

**SEMPAE** 

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 **utc** Recherche  
Roberval

# Nonlinear and time-dependent behaviour of compressed melamine foam: application to pyramidal asperities in a surface roughness model

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1: Université de technologie de Compiègne,  
Laboratoire Roberval, 60203 Compiègne

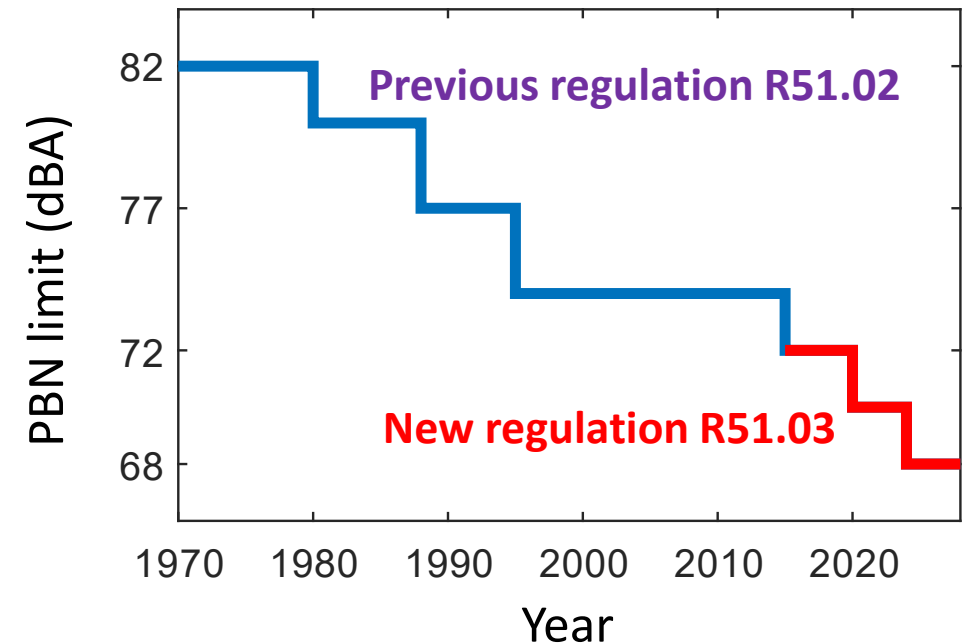
2: Laboratoire Quartz (EA-7393), ISAE-Supméca,  
93400 Saint-Ouen-sur-Seine

07/11/2023

# Porous acoustic screens with partial contact

Road noise is big source of complaints

European regulation is lowering pass-by noise limit



# Porous acoustic screens with partial contact

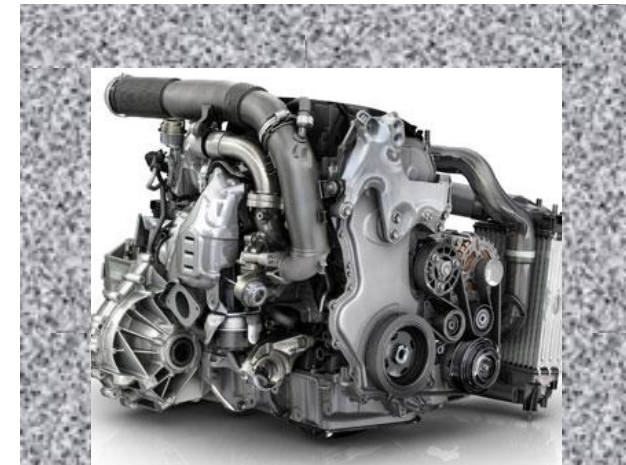
Completed project: EcOBEx (2014-2017)



# Porous acoustic screens with partial contact

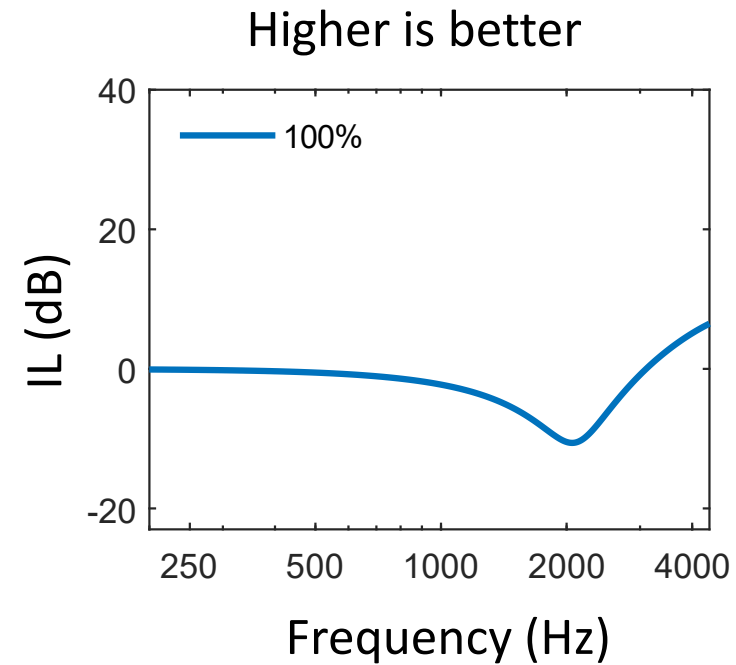
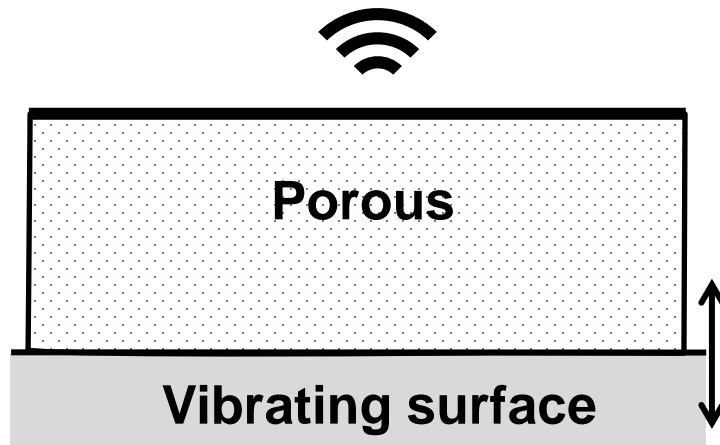
Completed project: EcOBEx (2014-2017)

Current project: SEMPAAE (2020-2023)



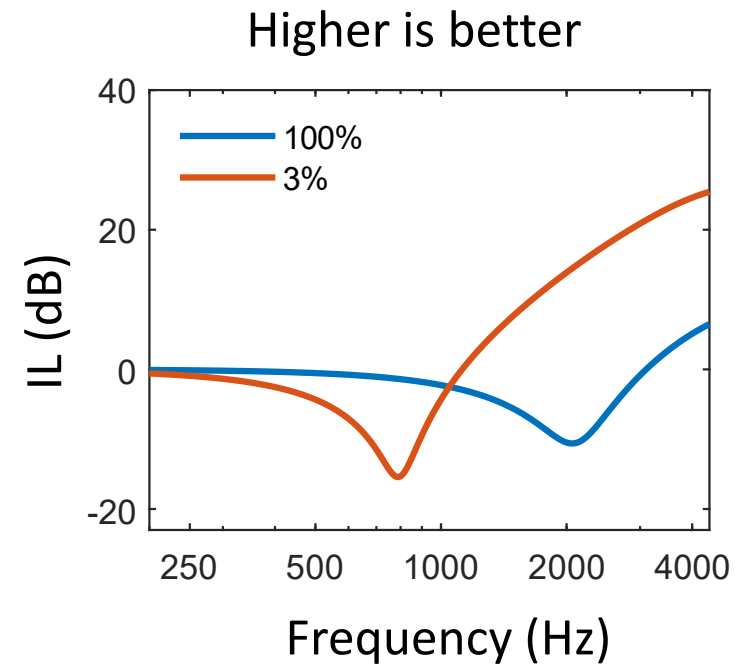
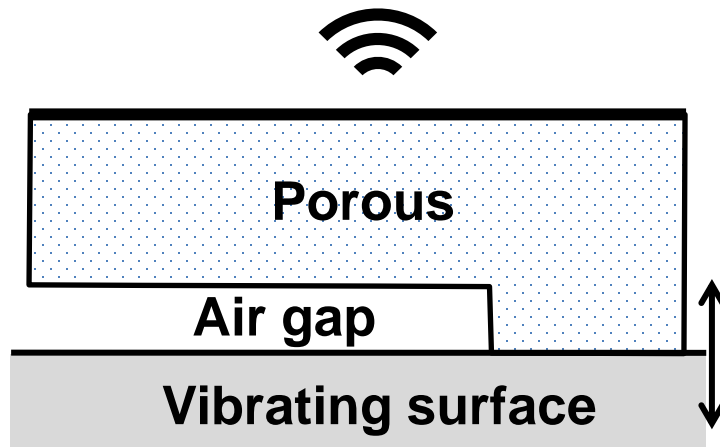
# Porous acoustic screens with partial contact

Strong effect of screen mechanical properties  
Partial contact yields better decoupling



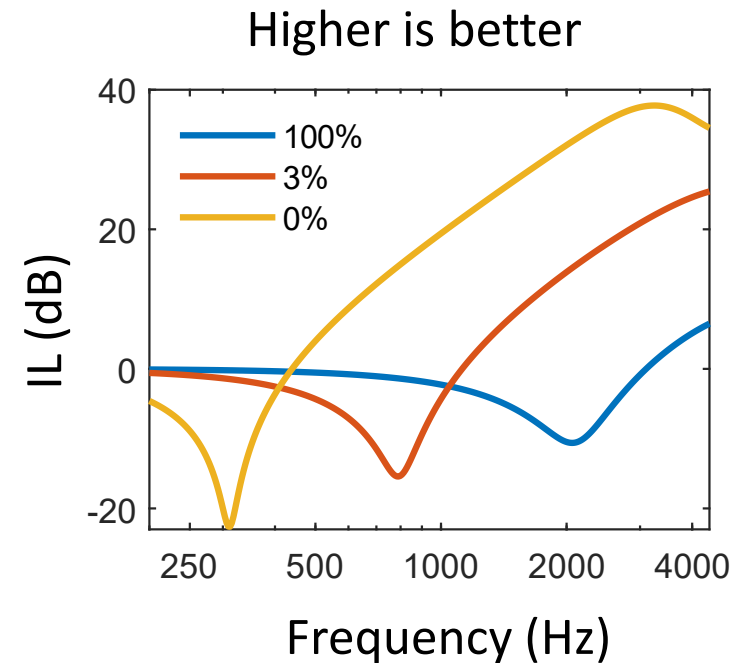
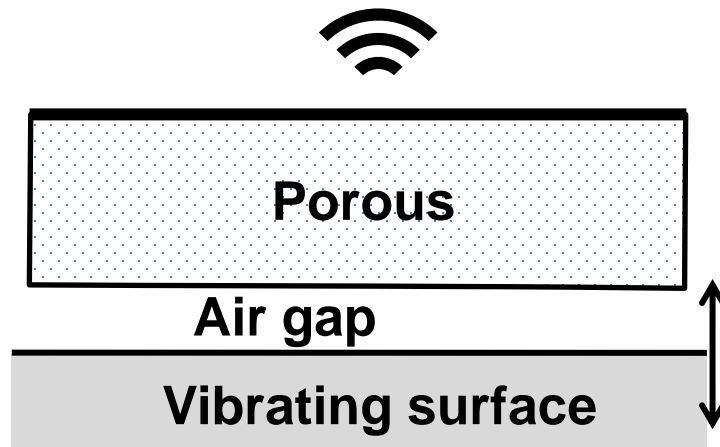
# Porous acoustic screens with partial contact

Strong effect of screen mechanical properties  
Partial contact yields better decoupling  
Modelled with PTMM (Verdière, 2013)



# Porous acoustic screens with partial contact

Strong effect of screen mechanical properties  
Partial contact yields better decoupling  
Modelled with PTMM (Verdière, 2013)



# Porous acoustic screens with partial contact

## Experimental results of partial contact

Shaker:  
Injected power



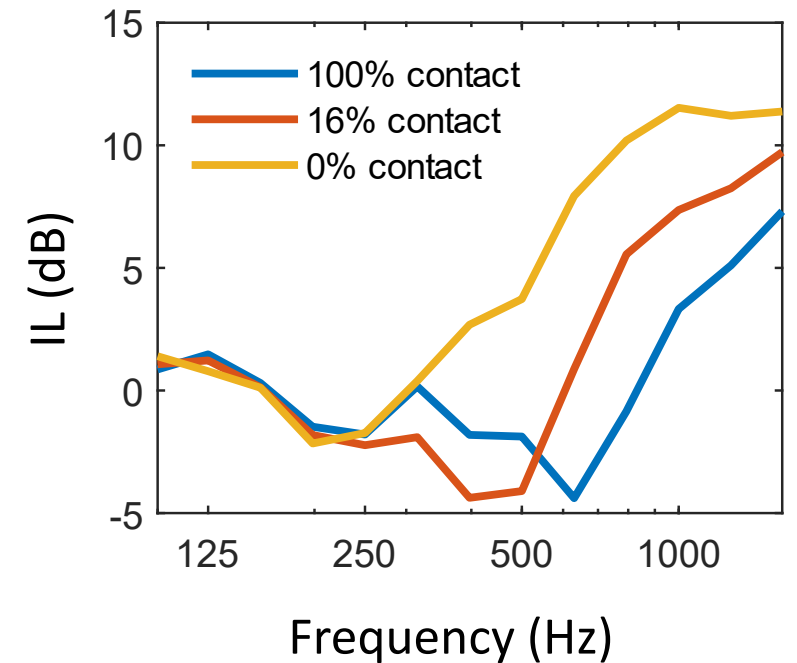
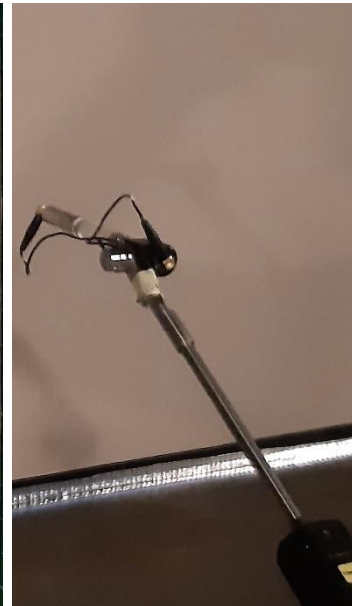
Plate



Porous screen  
+ heavy layer



Intensity probe:  
Radiated power

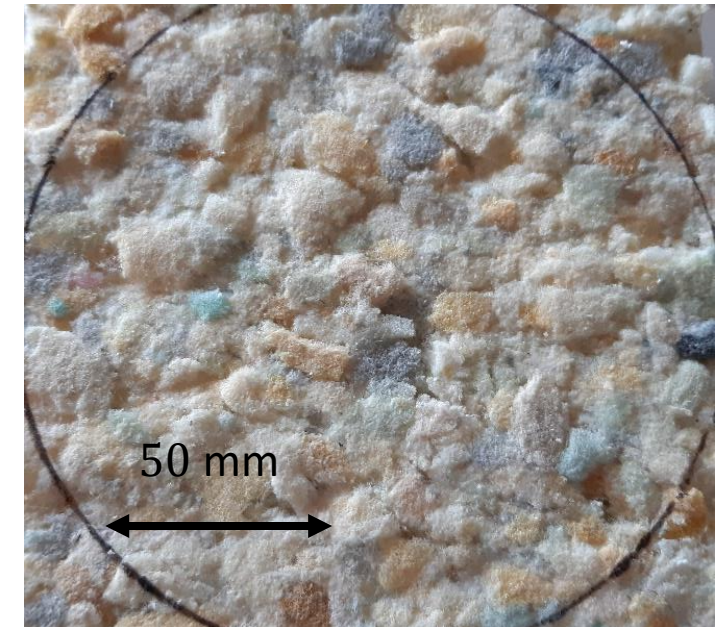
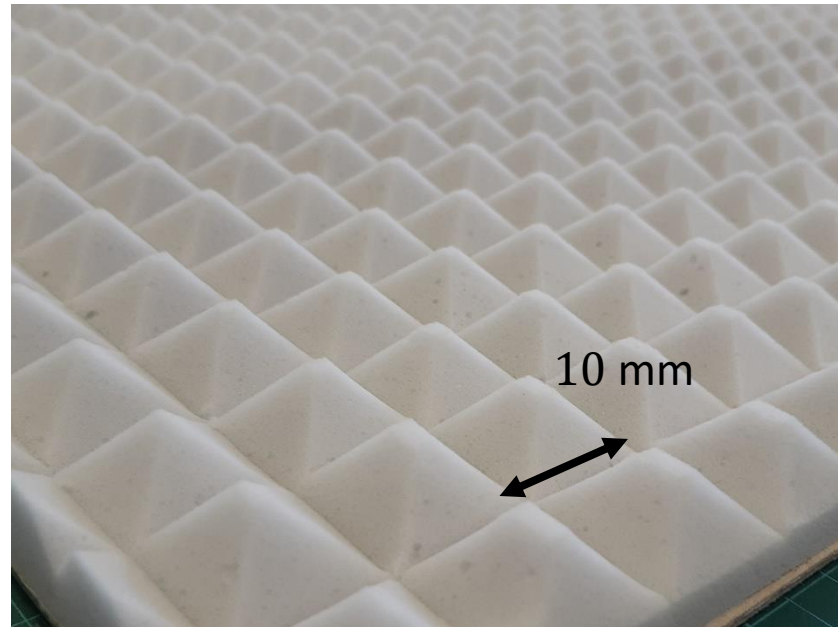




## Porous acoustic screens with partial contact

The contact region between the engine and the porous screen should be modelled

- 1) How much contact when compressed ?
- 2) What is the compression stiffness?



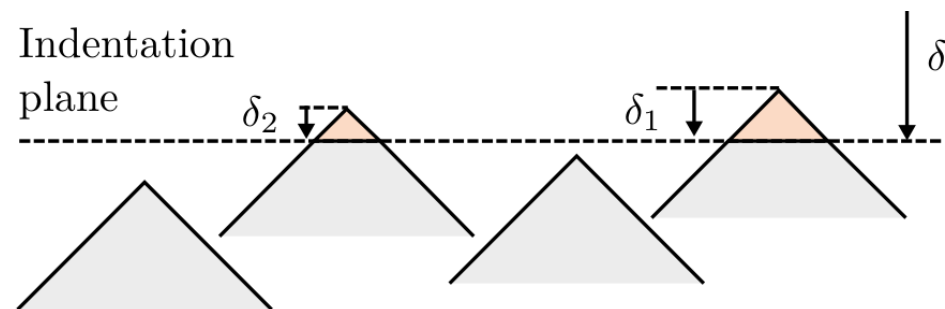
# Porous acoustic screens with partial contact

## Modelling a rough surface



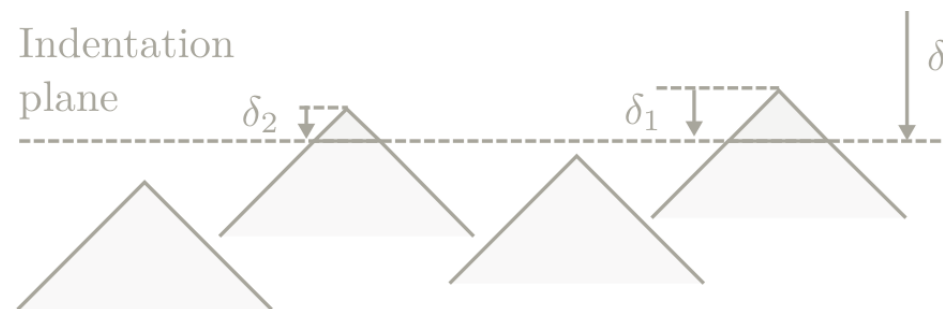
# Porous acoustic screens with partial contact

## Modelling a rough surface



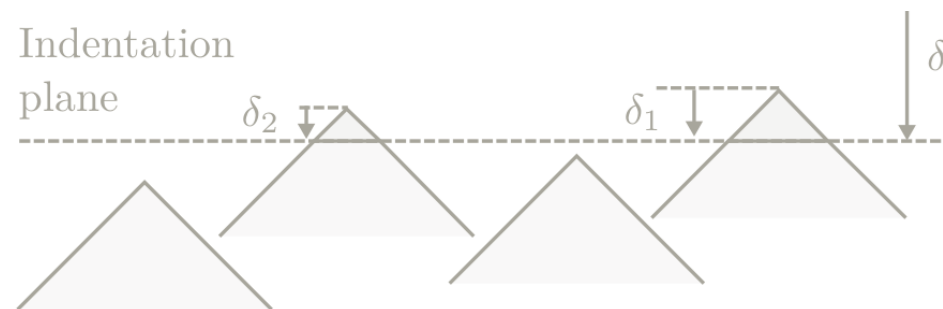
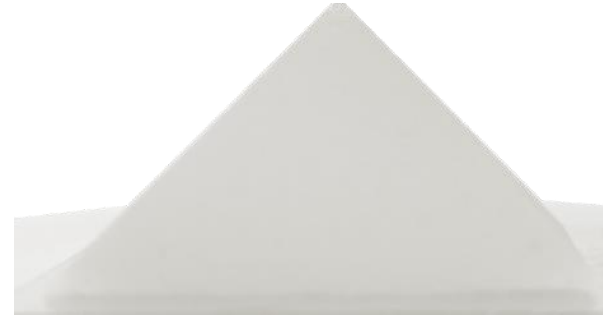
# Porous acoustic screens with partial contact

## Modelling a rough surface



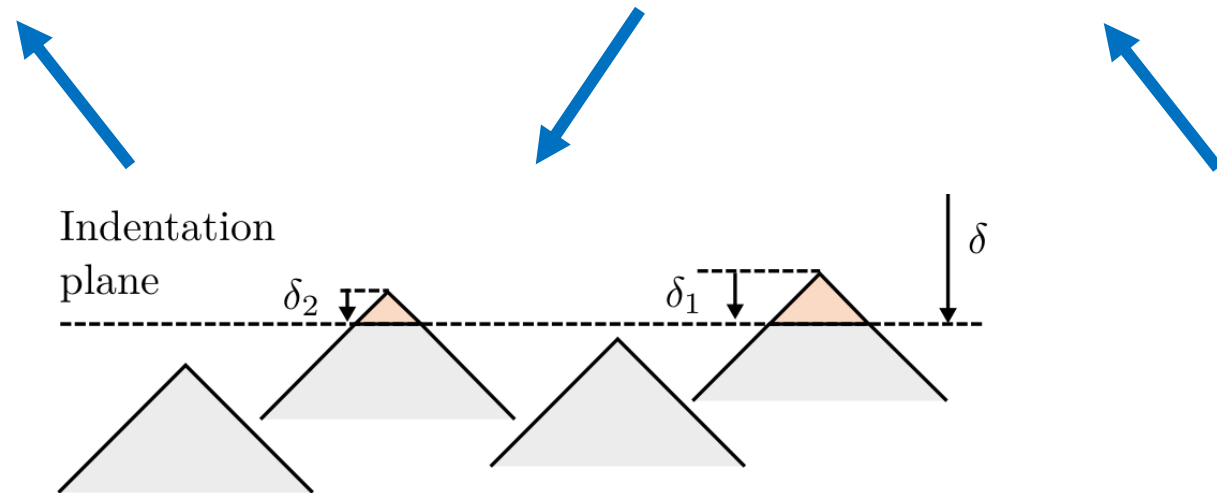
# Porous acoustic screens with partial contact

## Modelling a rough surface



# Porous acoustic screens with partial contact

## Modelling a rough surface



# Plan

- 1) Intrinsic material behaviour
- 2) Pyramid compression

## Modelling material behaviour: nonlinearity

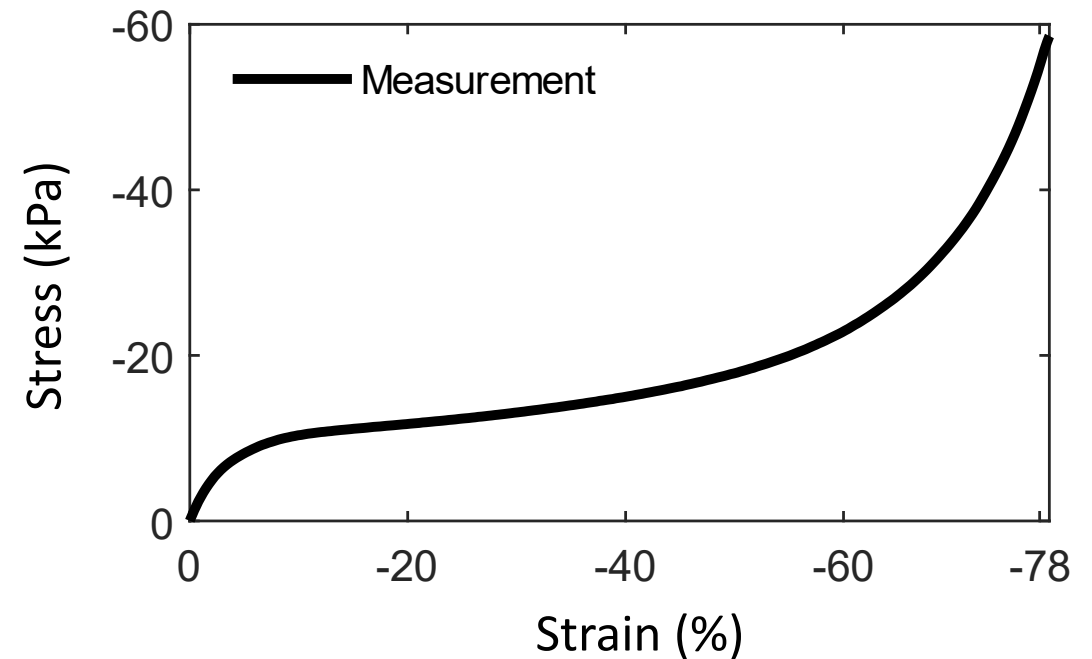
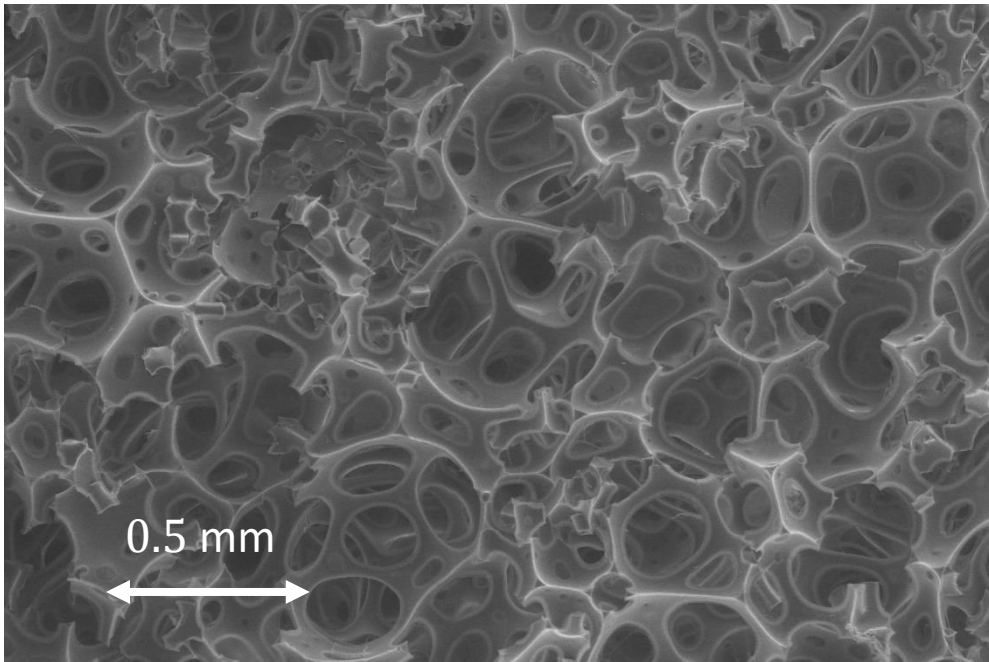
Porous microstructural material  
Known to behave non linearly  
Modelled with a hyperelastic model





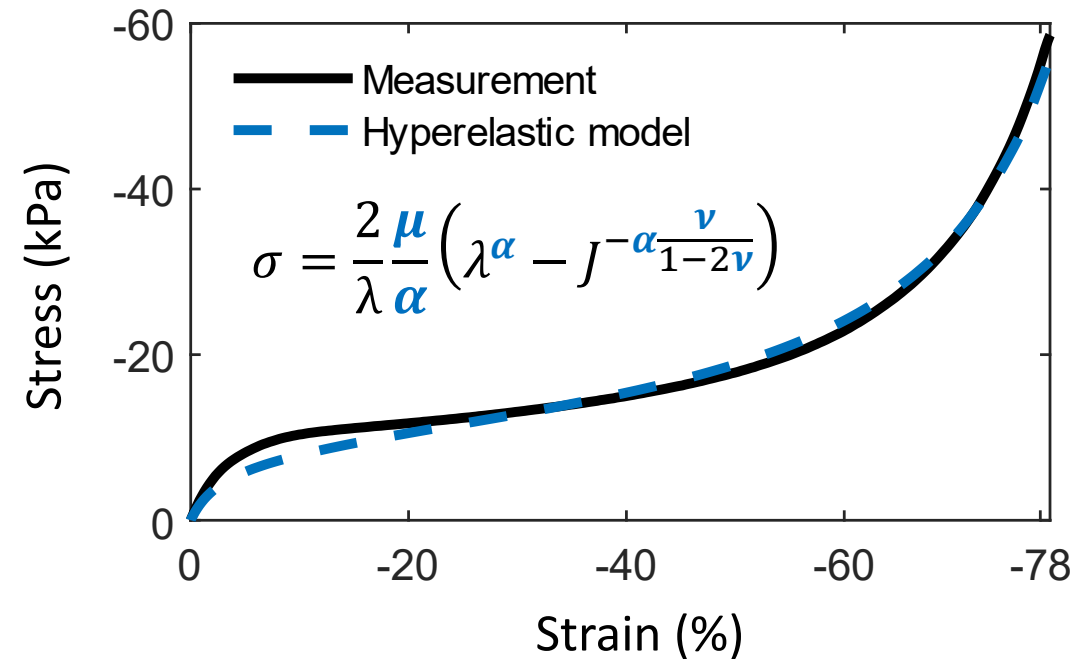
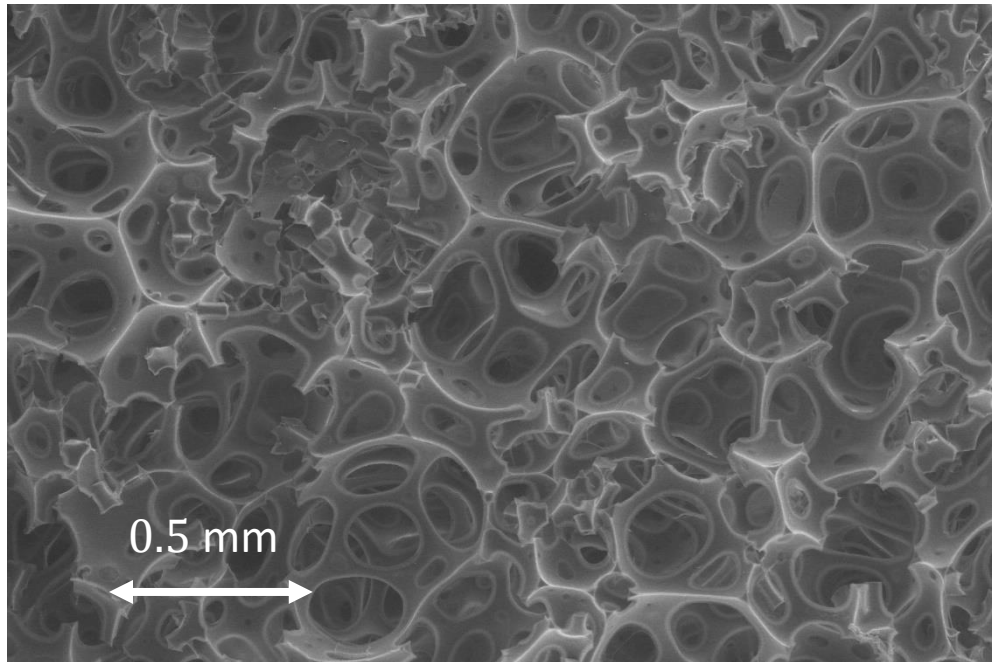
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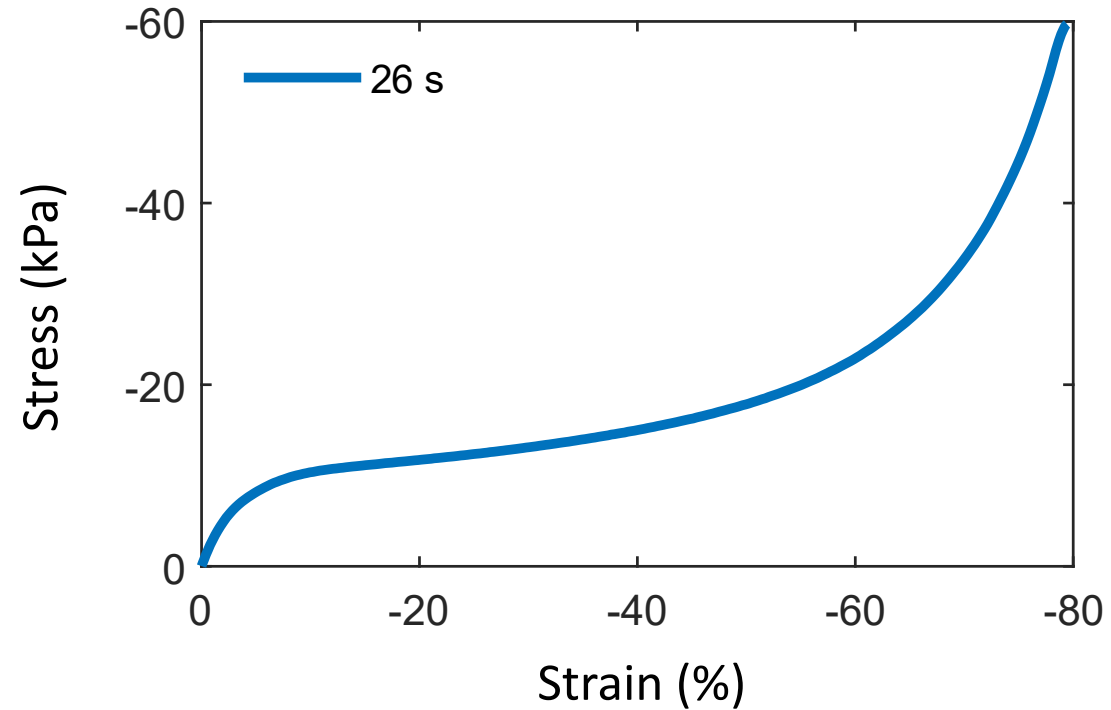
# Modelling material behaviour: nonlinearity

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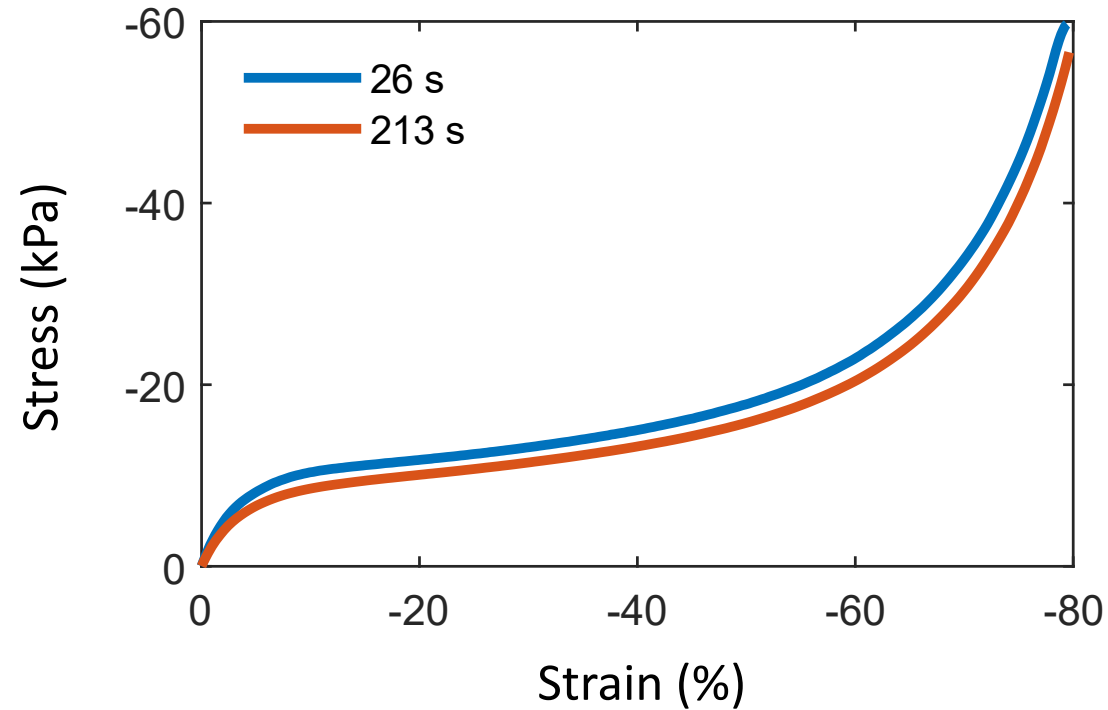
# Modelling material behaviour: relaxation

Time-dependence of measurements due to relaxation  
Can the instant response be obtained?



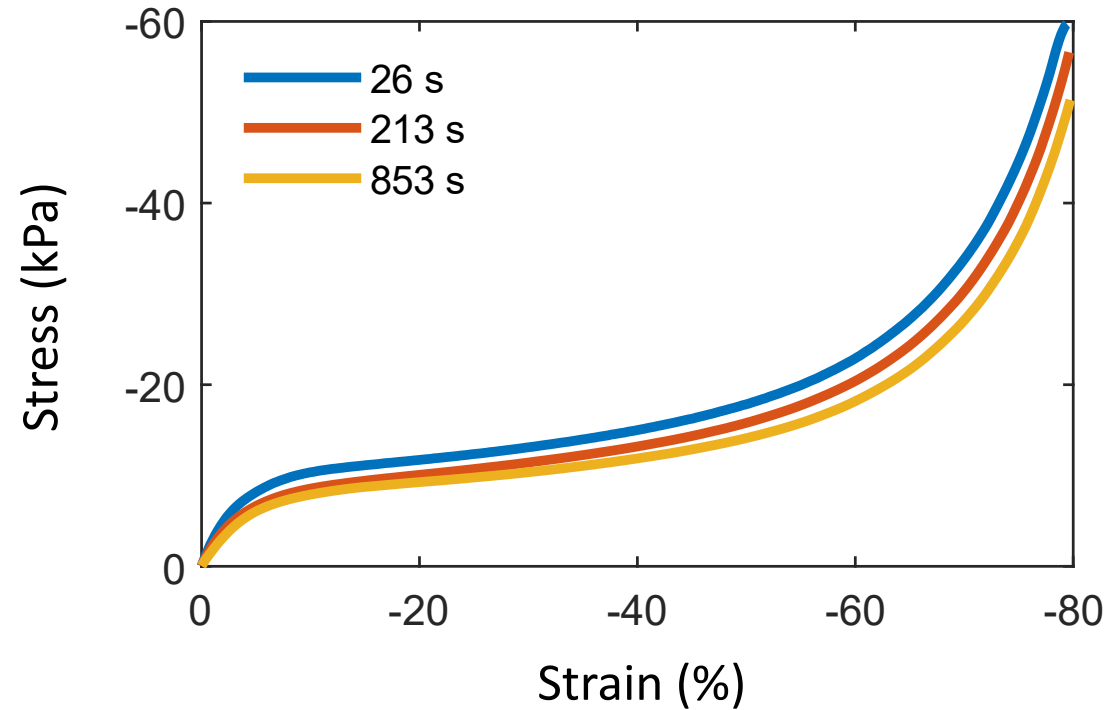
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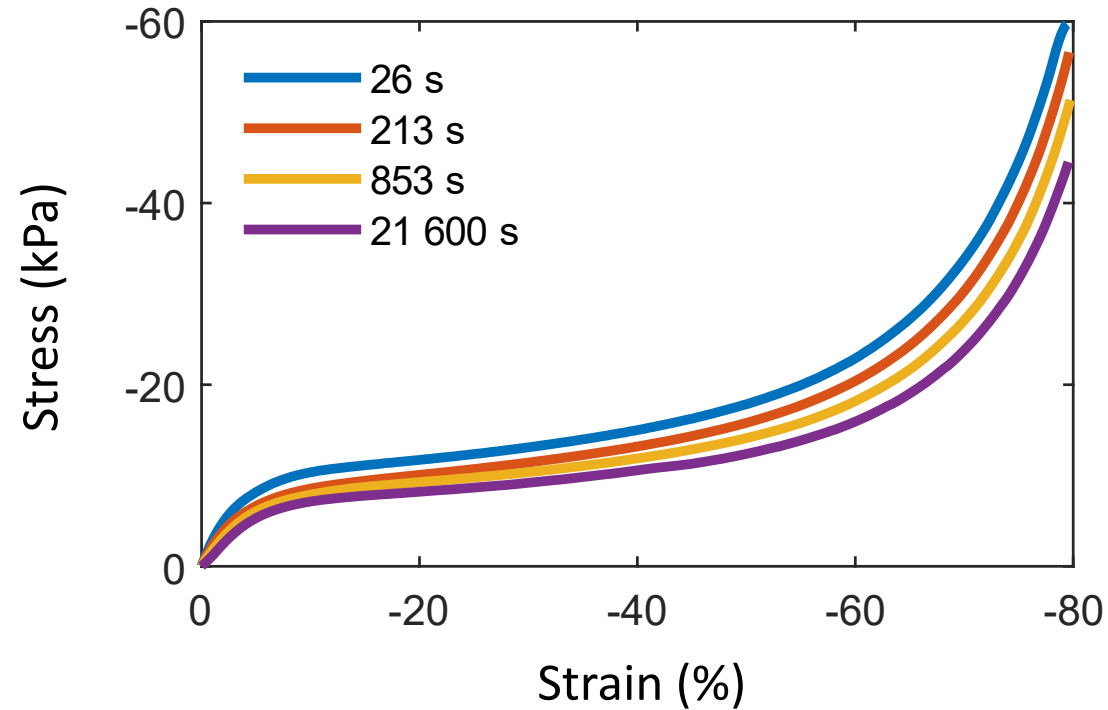
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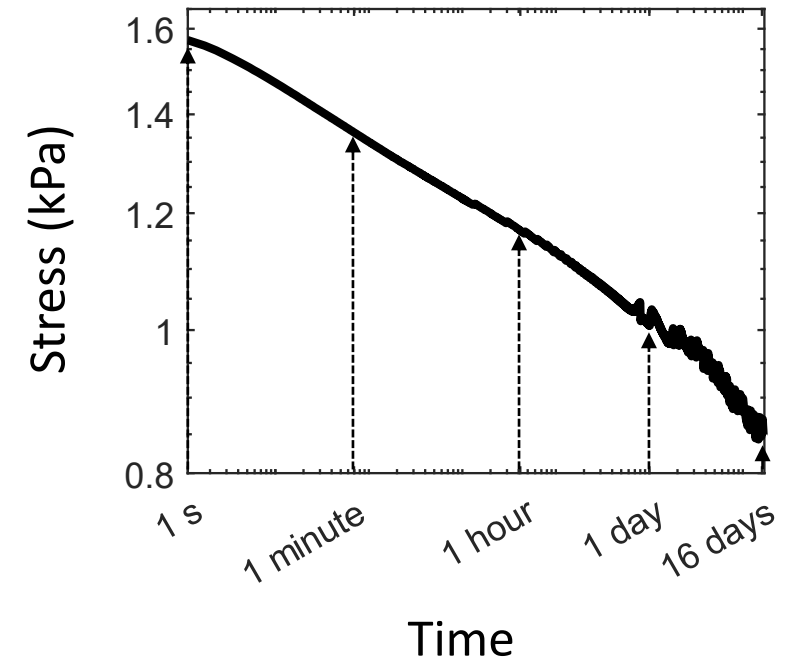
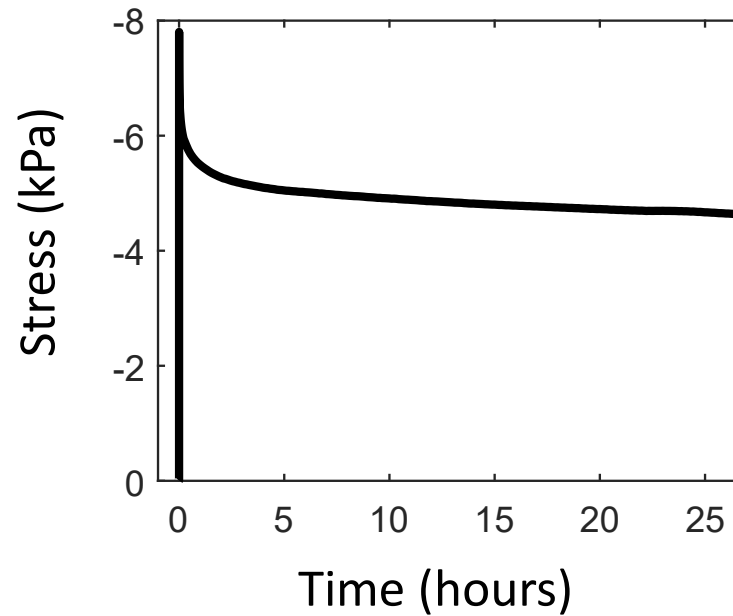
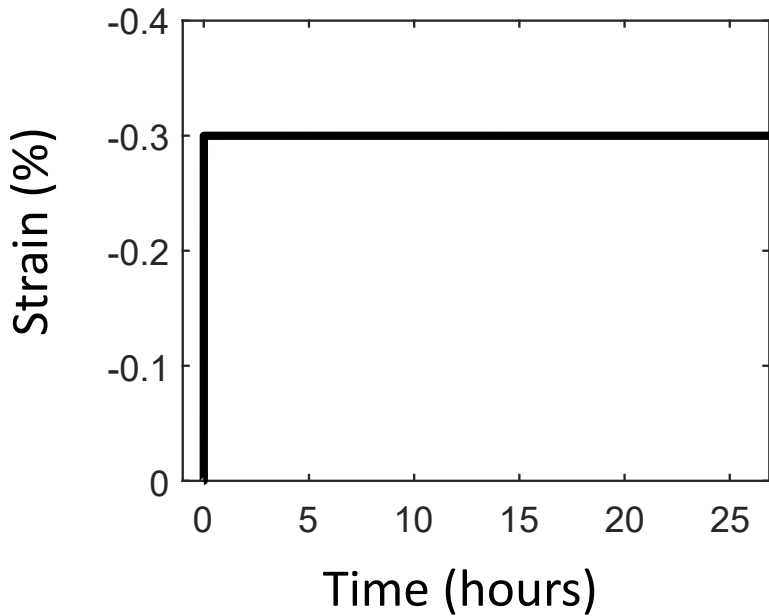
# Modelling material behaviour: relaxation

Time-dependence of measurements due to relaxation  
Can the instant response be obtained?



# Modelling material behaviour: relaxation

Over long durations, relaxation leads to large variations  
How can it be modelled?



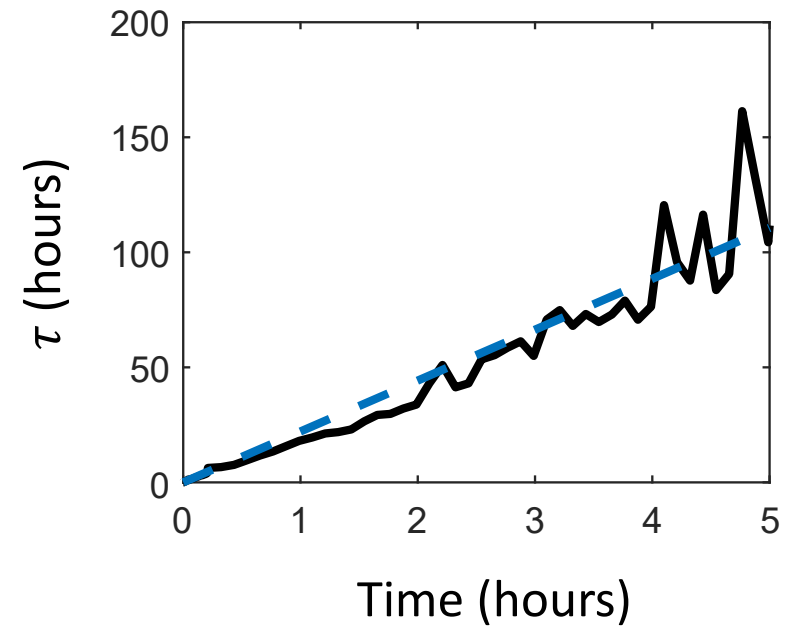
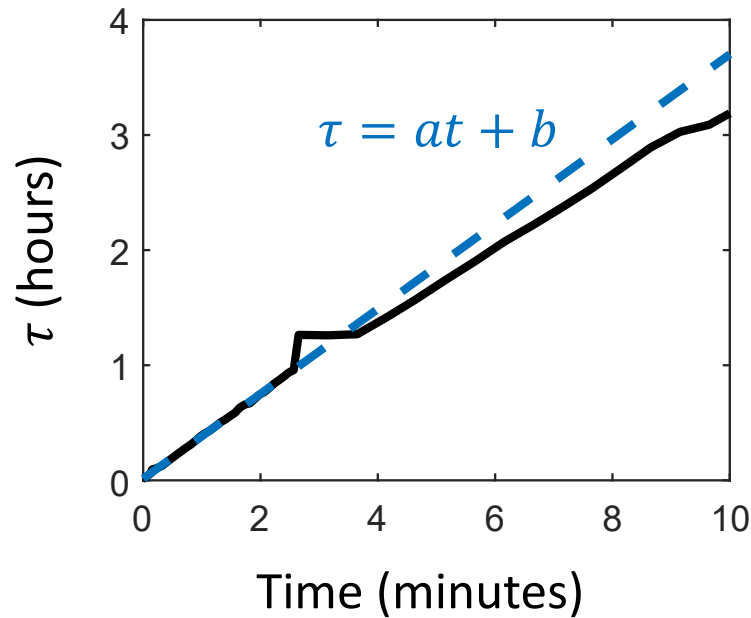
- 5 minutes: 20 % difference
- 24 hours: 40 % difference

# Modelling material behaviour: relaxation

At constant strain, relaxation time  $\tau$  increases linearly with time

Relaxation time :

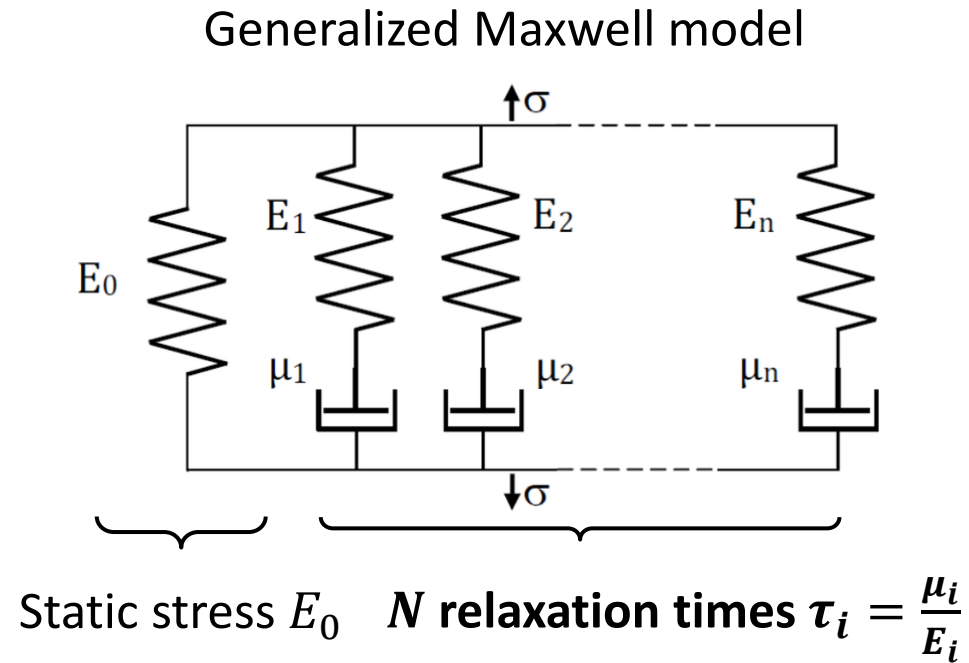
$$\tau = \frac{-F}{\dot{F}}$$





# Modelling material behaviour: relaxation

Different relaxation times could be modelled with generalized Maxwell model



# Modelling material behaviour: relaxation

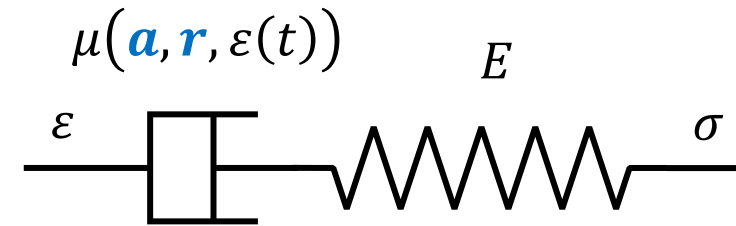
However the behaviour is more reminiscent of an aging phenomenon

$$\begin{cases} \dot{\sigma} = -\frac{1}{\tau} \sigma + E \dot{\varepsilon} \\ \dot{f} = -a f^2 + r \dot{\varepsilon}^2 \end{cases}$$

Aging: when  $\dot{\varepsilon} = 0$ ,  
 $\tau$  increases with slope  $a$

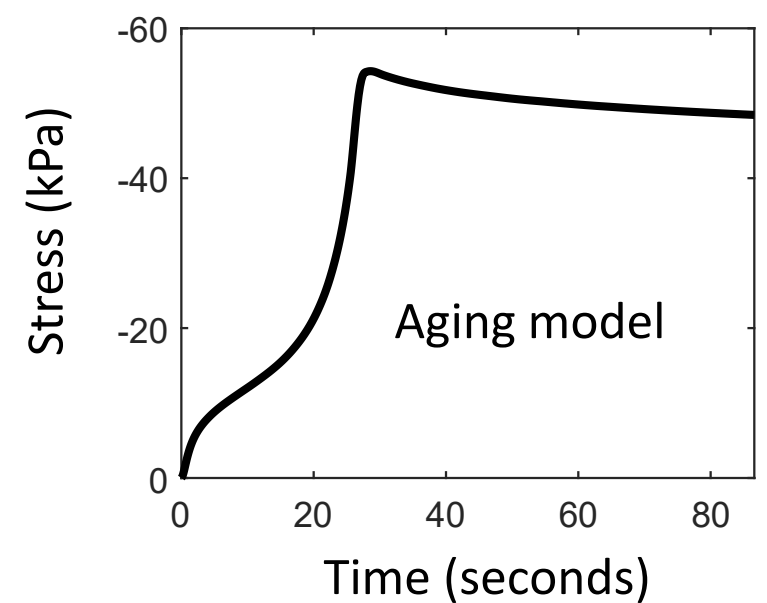
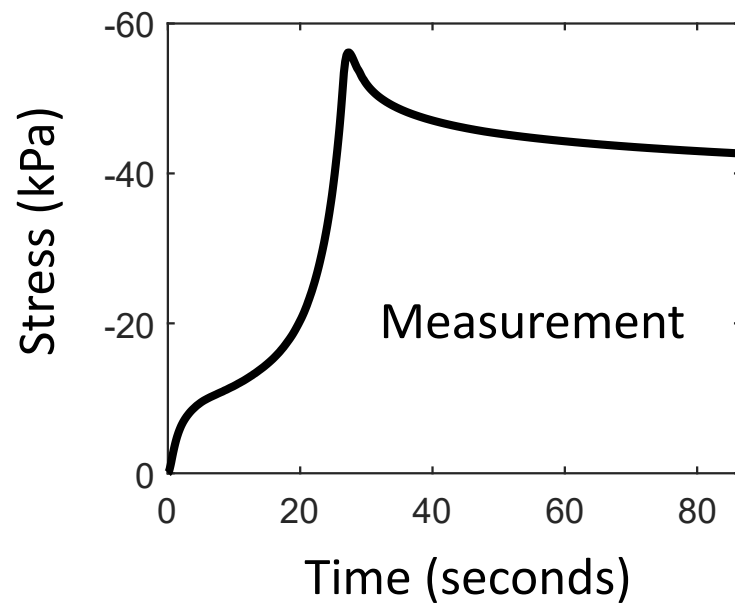
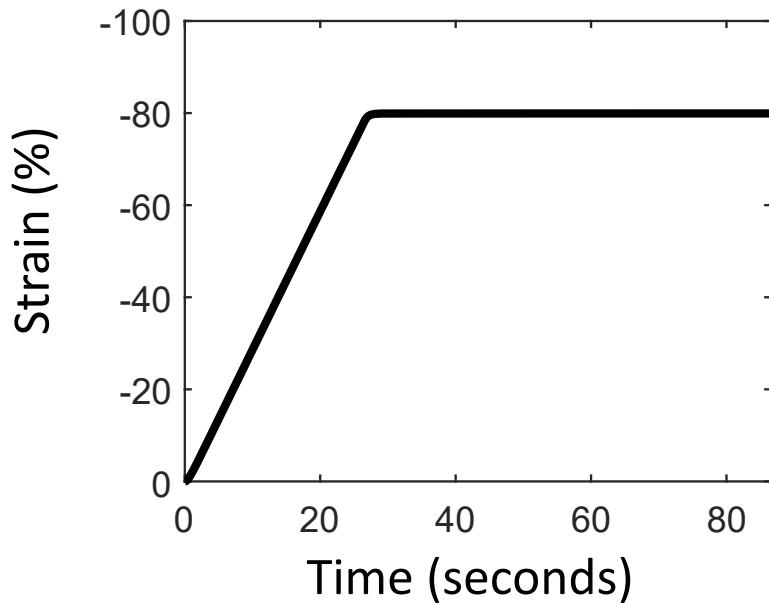
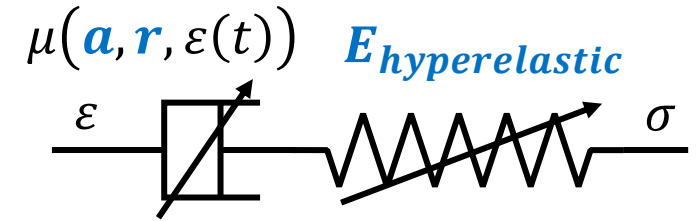
Rejuvenation: when  
 $\dot{\varepsilon} \neq 0$ ,  $\tau$  decreases

Aging model



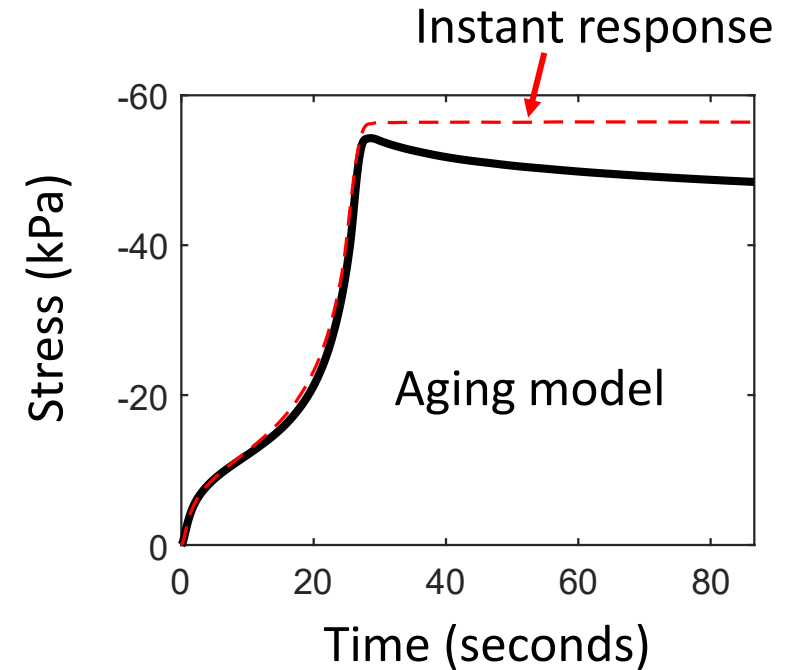
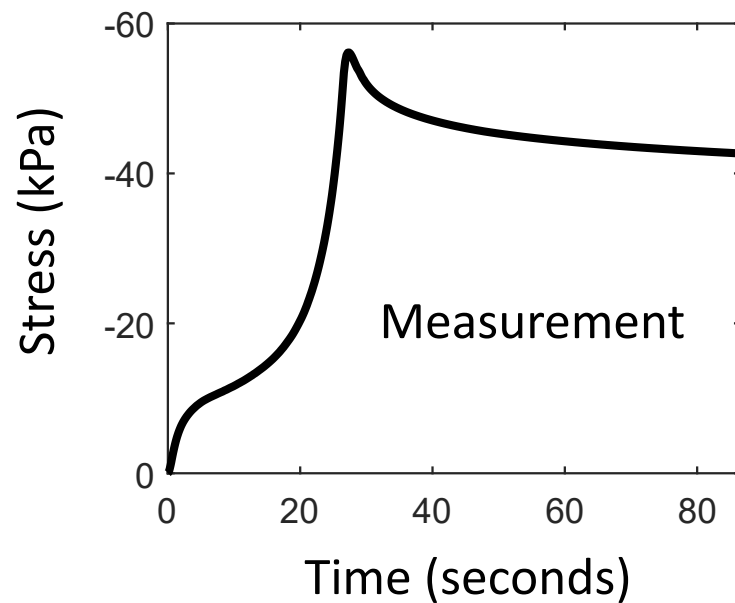
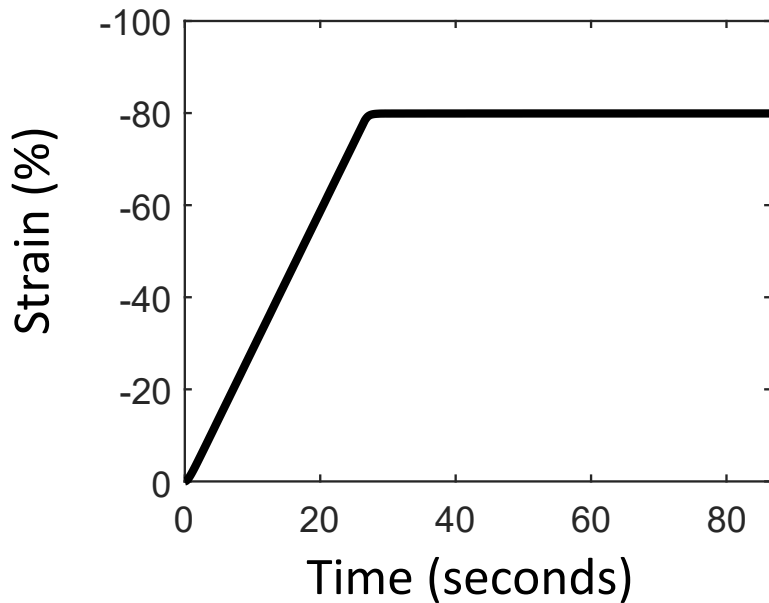
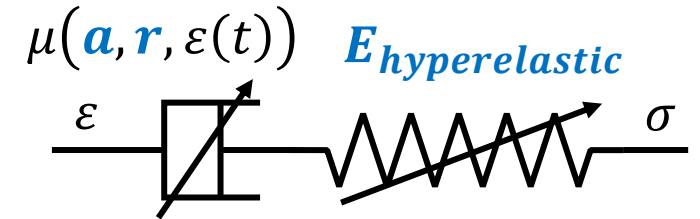
# Modelling full material behaviour

Aging model combining nonlinearity and relaxation  
Can predict response at any time



# Modelling full material behaviour

Aging model combining nonlinearity and relaxation  
Can predict response at any time  
Measure instant response if quick enough



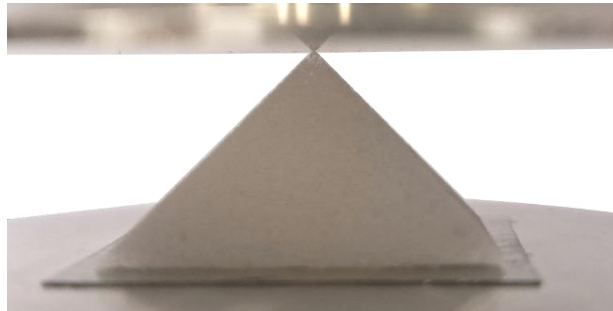
# Plan

- 1) Intrinsic material behaviour
- 2) Pyramid compression**

# Behaviour of an asperity

Measurements on pyramidal asperities of melamine foam  
Numerical FEM model  
Analytical expectation

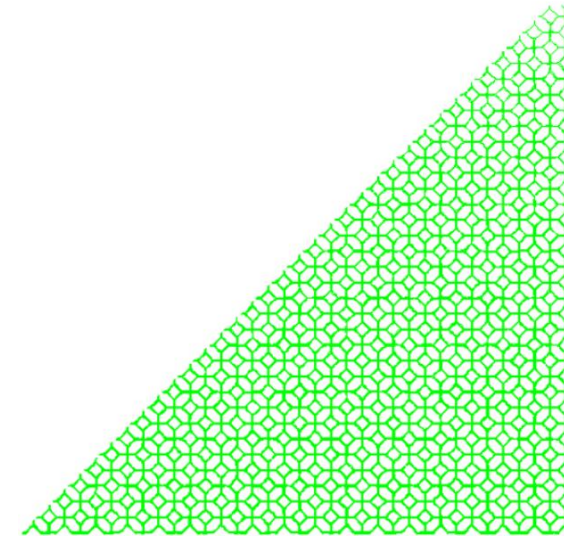
1) Experiment



2) Analytical

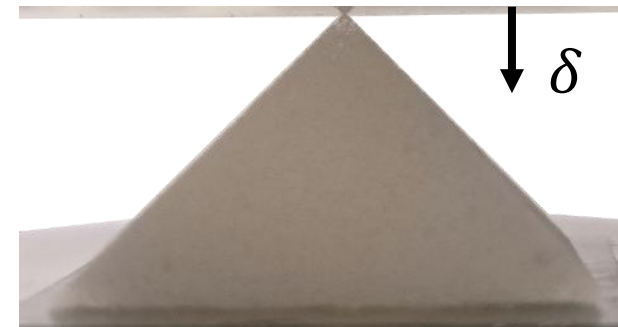
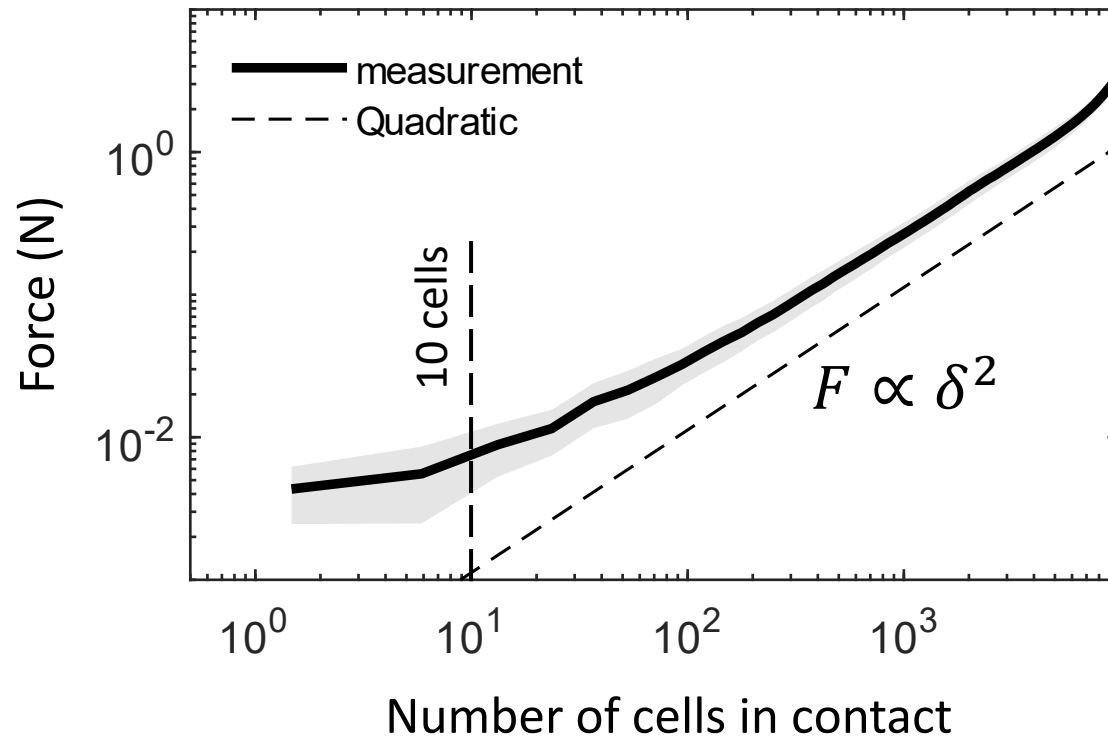
$$F \propto \delta^2$$

3) FEM models



# Behaviour of an asperity

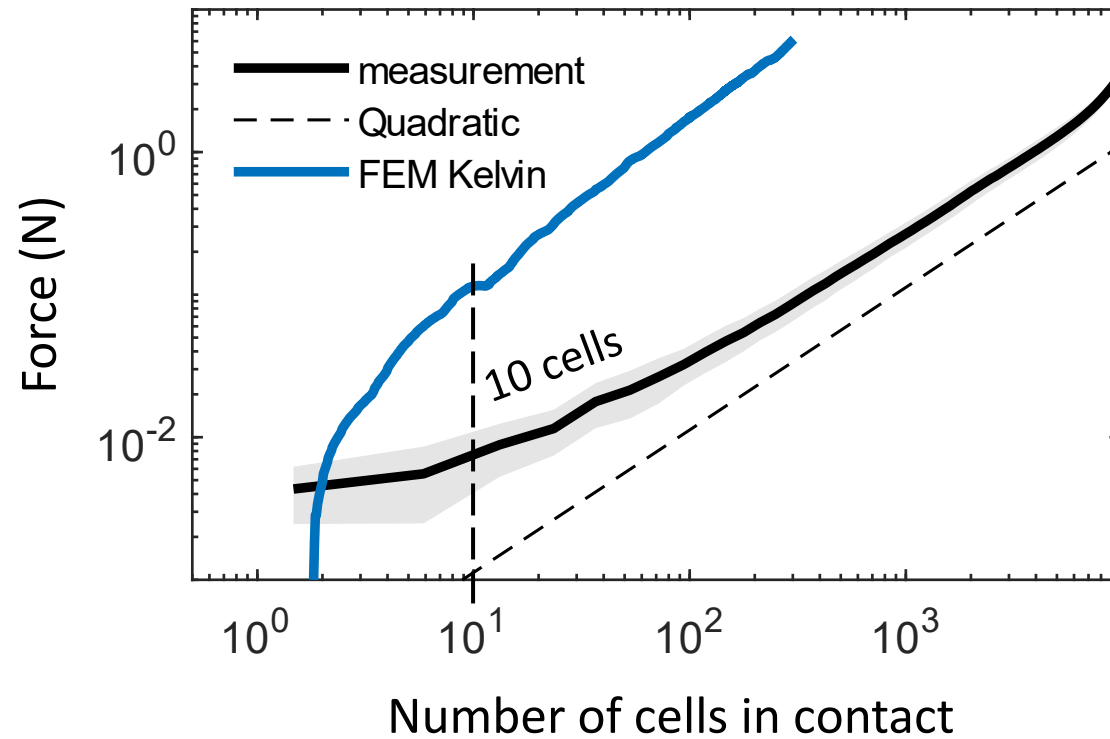
Experimental results similar to quadratic tendency!  
Works  $\gtrsim 10$  cells in contact



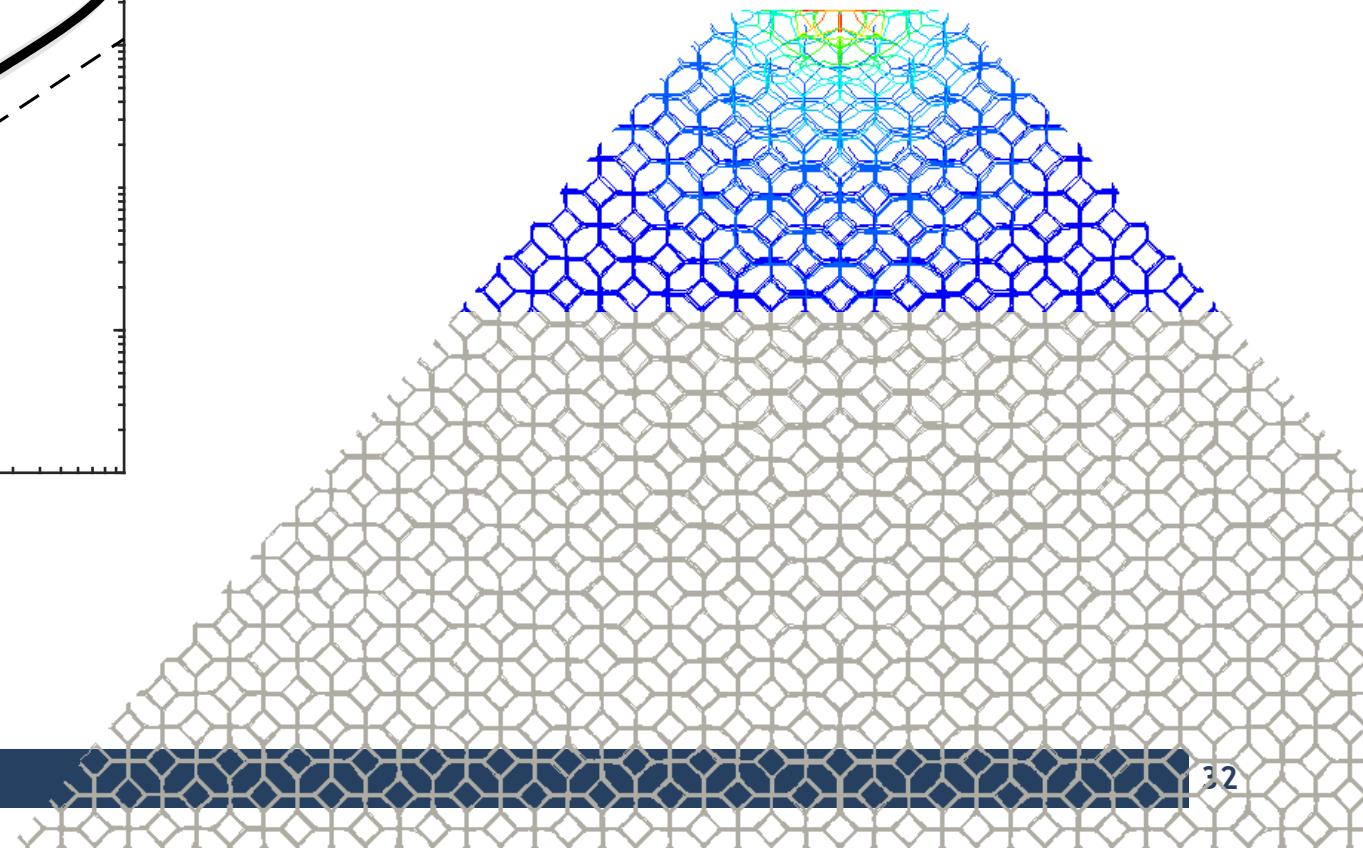
# Behaviour of an asperity

## Comparison with FEM model

- Quadratic tendency  $\approx$  10 cells in contact



12 cells in contact : nearly continuous

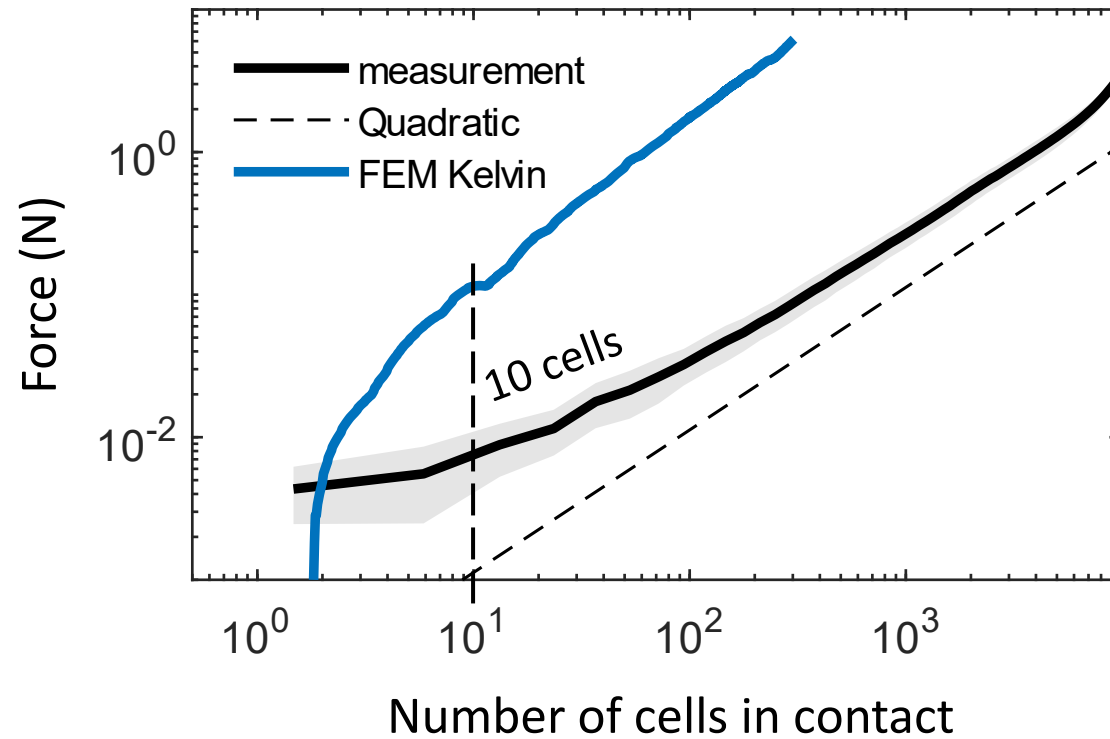




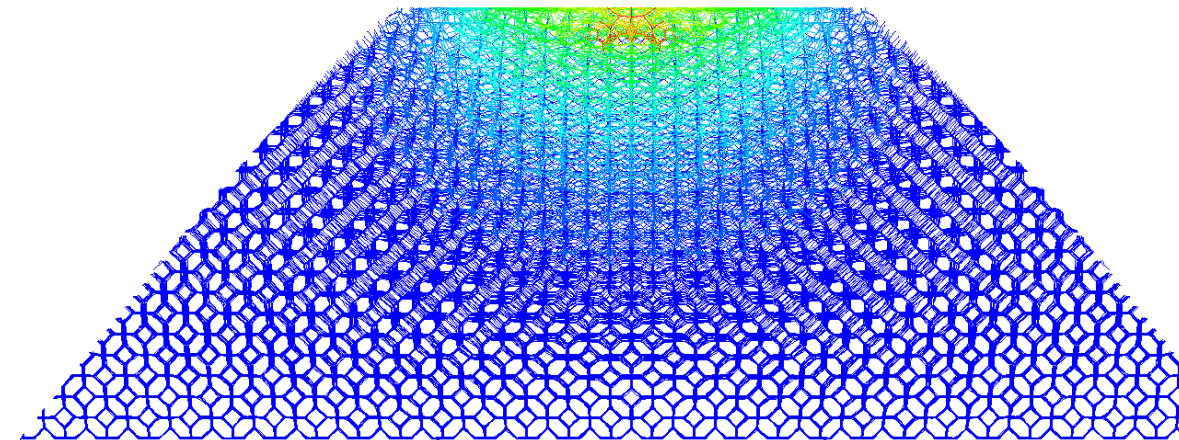
# Behaviour of an asperity

## Comparison with FEM model

- Quadratic tendency  $\gtrsim$  10 cells in contact



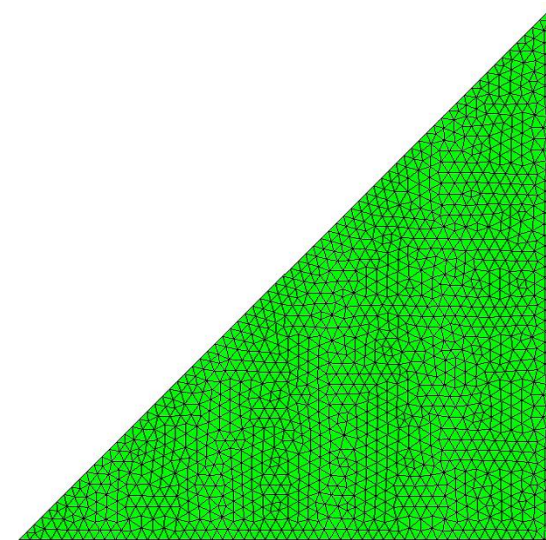
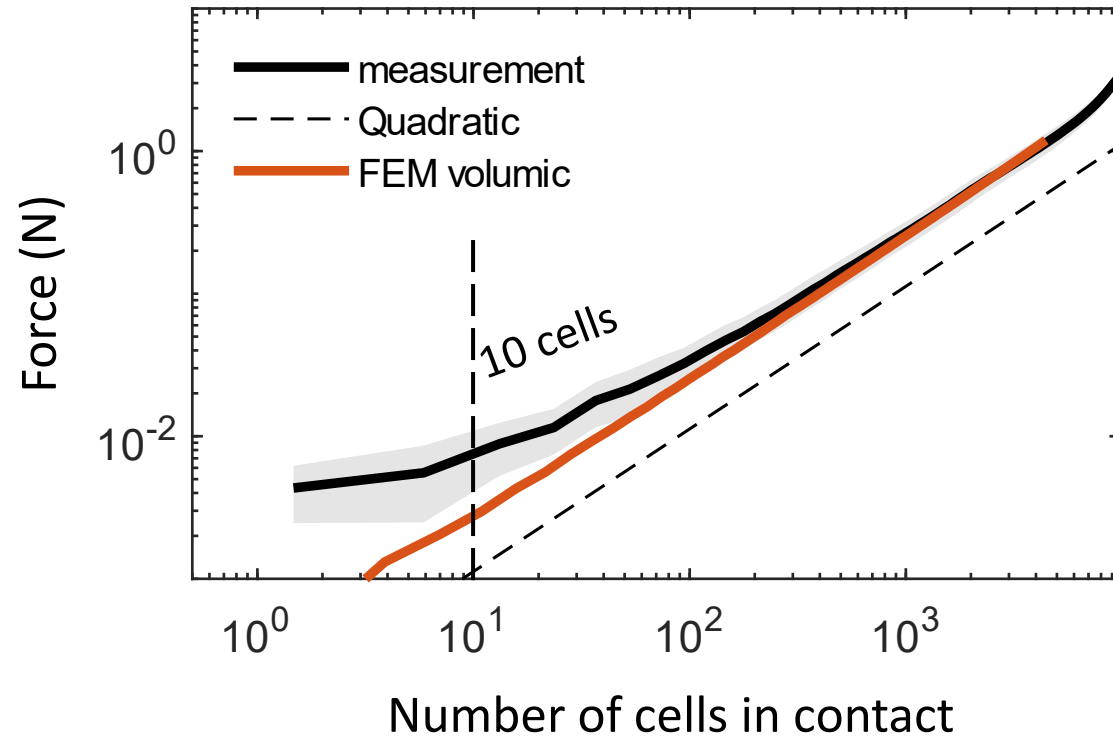
194 cells in contact: continuous



# Behaviour of an asperity

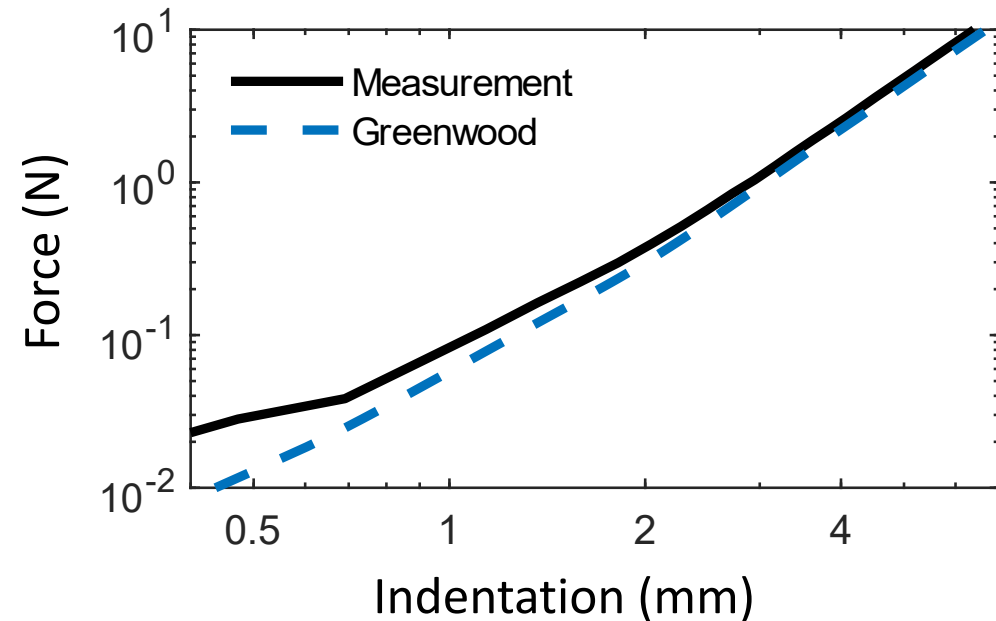
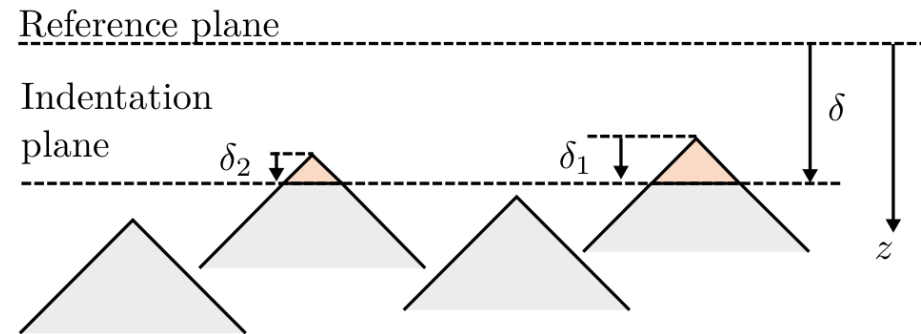
Continuous hyperelastic FEM model predicts prefactor

$$F \propto E \delta^2$$



# Application to a surface of several asperities

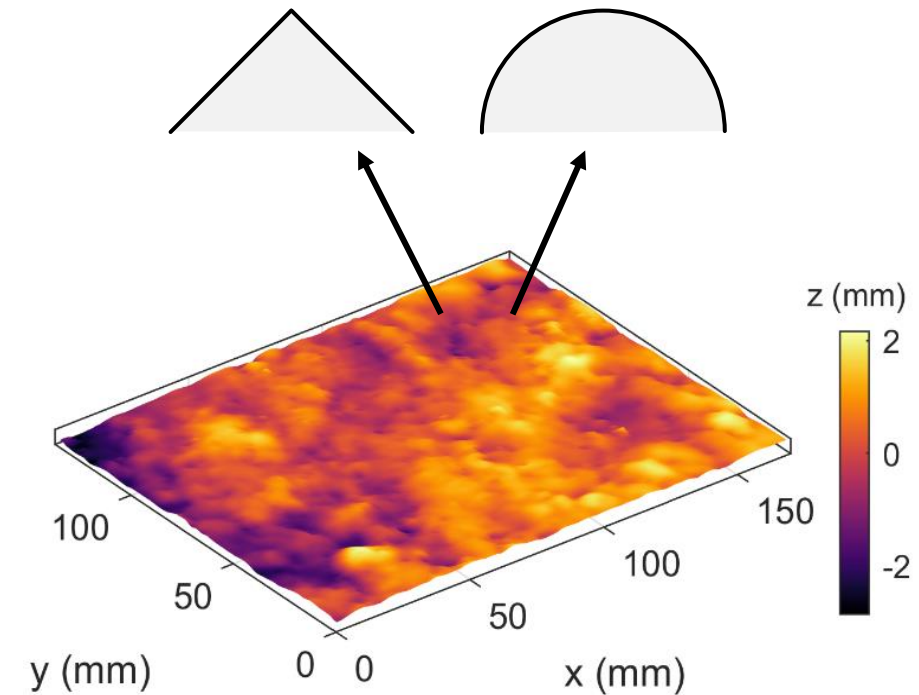
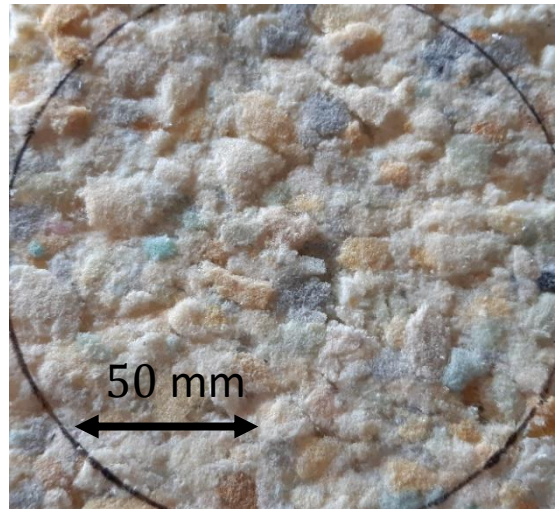
- A surface of several pyramids was created and modelled
- Asperity height distribution: quasi-uniform
- Greenwood surface roughness model was used



# Outlook

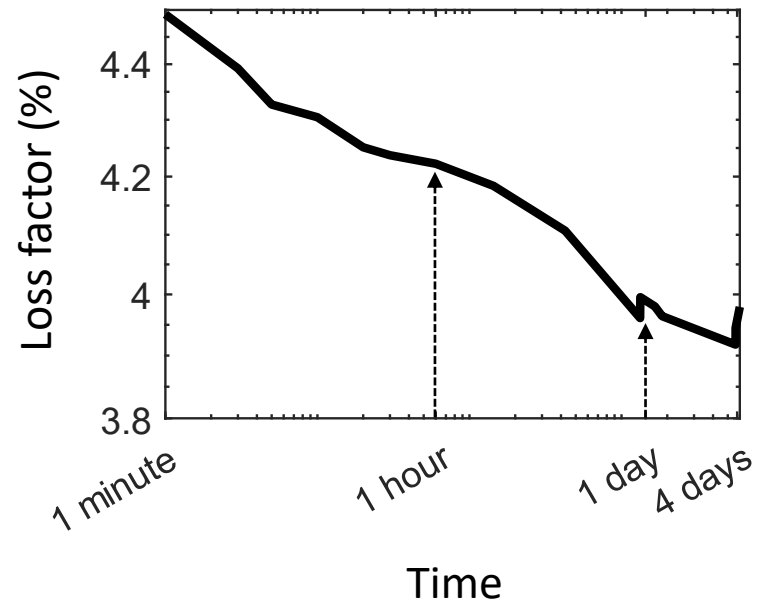
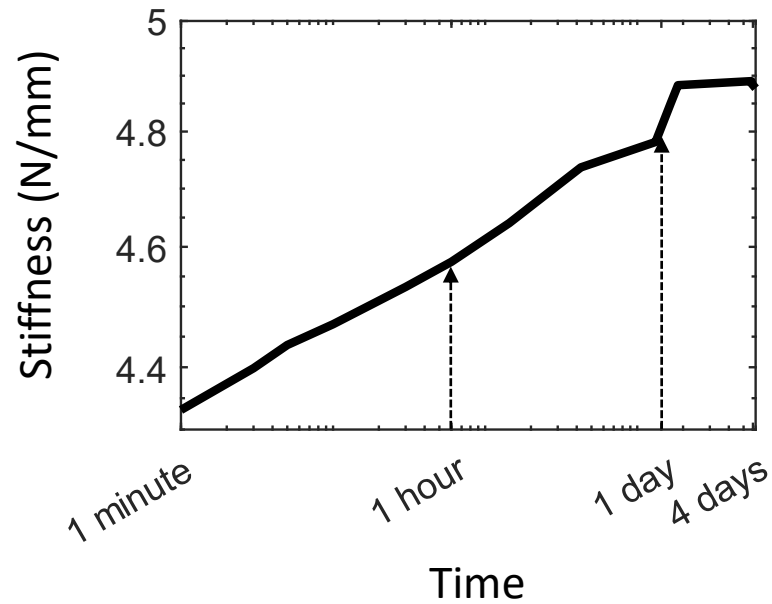
## Application to a real material

- A 3D scan could be analysed to compute asperity info
- Transition to bulk behaviour can be predicted
- Study impact of Poisson effect?



# Outlook

Effect of relaxation on dynamic behaviour should be examined



QMA measurements  
(20-200 Hz)

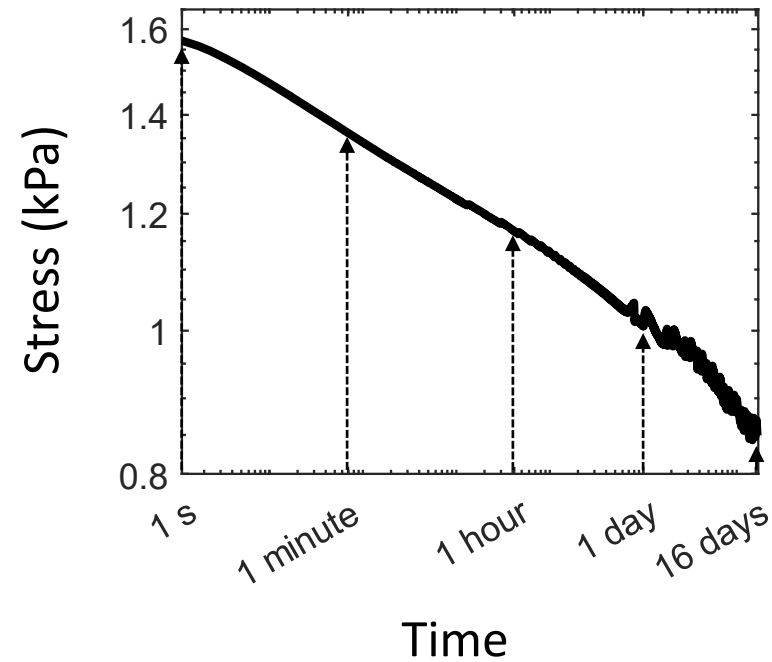
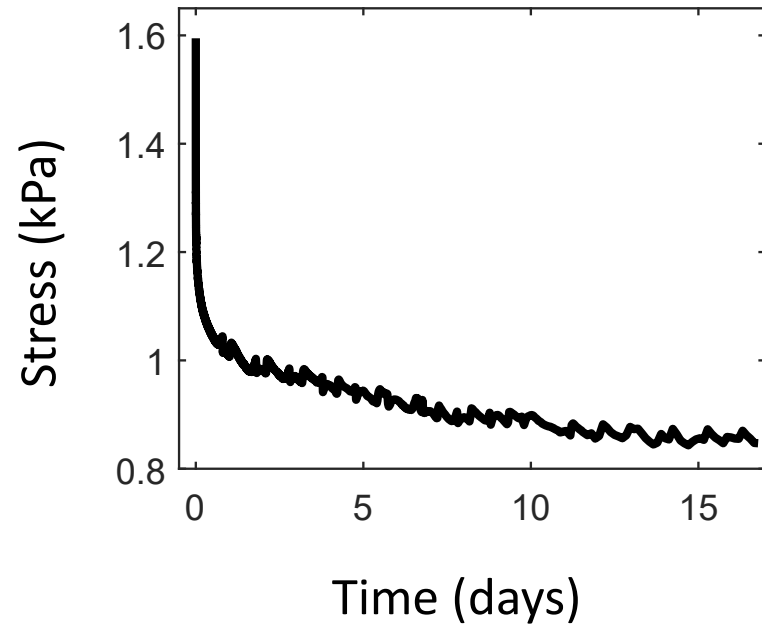
Difference after

- 30 minutes: 5%
- 24 hours: 10%

# Thank you

# Modelling material behaviour: relaxation

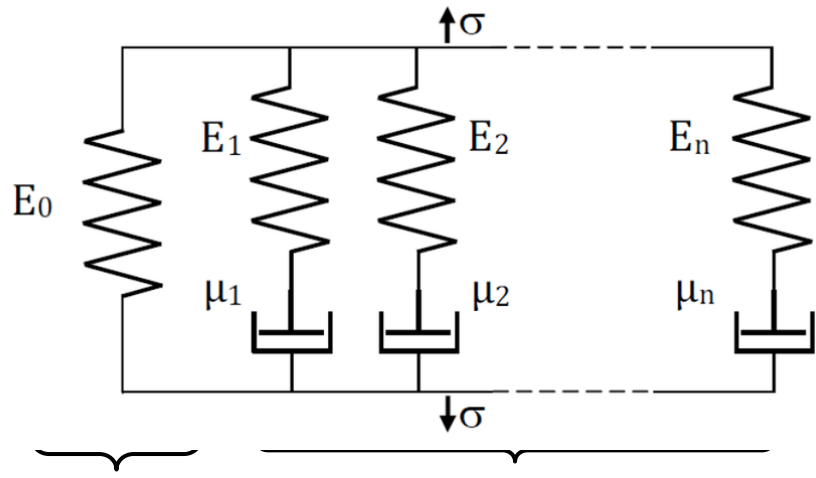
Relaxation continues at very long durations



# Modelling material behaviour: relaxation

Relaxation could be modelled with generalized Maxwell model

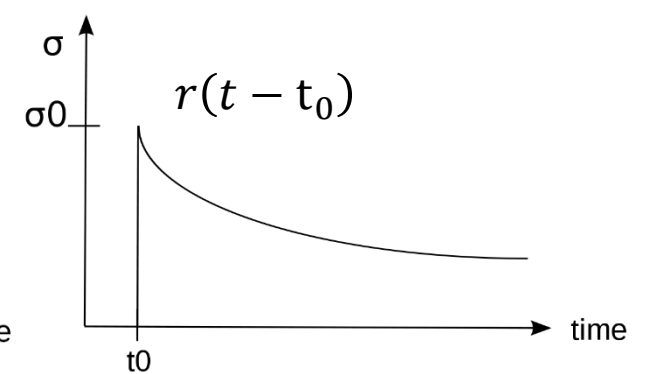
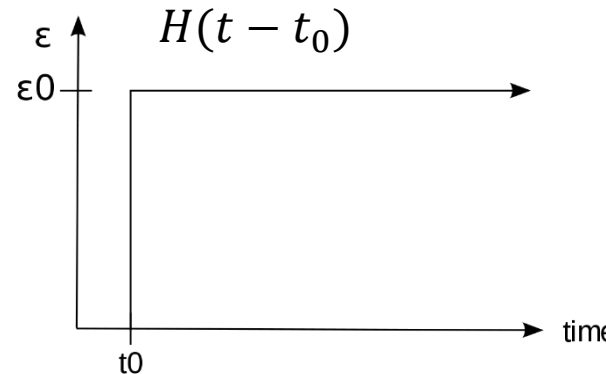
Generalized Maxwell model



Static stress  $E_0$      $N$  decay times  $\tau_i = \frac{\eta_i}{E_i}$

Stress response to a Heaviside step strain  $r(t)$ :

$$r(t) = E_0 H(t) + \sum_{i=1}^N E_i e^{-\frac{t}{\tau_i}} H(t)$$





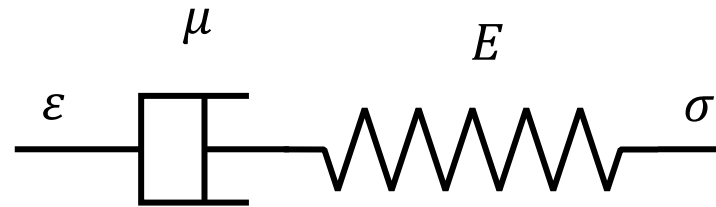
# Modelling material behaviour: relaxation

However the behaviour is more reminiscent of an aging phenomenon

$$\dot{\sigma} = -\frac{E}{\mu} \sigma + E \dot{\varepsilon}$$

$\frac{1}{\tau}$   $\swarrow$

Maxwell model

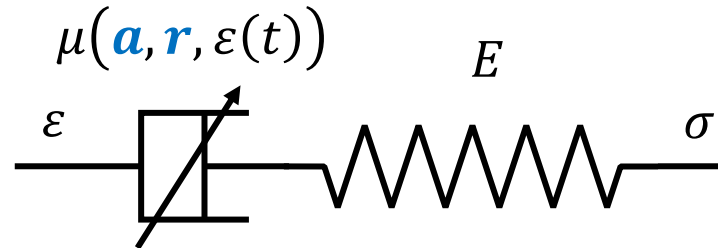


# Modelling material behaviour: relaxation

However the behaviour is more reminiscent of an aging phenomenon

$$\begin{cases} \dot{\sigma} = -f\sigma + E\dot{\varepsilon} \\ \dot{f} = -af^2 + r\dot{\varepsilon}^2 \end{cases}$$

Aging model



Aging: when  $\dot{\varepsilon} = 0$ ,  $\tau = \frac{1}{f}$  increases with slope  $a$

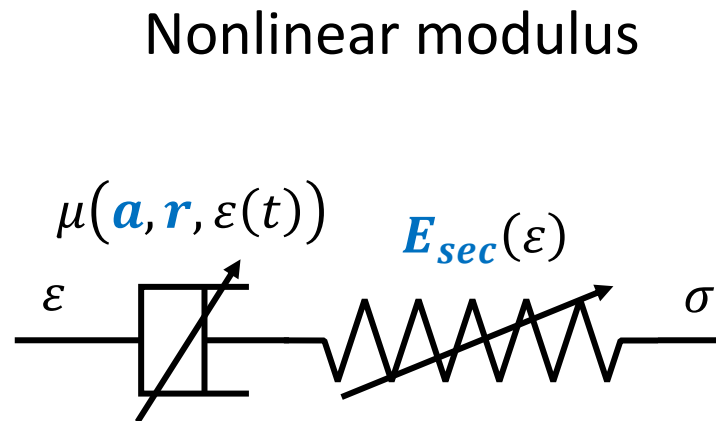
Rejuvenation: when  $\dot{\varepsilon} \neq 0$ ,  $\tau = \frac{1}{f}$  decreases

# Modelling material behaviour: relaxation

However the behaviour is more reminiscent of an aging phenomenon

$$\begin{cases} \dot{\sigma} = -f\sigma + E_{sec}(\varepsilon)\dot{\varepsilon} \\ \dot{f} = -af^2 + r\dot{\varepsilon}^2 \end{cases}$$

$\frac{1}{\tau}$       Strain-dependant modulus



Aging: when  $\dot{\varepsilon} = 0$ ,  $\tau = \frac{1}{f}$  increases with slope  $a$

Rejuvenation: when  $\dot{\varepsilon} \neq 0$ ,  $\tau = \frac{1}{f}$  decreases

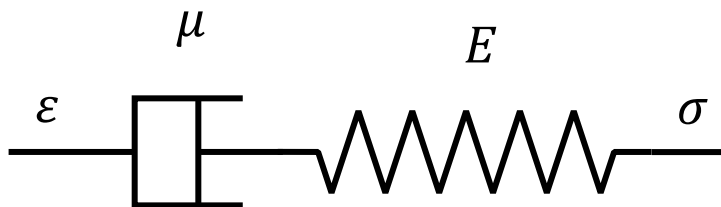
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However the behaviour is more reminiscent of an aging phenomenon

$$\dot{\sigma} = -\frac{E}{\mu}\sigma + E\dot{\varepsilon}$$

$= \frac{1}{\tau}$

Maxwell model

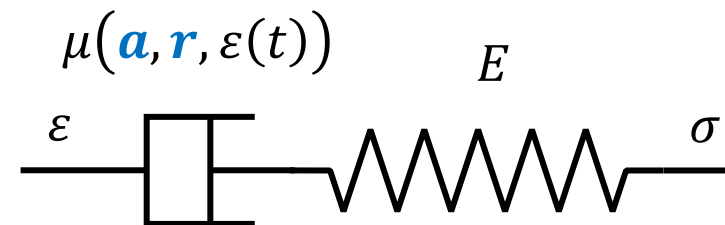


$$\begin{cases} \dot{\sigma} = -f\sigma + E\dot{\varepsilon} \\ \dot{f} = -af^2 + r\dot{\varepsilon}^2 \end{cases}$$

$= \frac{1}{\tau}$

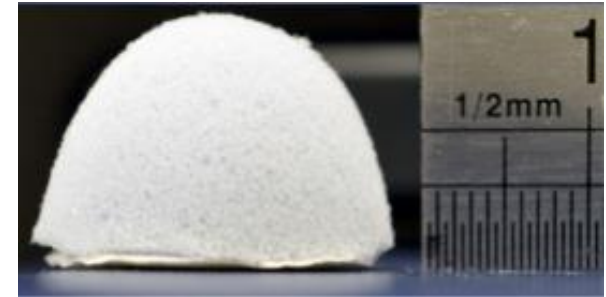
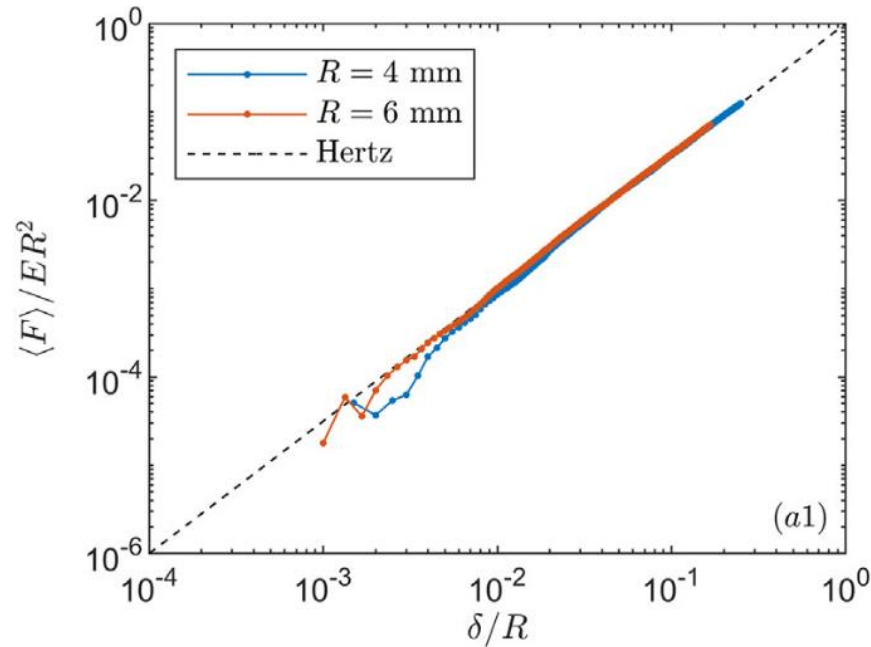
Aging                  Rejuvenation

Aging model



# Behaviour of an asperity

A sphere of foam follows Hertz' law (previous work: Hentati, 2020)



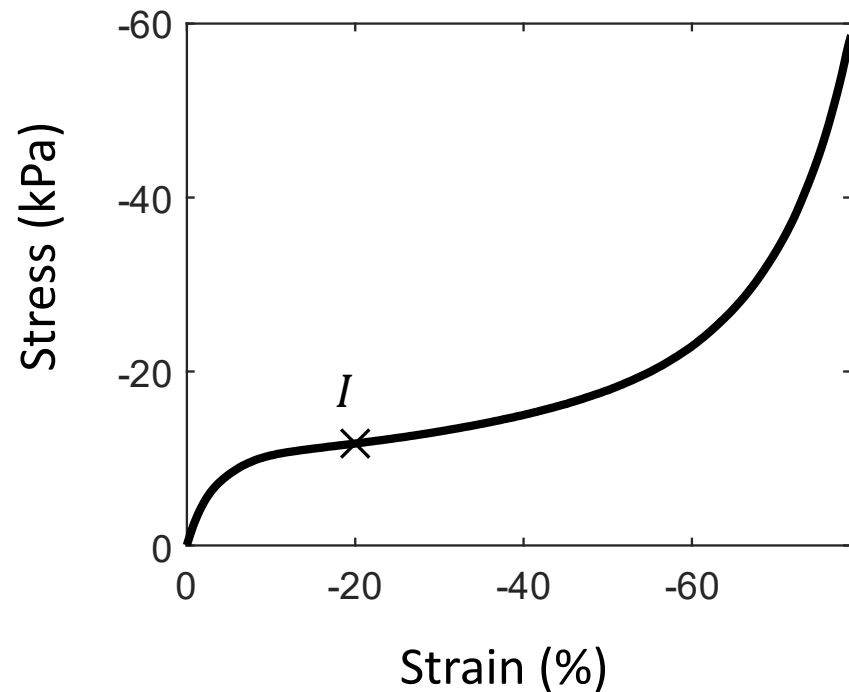
$$F \propto ER^{\frac{1}{2}}\delta^{\frac{3}{2}}$$

# Behaviour of an asperity

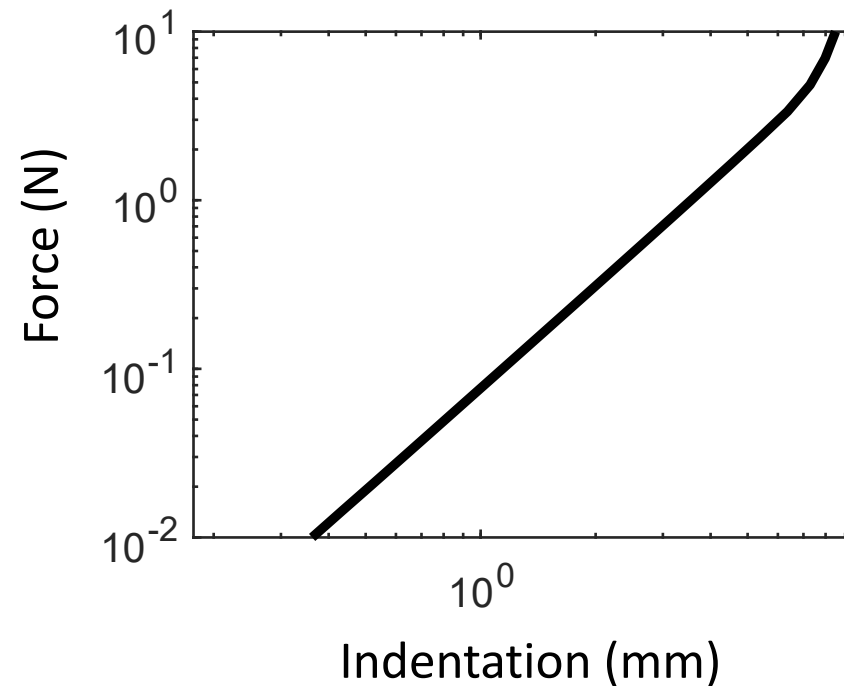
Analytical approximation with a single modulus  
Which modulus should be taken?

$$F \propto E \delta^2$$

Hyperelastic stress / strain response



Predicted pyramid force

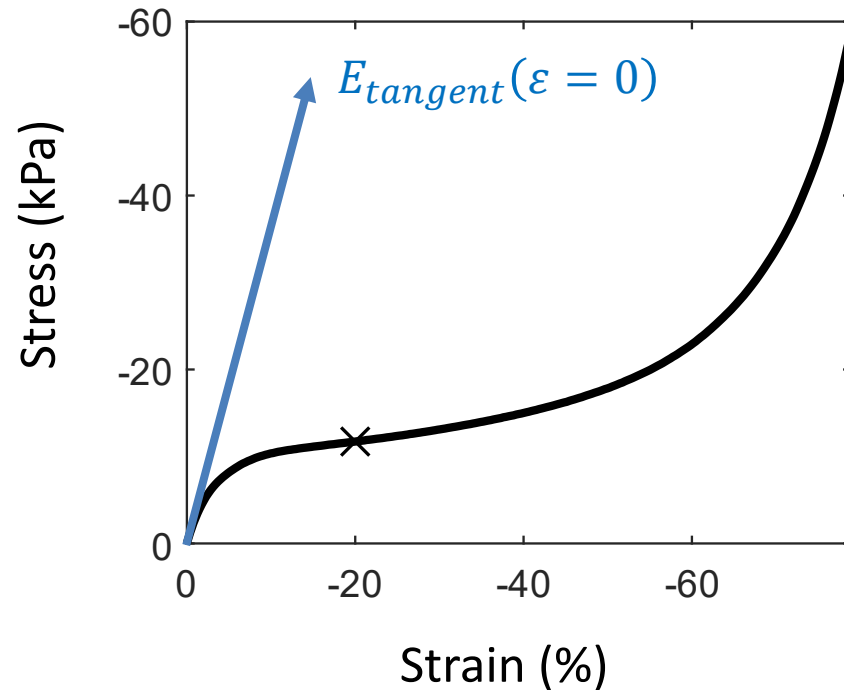


# Behaviour of an asperity

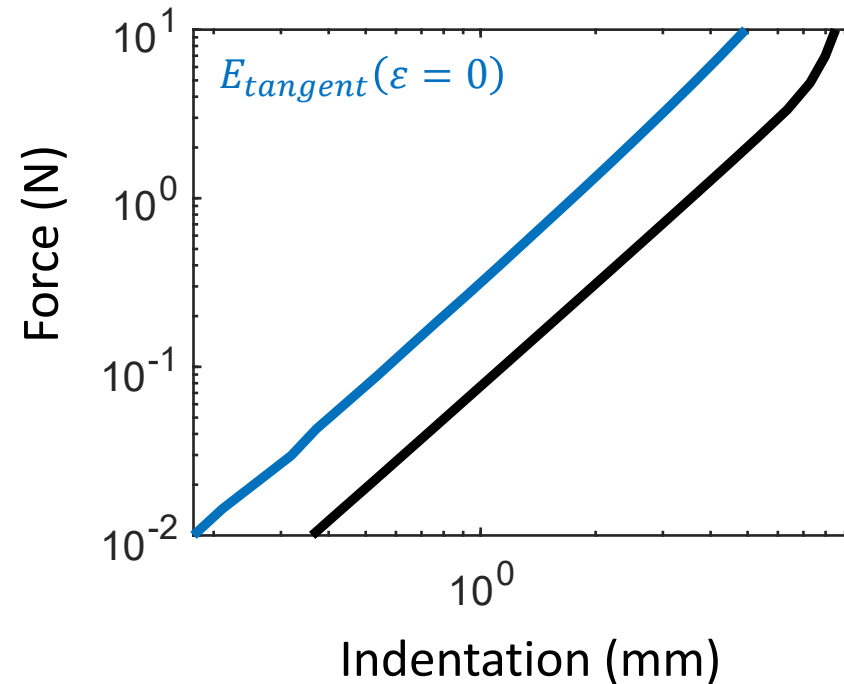
Analytical approximation with a single modulus  
Which modulus should be taken?

$$F \propto E \delta^2$$

Hyperelastic stress / strain response



Predicted pyramid force

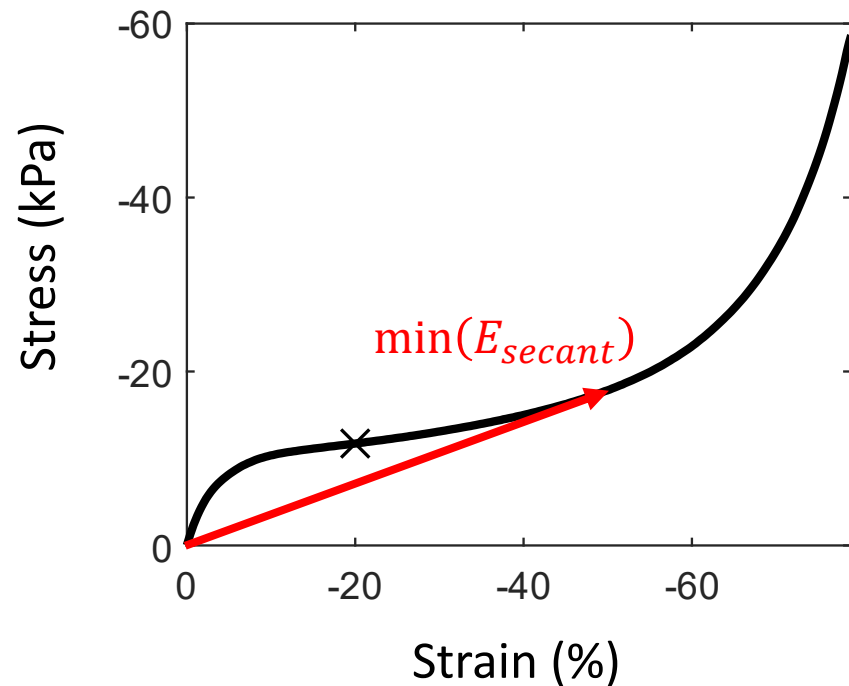


# Behaviour of an asperity

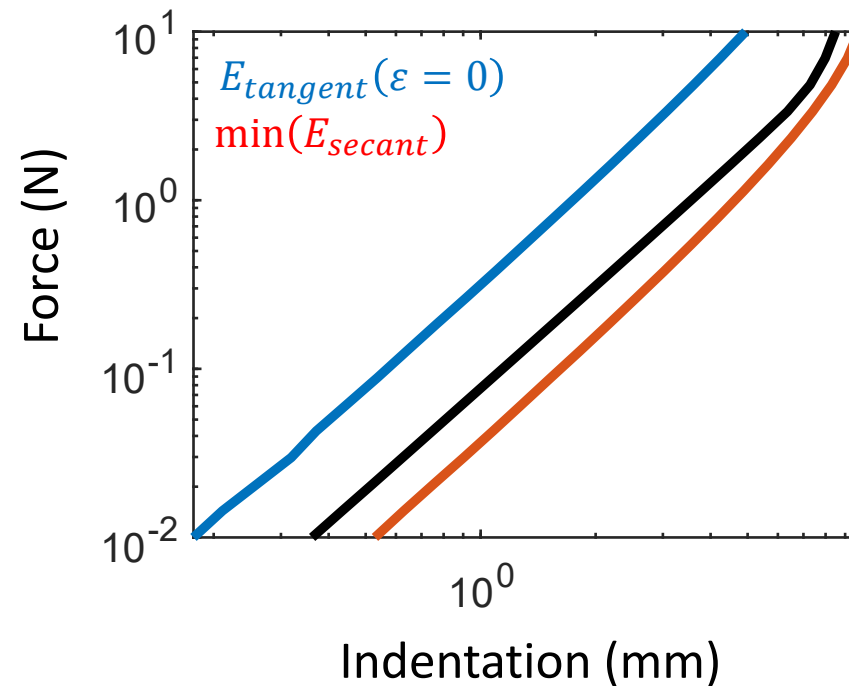
Analytical approximation with a single modulus  
Which modulus should be taken?

$$F \propto E \delta^2$$

Hyperelastic stress / strain response



Predicted pyramid force



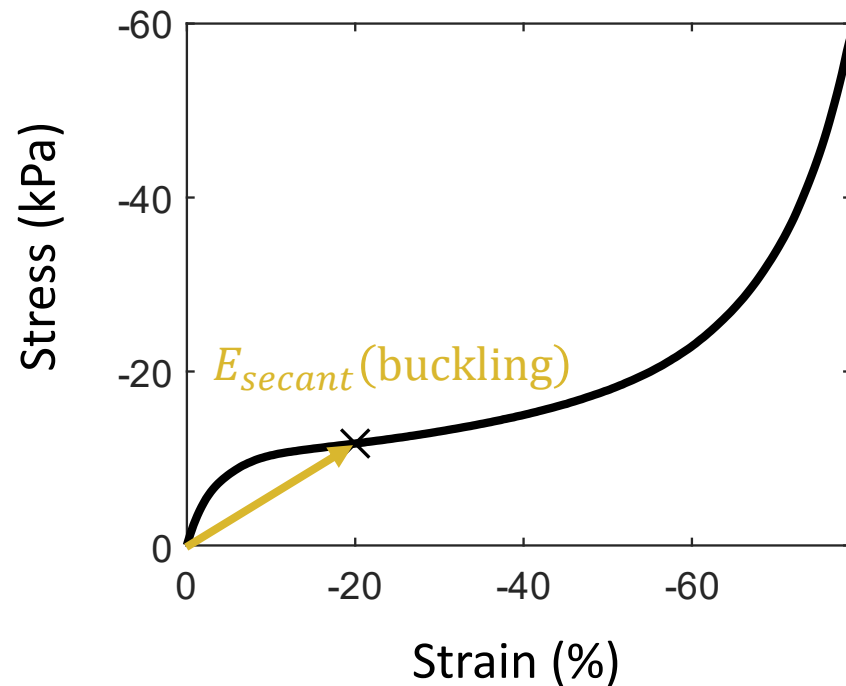


# Behaviour of an asperity

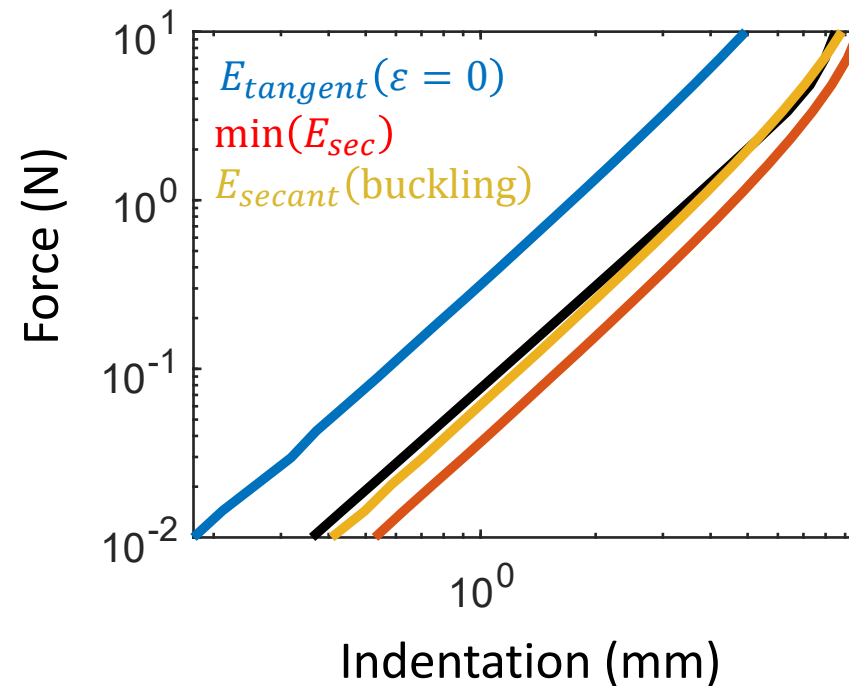
Analytical approximation with a single modulus  
Which modulus should be taken?

$$F \propto E \delta^2$$

Hyperelastic stress / strain response

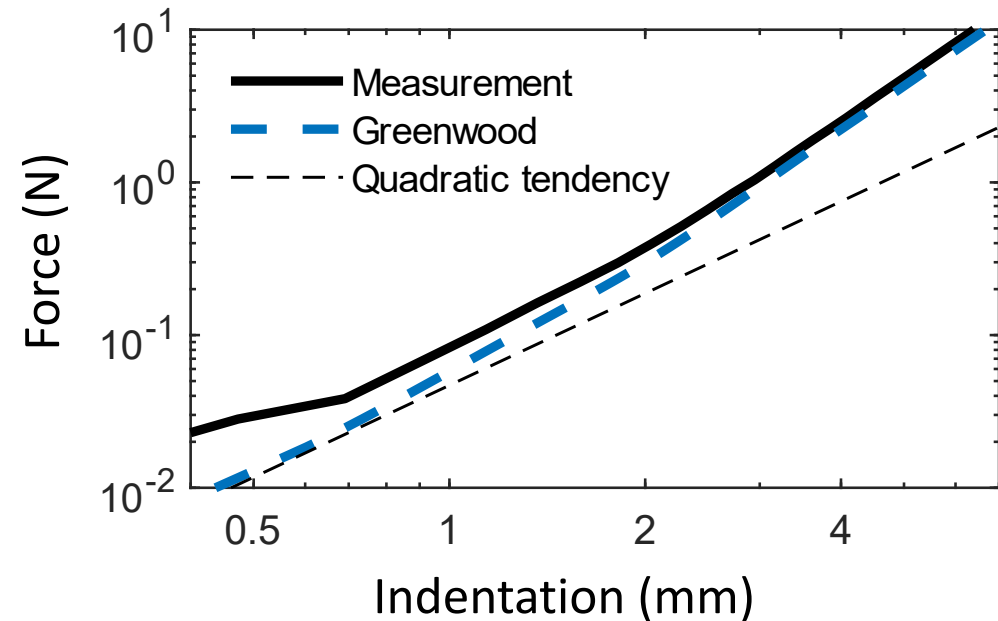
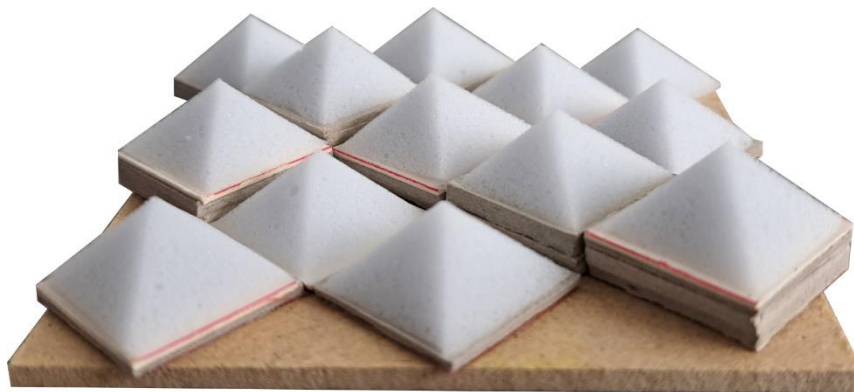
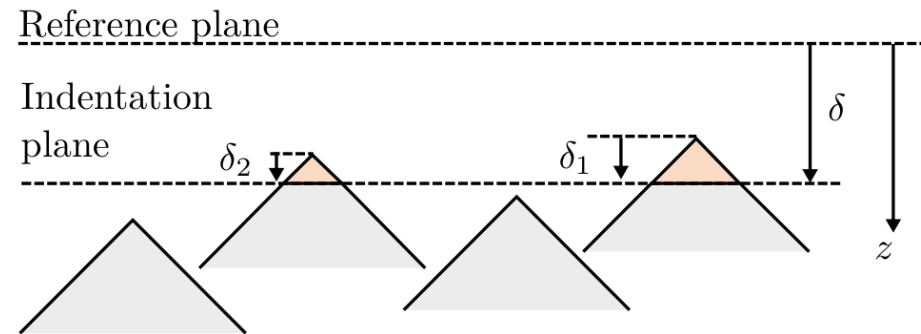


Predicted pyramid force



# Application to a surface of several asperities

A surface of several pyramids was created and modelled  
Quasi-uniform asperity height distribution  
Greenwood surface roughness model



# Outlook

Measurements on radiating plate  
Measurements on real engine casing

