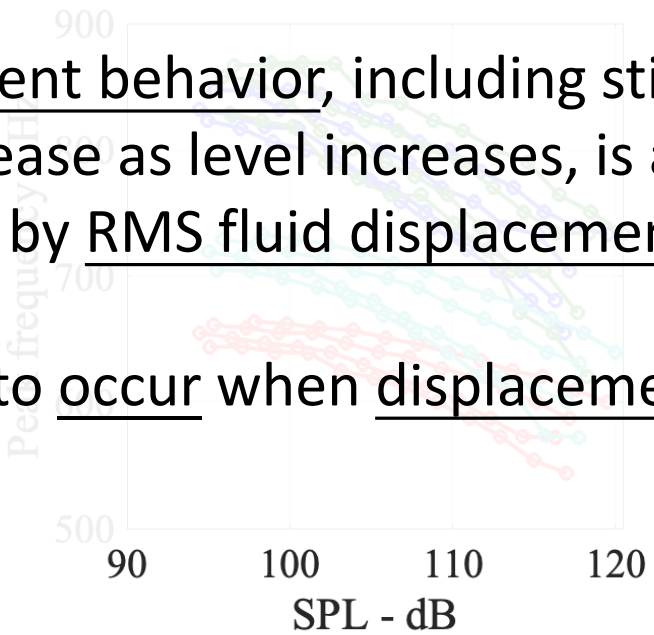
- All the peaks collapse to one single line when plotting against integrated RMS fluid displacement at surface of particle stack, independent of signal bandwidth



Test results: 40 mm Type A-D GAC stacks



- Level-dependent behavior, including stiffness decrease and damping increase as level increases, is accurately characterized by RMS fluid displacement at surface of sample.
- Effect begins to occur when displacement is a small fraction of particle size.



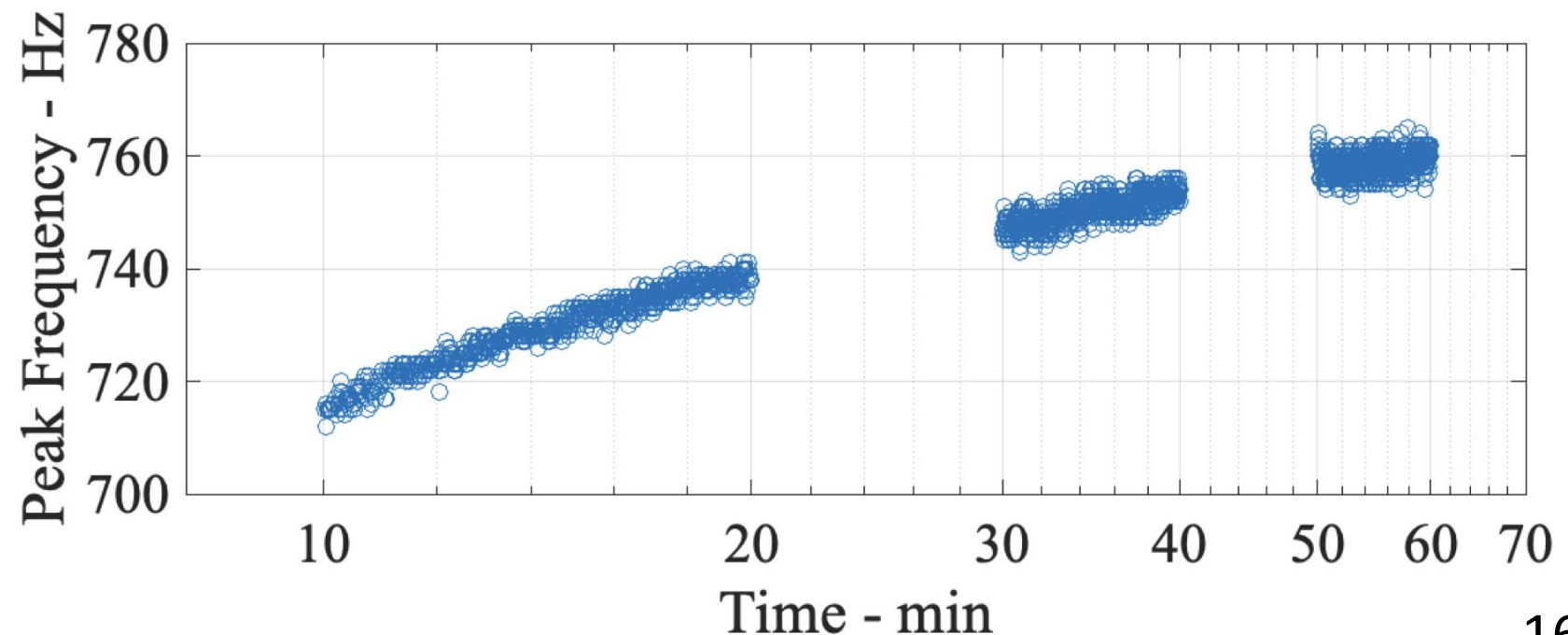
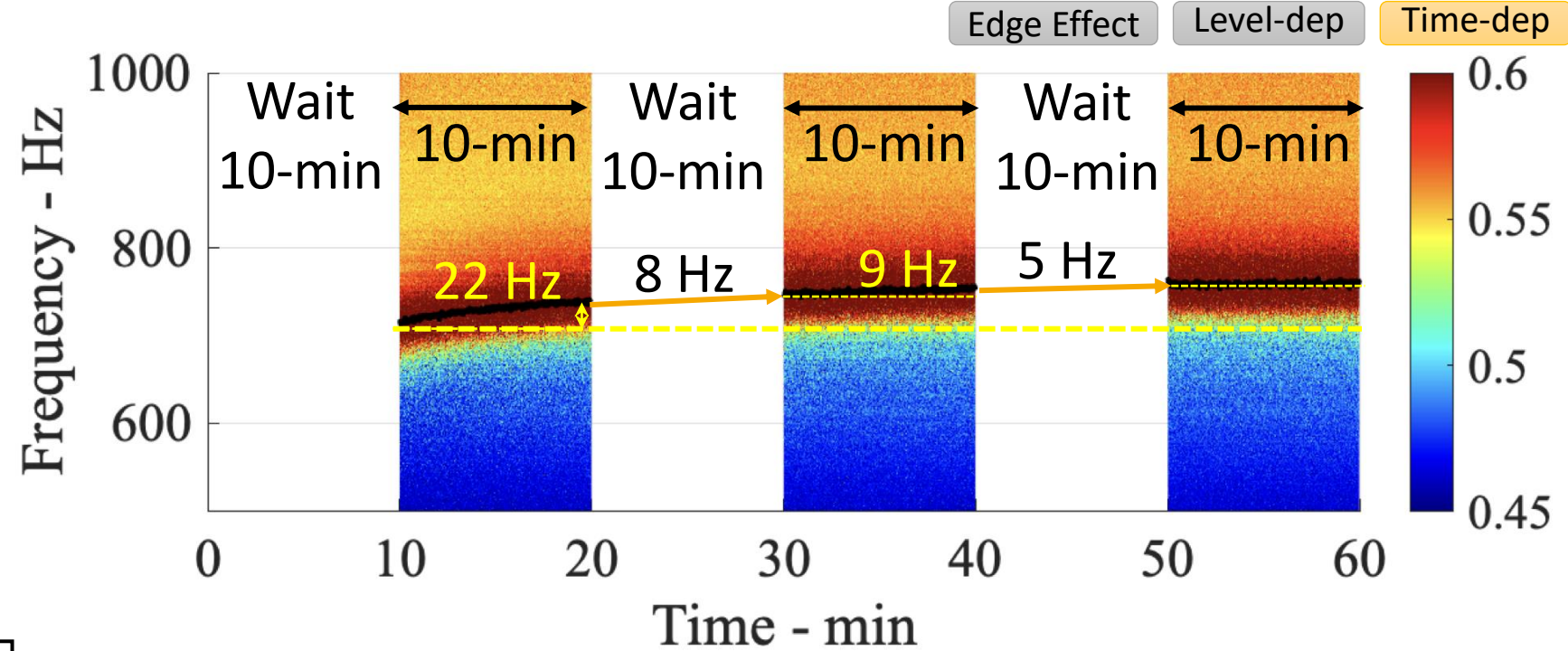
Time-dependent: 40 mm Type A GAC

Procedure:

Load the sample

1. Wait 10-min → 10-min noise
2. Wait 10-min → 10-min noise
3. Wait 10-min → 10-min noise

- Particle stack gradually consolidates over minutes and hours whether or not exposed to sound field.
- Increase in peak frequency indicates stiffening of material.

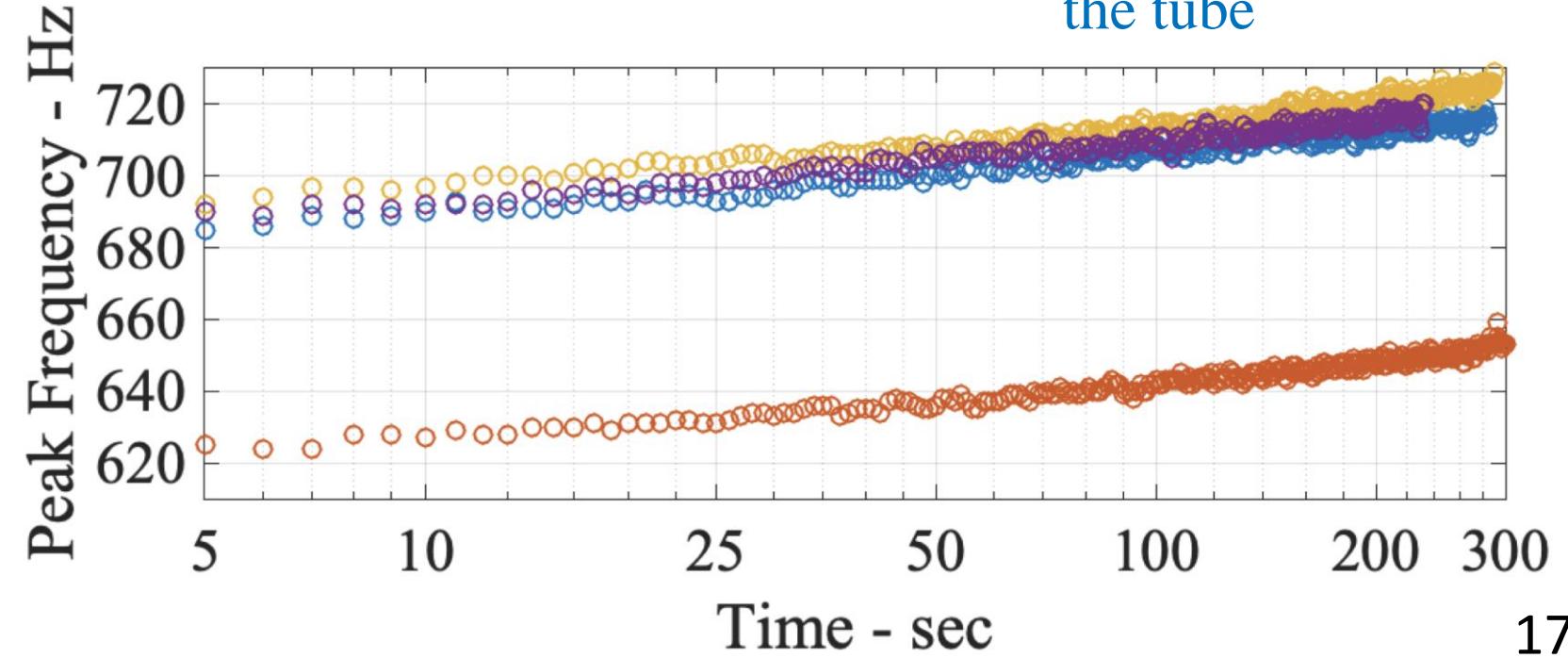
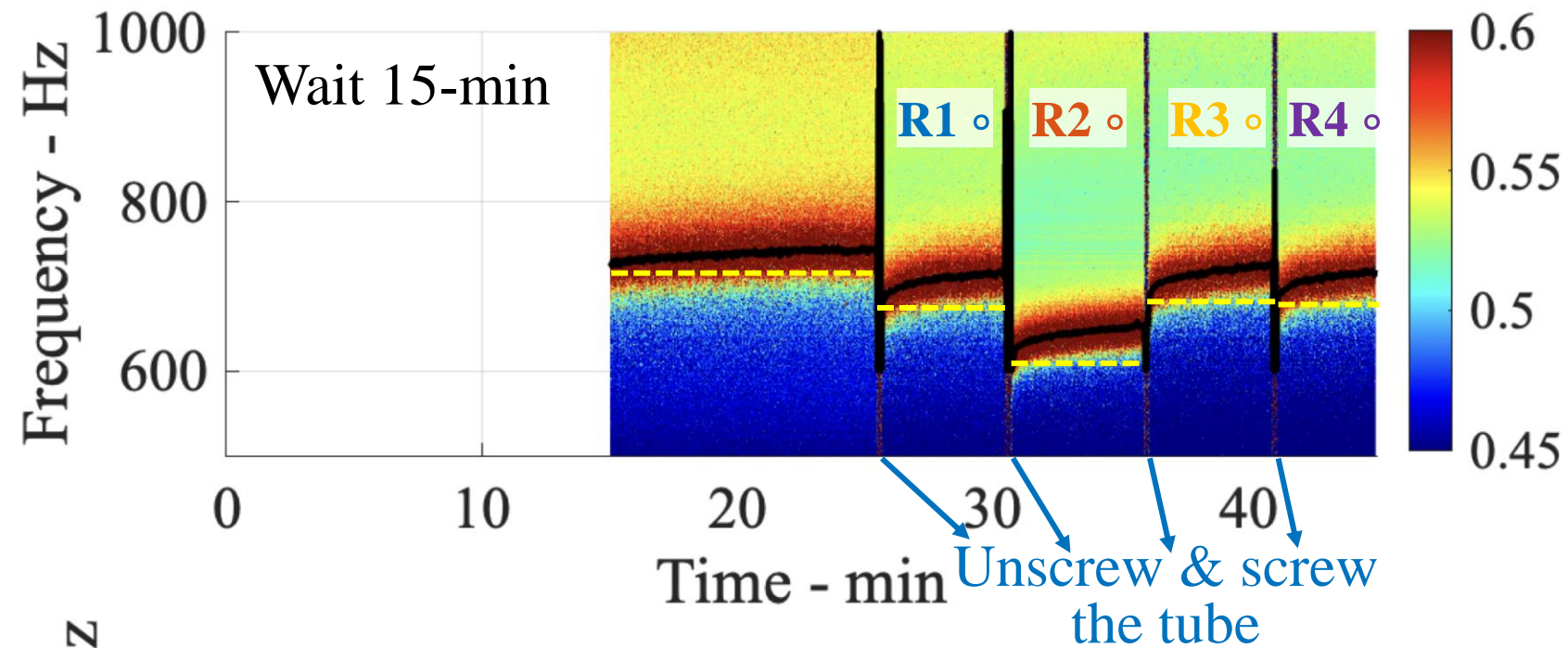


Time-dependent: 40 mm Type A GAC

Procedure:

- Load the sample
- 1. Wait 15-min
- 2. 30-min white noise
- Vibrate sample 4 times

- This is an example of “slow dynamics”
- Properties changes as a linear function of $\log(\text{Time})$



Conclusions

- The circumferential edge-constraint has shown a significant impact on the acoustical behavior of granular particle stacks when the stack depth is comparable to or larger than the sample holder size.
- For granular particle stacks: as the input sound level goes up, the resonance peaks: 1. shift to a lower frequency (i.e., modulus softening); 2. grow broader (i.e., increasing damping)
The level-dependent modulus and damping of granular material can be characterized with a strain-related metric: i.e., the total RMS fluid displacement at the stack surface.
- It has been found that some granular materials will consolidate over time, resulting in an increase in modulus, and the change of properties is linearly related with the logarithm of time. Such time-varying properties can be “initialized” by vibrating or disturbing the particle stack. This is an example of “slow dynamics”.

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Thanks