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Symposium on the Acoustics of Poro-Elastic Materials

Acoustical Properties of Anisotropic Spinodoid Structures

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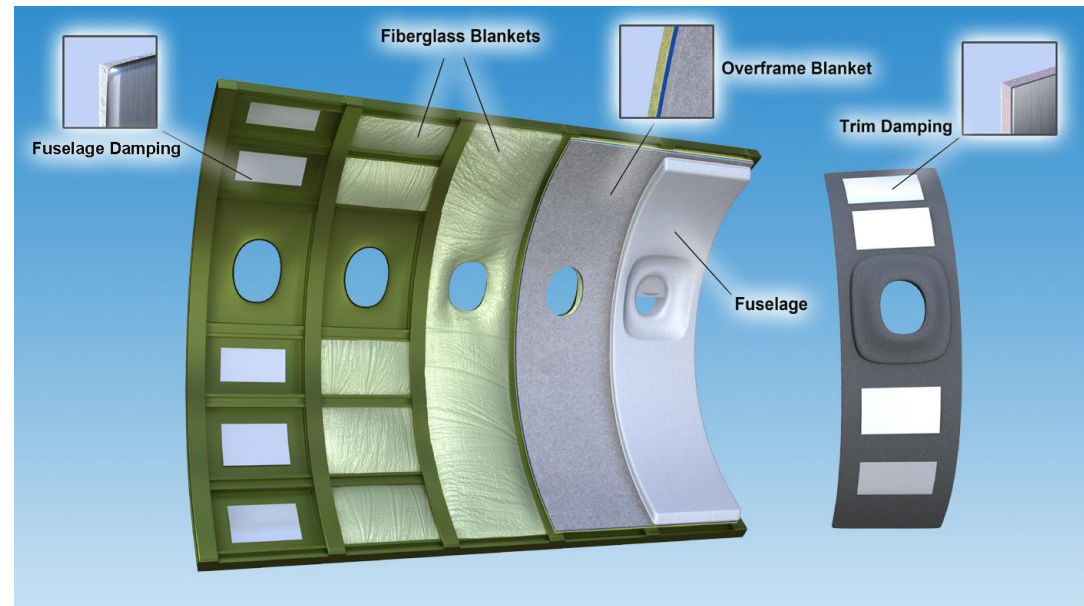
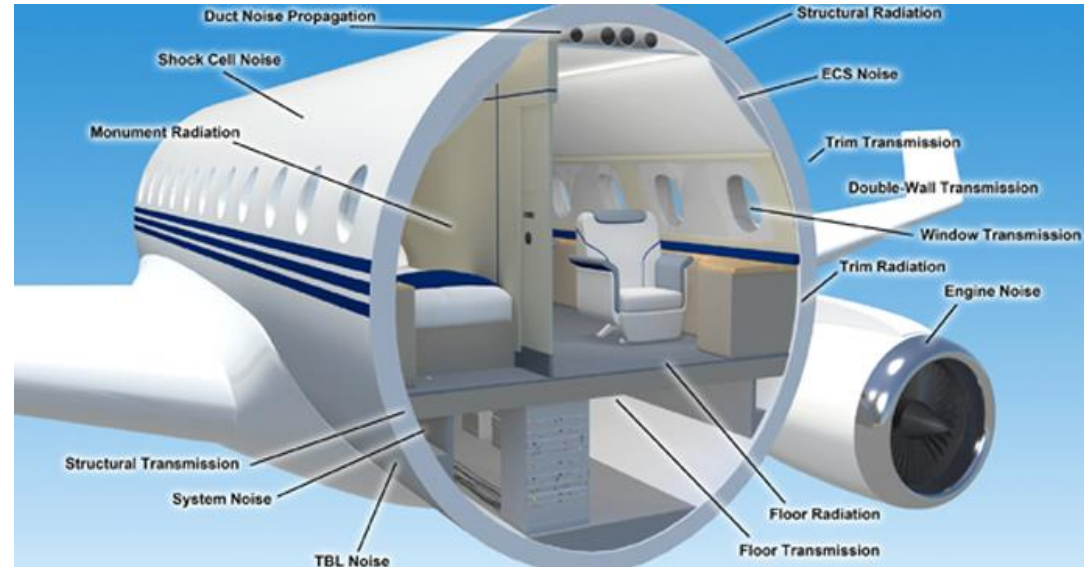
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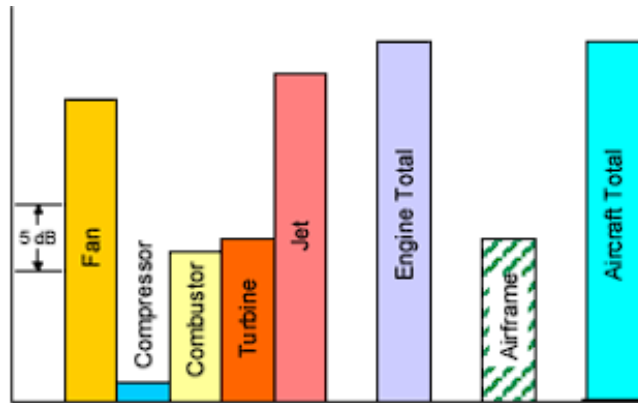
Challenge: Noise Control = “Constrained” Acoustics

What’s important about noise control materials?

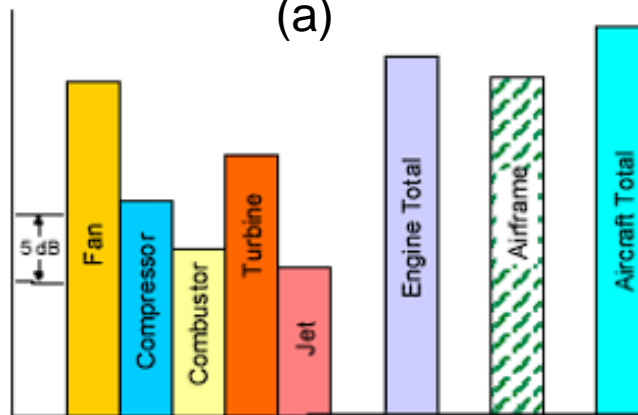
- Cost
- Safety
- Weight
- Volume
- Recyclability
- Structural Performance
- Thermal Performance
- ...
- Acoustical Performance



Jet Noise: Broadband Dominant

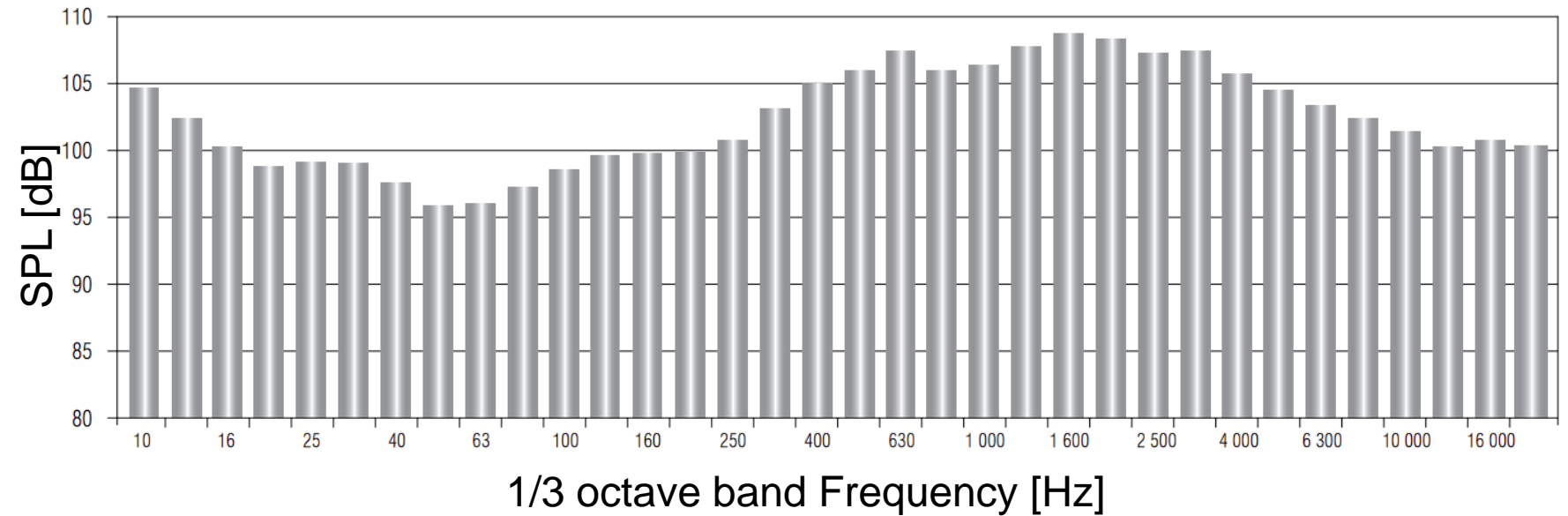


(a)



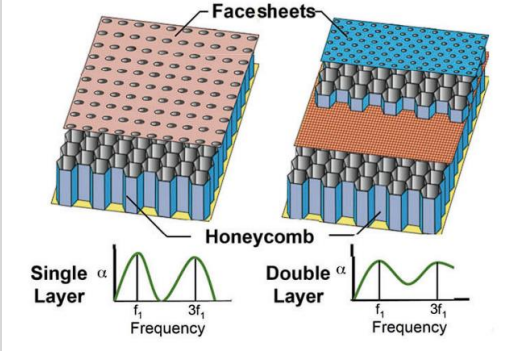
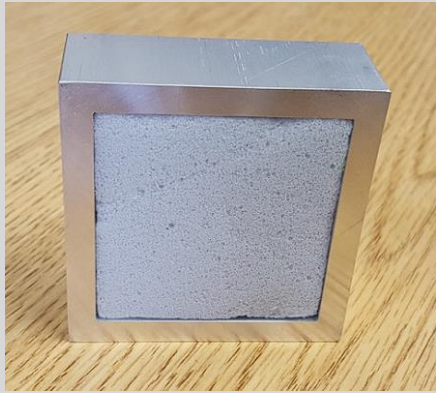
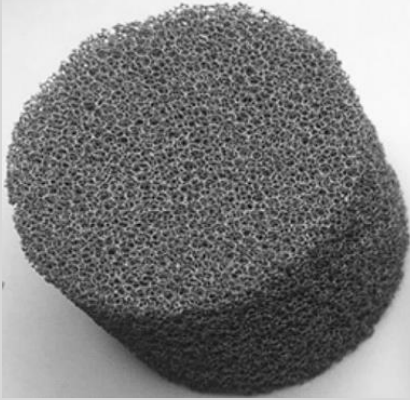
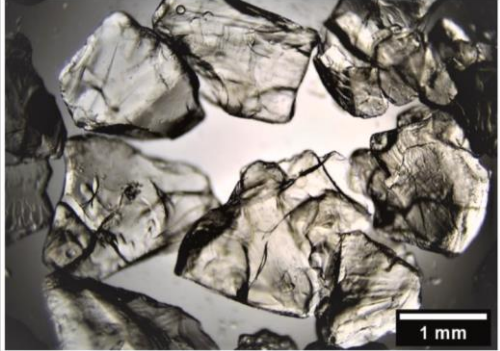
(b)

Aircraft noise source on (a) take-off and (b) approach [1]



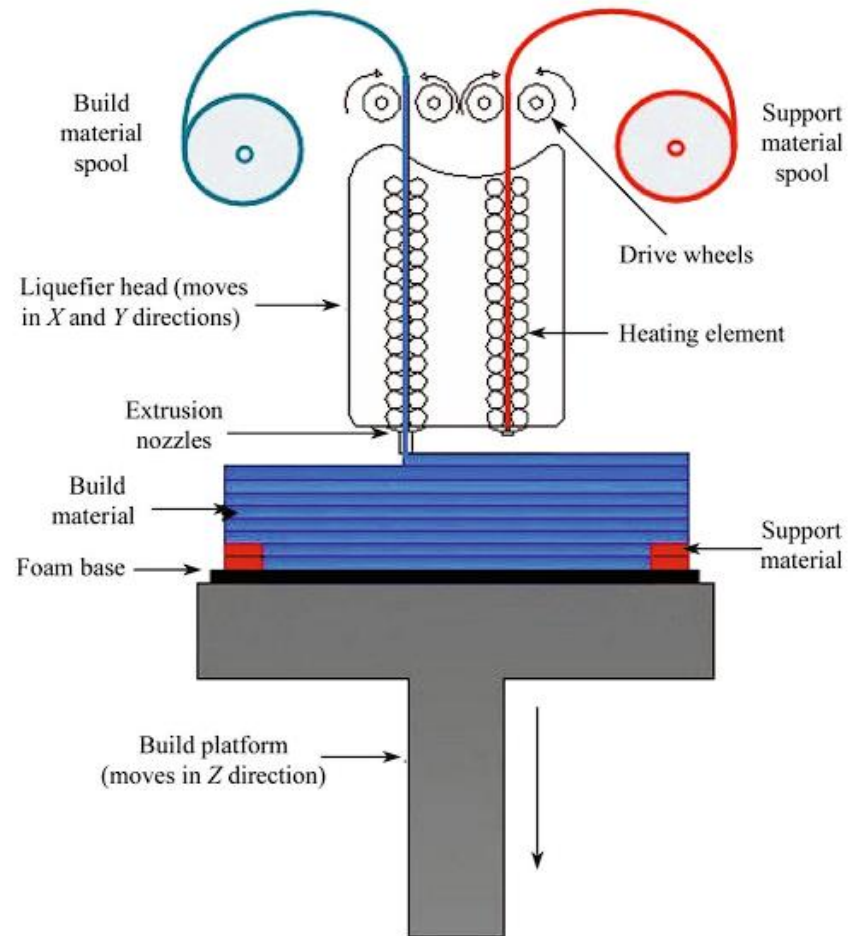
Noise generated by a modern jet engine [2]

Acoustic Treatments: A Comparison

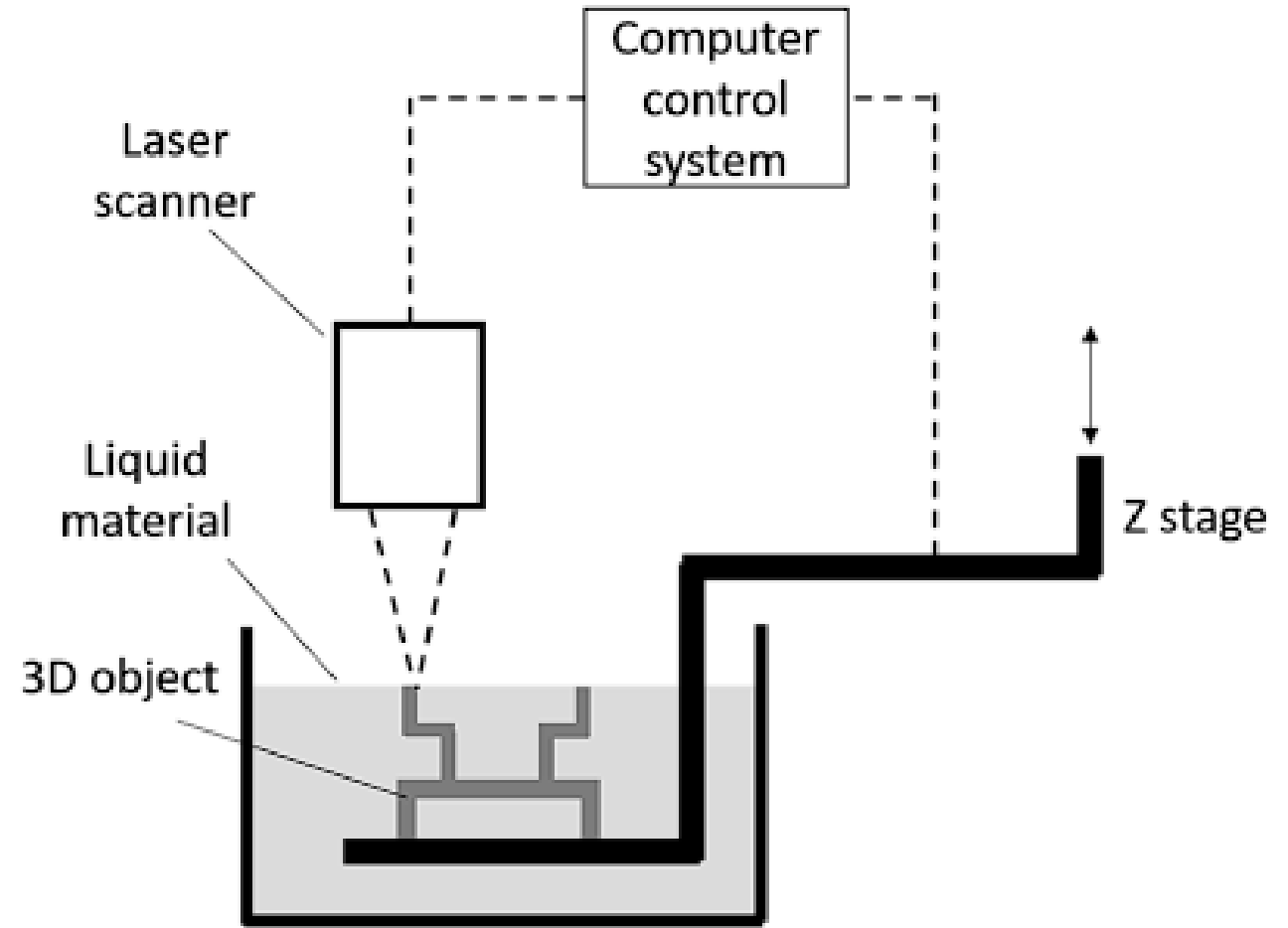
Material	Honeycomb acoustic liners [3]	Insulation foams [4-5] (melamine, polyimide)	Metal foams [6] (Aluminum)	Granular materials (aerogel [7], beads [8])
Demonstration	 <p>The diagram illustrates the structure of a honeycomb acoustic liner. It shows two configurations: a single layer and a double layer. The single layer consists of a top facesheet, a honeycomb core, and a bottom facesheet. The double layer has an additional top facesheet. Below the diagrams are two graphs showing the absorption coefficient α versus frequency. The single layer graph shows two peaks at frequencies f_1 and $3f_1$. The double layer graph shows a broader absorption band between f_1 and $3f_1$.</p>	 <p>A photograph of a square acoustic foam sample mounted in a wooden frame. The foam is a light gray color with a porous, fibrous texture.</p>	 <p>A photograph of a dark, porous metal foam sample. It has a highly textured, interconnected network of metal cells.</p>	 <p>A photograph showing granular materials, including aerogel and beads. The aerogel is a translucent, fibrous material, and the beads are small, dark particles. A 1 mm scale bar is visible in the bottom right corner.</p>
Advantages	Structural Tunable	Lightweight; Broadband absorption	Stiffer than normal foams; Lightweight; Broadband absorption	Low frequency noise control; Lightweight
Disadvantages	Tonal over broadband noise control feature	Structural Limited tunability	Limited tunability	Difficult to contain

→ Motivation: development of tunable and broadband acoustical treatments

Additive Manufacturing

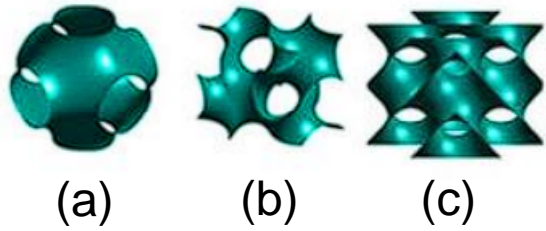


Schematic of fused deposition modeling (FDM) printer [9]

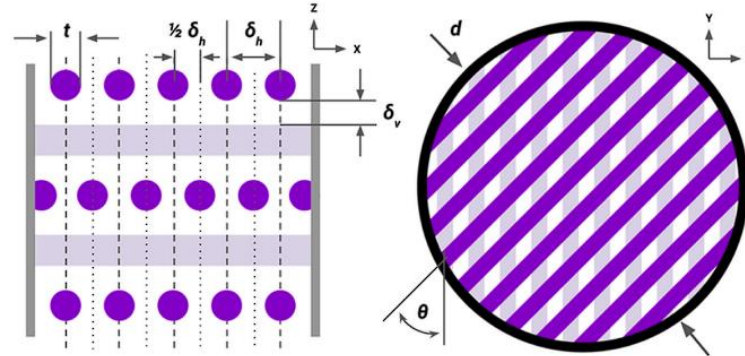


Schematic of stereolithographic (SLA) printer [10]

3D Printed Acoustic Treatments with Periodic Microstructure



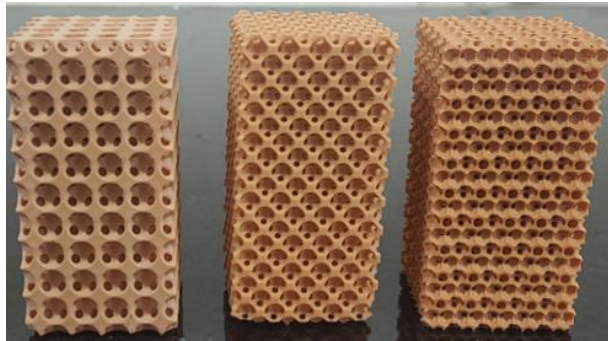
Triply periodic minimal surfaces (TPMS) with (a) primitive, (b) gyroid, and (c) diamond unit cells [11]



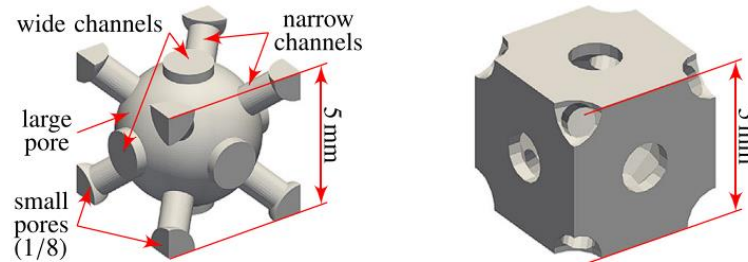
Schematic of fiber sample [12]



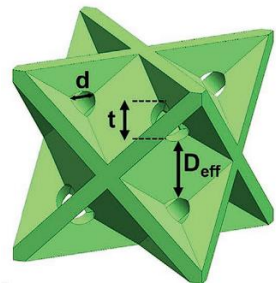
Gyroid with overlaid fibers [13]



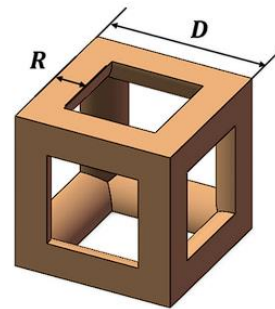
Truss Structures [14]



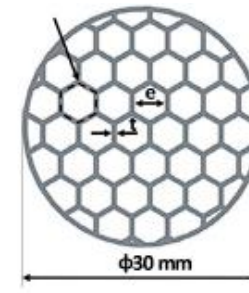
'Sphere subtracting' sample (a) pore network and (b) unit cell [15]



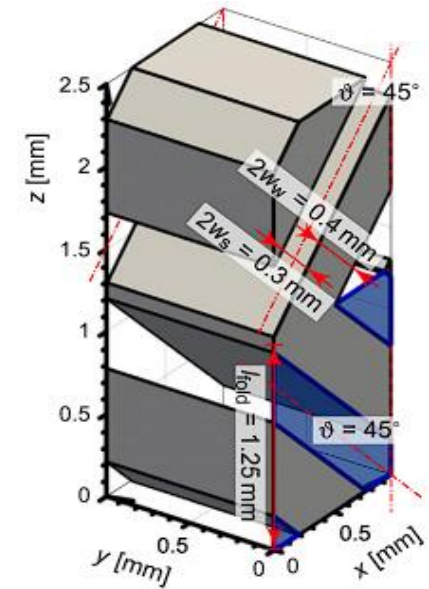
Fluorite-plate unit cell [16]



Body-centered cubic unit cell [17]



Narrow tube array with hexagonal unit cell [18]



Folded slit unit cell [19]

3D Printed Spinodoid with Non-Periodic Microstructure

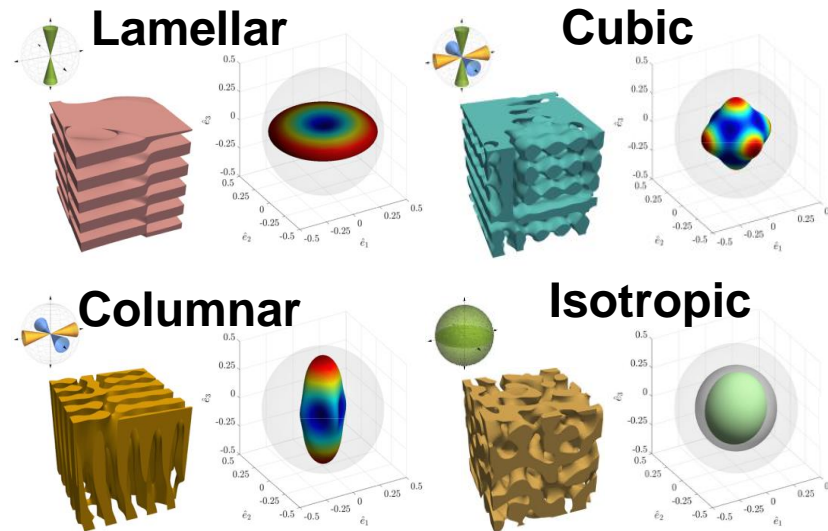
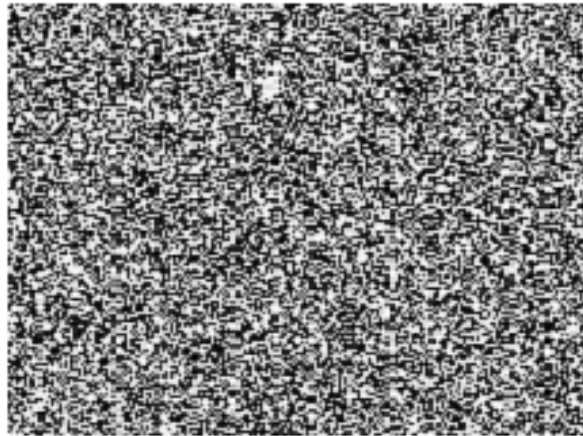
Advantage of non-periodic microstructure

- Optimization options
- Easy to generate gradients and anisotropy

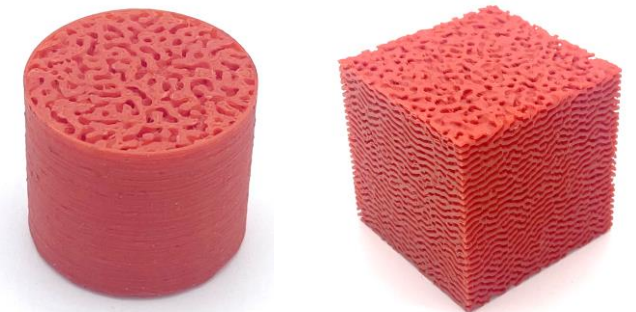


Introducing our target material

- **Spinodoid Structure**, with potentials in acoustical plus structural applications



Bed Temperature: 60°C
 Nozzle Diameter: 0.4 mm
 Layer height: 0.1 mm



Physics: Spinodal Decomposition [20-21], e.g. oil & water separating out

Modeling: Gaussian Random Fields [22]

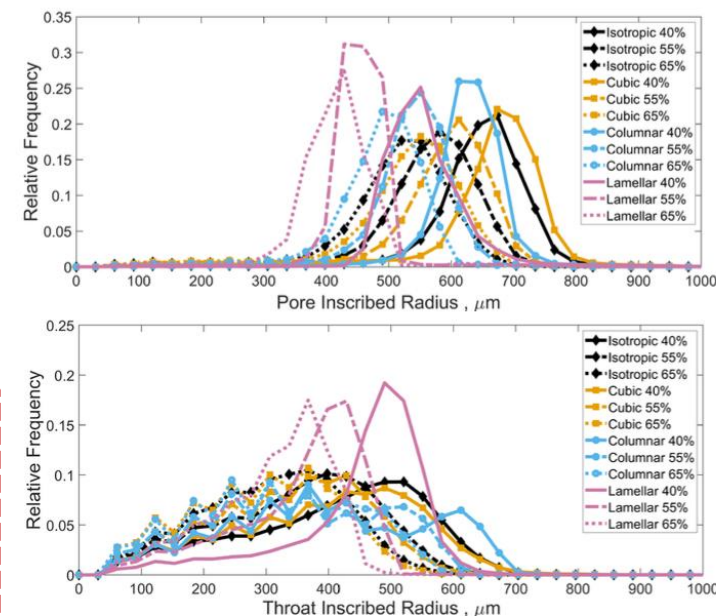
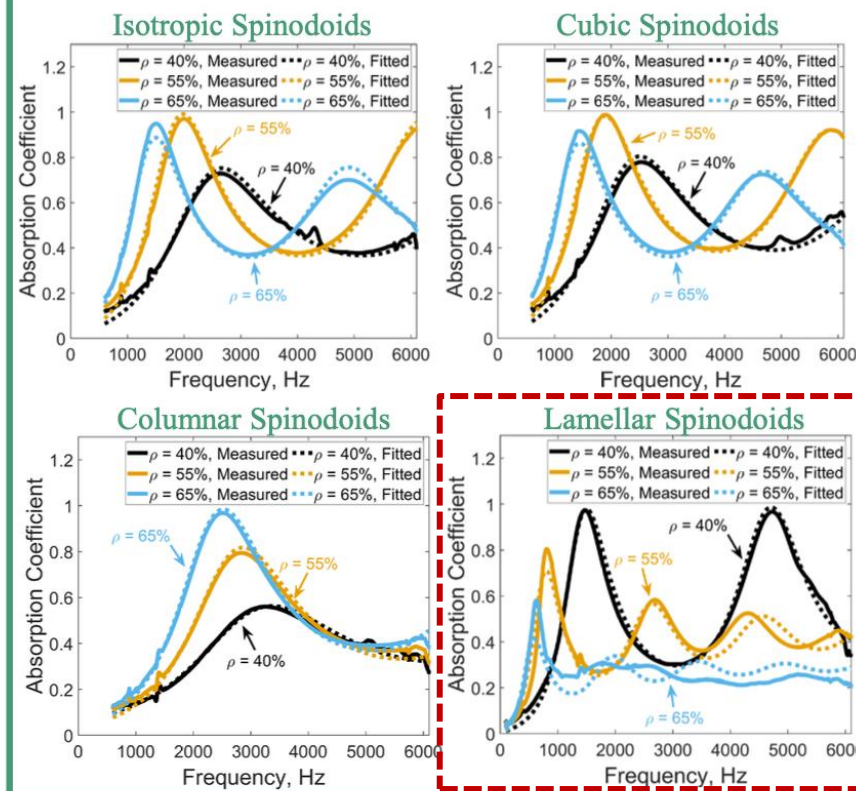
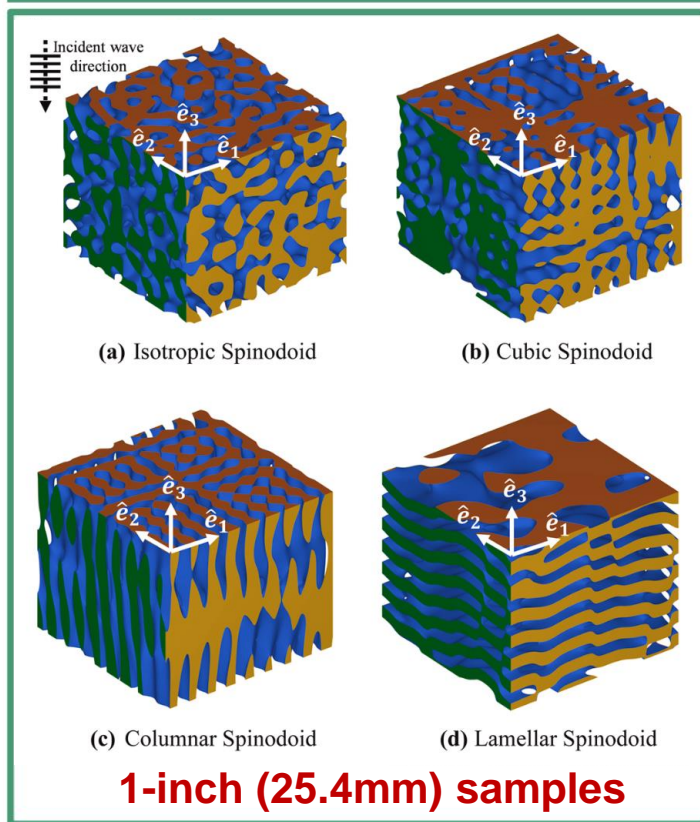
Fabrication: 3D Printing

Super-position of waves:

$$GRF = \sum_{i=1}^N \sqrt{\frac{2}{N}} \cos[(x_{w,i} \cdot x)\beta + \varphi_{w,i}] \quad \varphi_b = \sqrt{2} \operatorname{erf}^{-1}(2\rho - 1)$$

Acoustics of 3D Printed Spinodoid [23]

Additively Manufactured Spinodoid Sound Absorbers



The pore network and sound absorption behavior of open-celled spinodoid structures can be tailored by altering the relative density and wavenumber parameters within their Gaussian Random Functions.

Measured normal incidence sound absorption coefficient

Johnson-Champoux-Allard (JCA) Model [24-25]

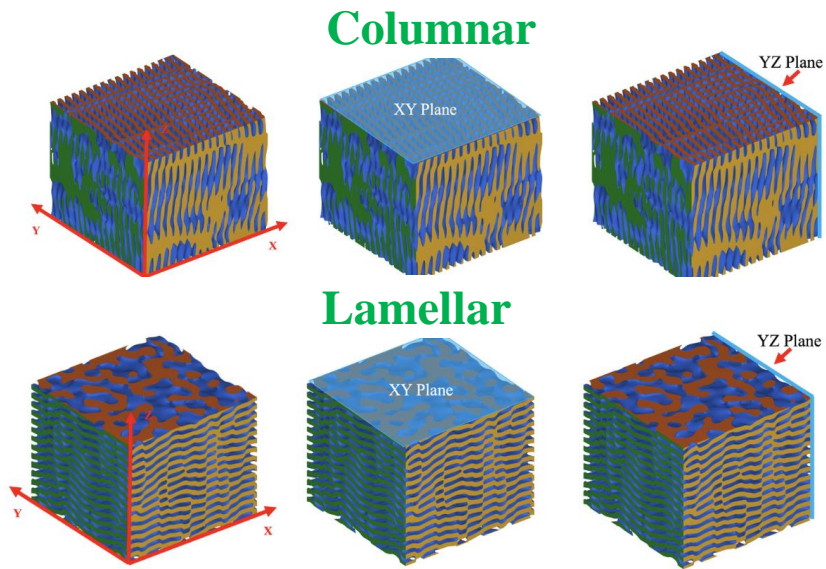
Inversely-Characterized Bulk Properties

Johnson-Champoux-Allard (JCA) Model [24-25]

Fitted sound absorption coefficient given characterized bulk properties

Anisotropic 3D Printed Spinodoid

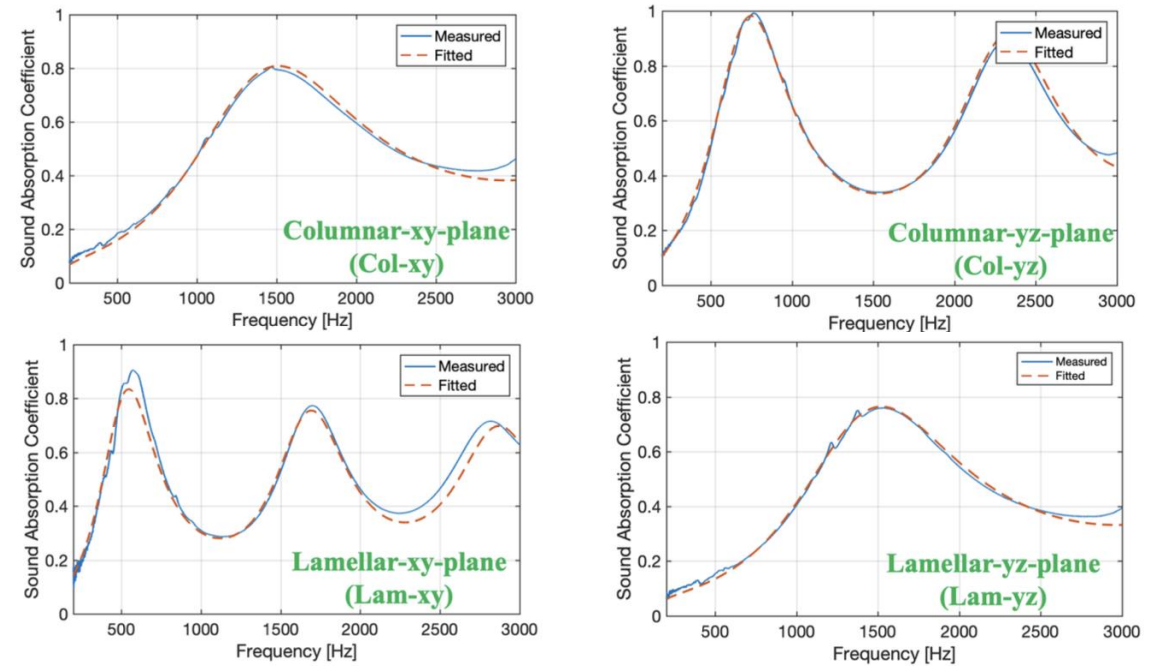
- Sound absorption measured at both XY- and YZ-plane-incidence



2-inch (50.8mm) samples

JCA Model [24-25] Fitted

Inversely-Characterized



- **Inversely-characterized properties are very different** in the XY-normal and YZ-normal directions, and are consistent with physical expectations:

	$\rho_b(\text{kg/m})^3$	ϕ	σ (Rayls/m MKS)	α_∞	Λ	Λ'
Col- xy	592	0.53	2912	1.1	323	358
Col- yz	592	0.53	14312	3.9	279	311
Lam- xy	613	0.51	30450	7.3	281	402
Lam- yz	613	0.51	2419	1.1	379	421

Note

- Bulk density, ρ_b (calculated from sample weight and volume)
- Porosity, $\phi = 1 - \rho_b/\rho_s$, $\rho_s = 1.25 \text{ g/cm}^3$ is the PLA density

Transversely-Isotropic Poro-elastic (TIP) Model

Bulk density, ρ_b
Porosity, ϕ

XY-normal direction
Flow resistivity, σ_{xy}
Tortuosity, $\alpha_{\infty xy}$
VCL, Λ_{xy}
TCL, Λ'_{xy}
Young's Modulus, E_{1xy}
Poisson's ratio, ν_{xy}
Loss factor, η_{mxy}

YZ-normal direction
Flow resistivity, σ_{yz}
Tortuosity, $\alpha_{\infty yz}$
VCL, Λ_{yz}
TCL, Λ'_{yz}
Young's Modulus, E_{1yz}
Poisson's ratio, ν_{yz}
Loss factor, η_{myz}

- JCA Model [24-25] applied for both directions
- Biot Theory [26] adapted for transversely isotropic poro-elastic media [27]

XY-normal direction
Bulk modulus, K_{fxy}
Mass coupling factors:
 $\rho_{111}, \rho_{121}, \rho_{221}$

YZ-normal direction
Bulk modulus, K_{fyz}
Mass coupling factors:
 $\rho_{112}, \rho_{122}, \rho_{222}$

Fluid coefficients:
 M, Q, R
Elastic coefficients:
 A, C, F, N, G

- Solution of characteristic dispersion equation

- Solution of amplitude coefficients of field variables

Wavenumbers:
 $k_1, k_2 = -k_1,$
 $k_3, k_4 = -k_3,$
 $k_5, k_6 = -k_5$
Amplitude coefficients:
 $\alpha_i, \beta_i, \gamma_i, i=1,2,3$

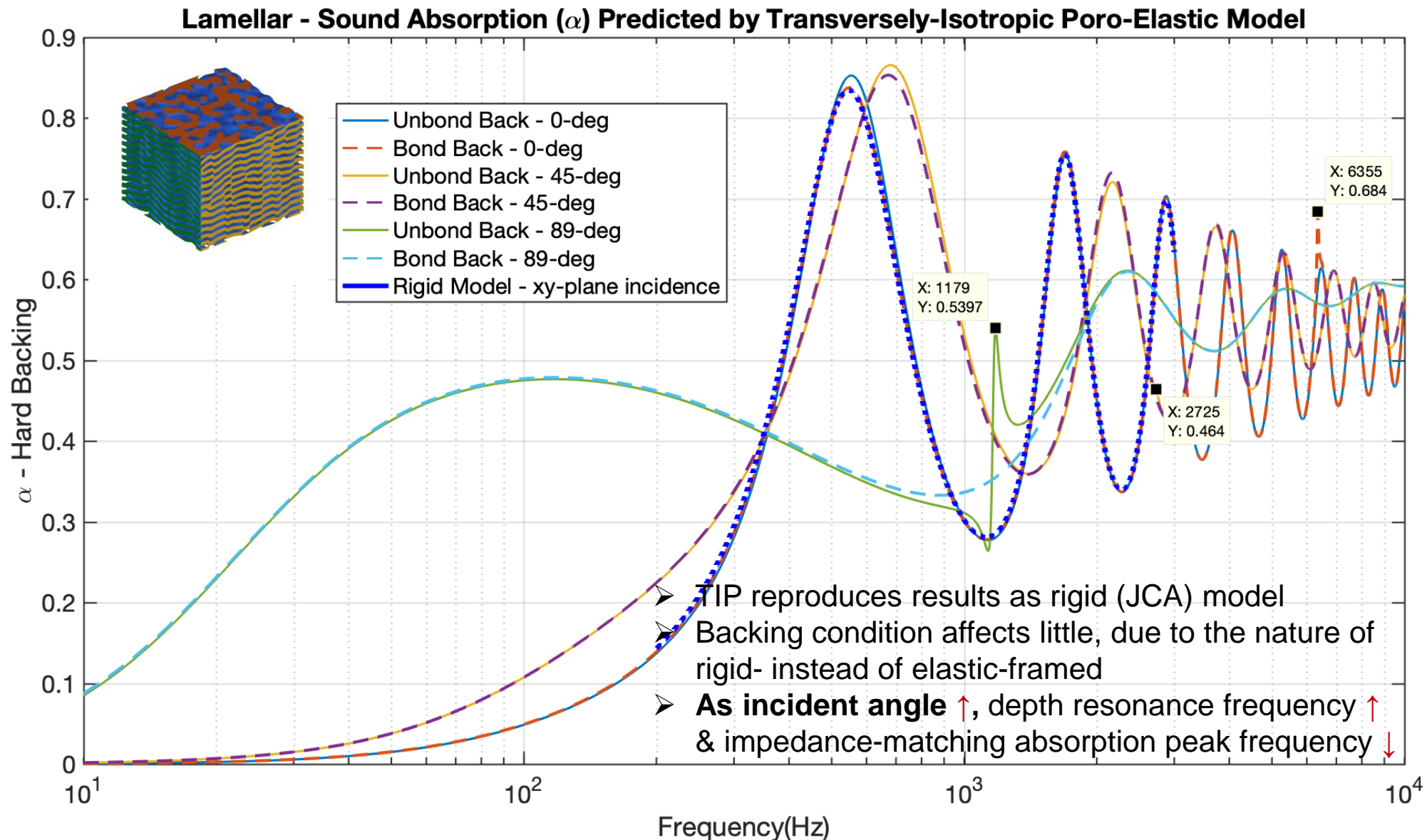
Note: In this study, Large but finite stiffness ($E_1=10^9\text{Pa}$, $\nu=0.1$, $\eta_m=0.01$) was given at anisotropic spinodoid's both directions to make it "rigid-framed"

- Boundary condition coupling by the transfer matrix method (TMM) [28] or the arbitrary coefficient method (ACM) [29]

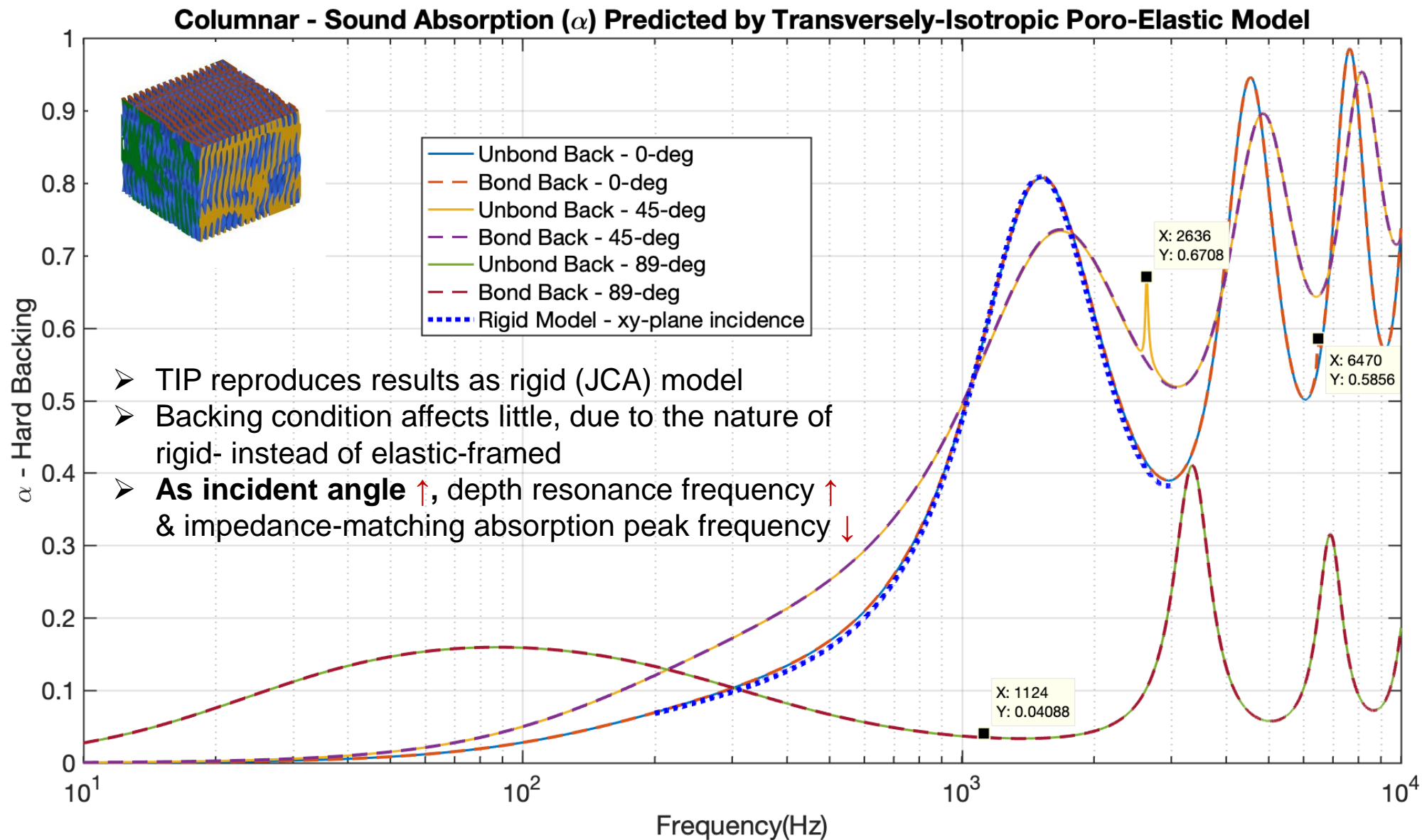


Sound absorption coefficients

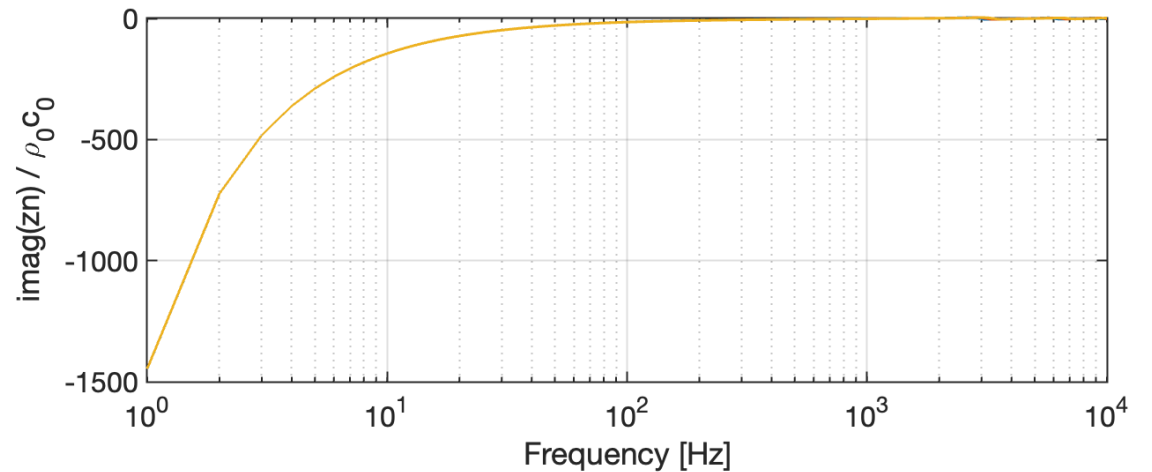
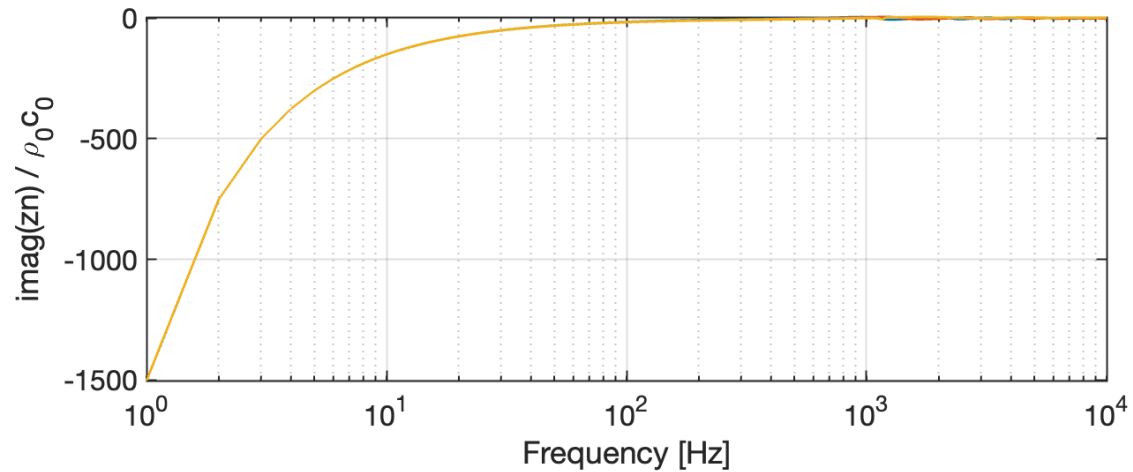
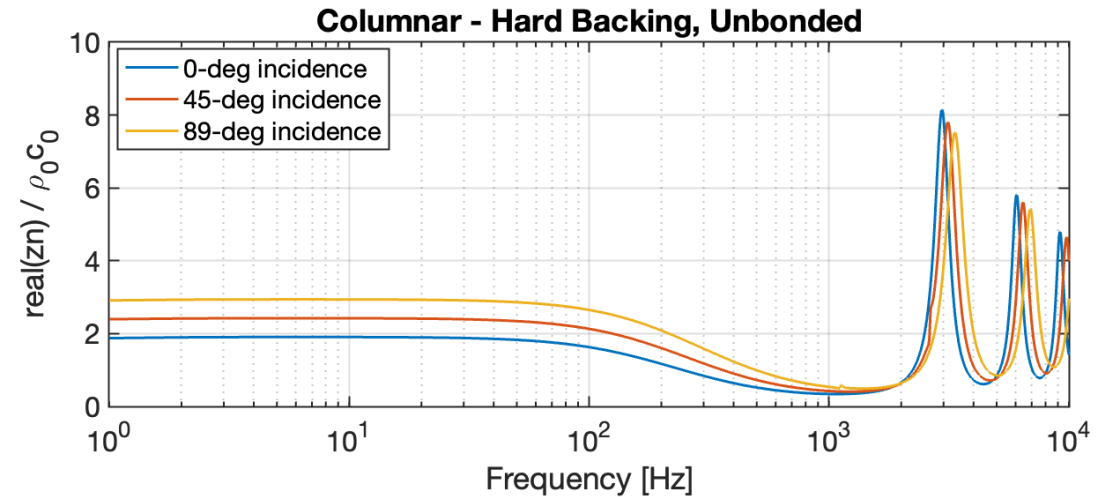
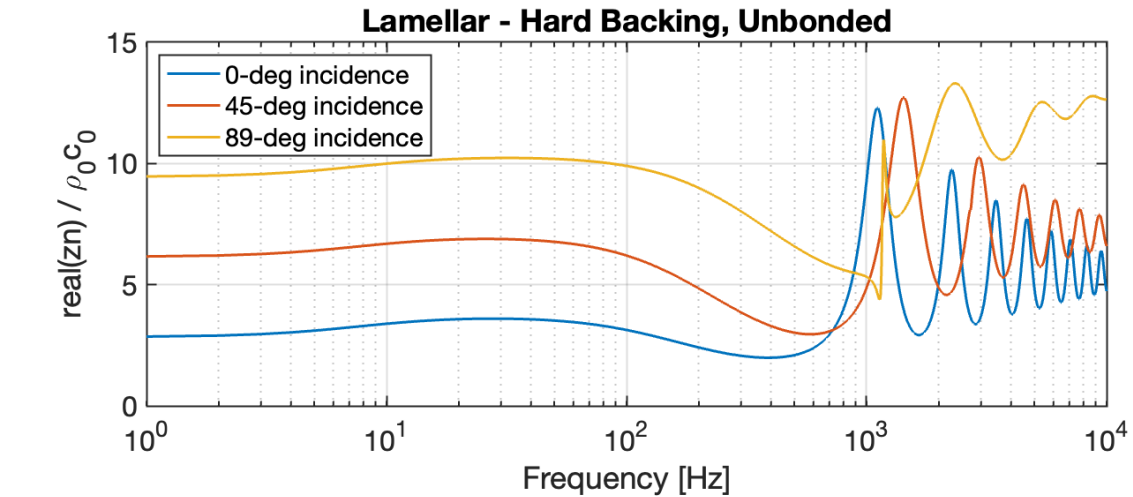
Sound Absorption Prediction by TIP



Sound Absorption Prediction by TIP



Surface Normal Impedance Normalized by $\rho_0 c_0$



➤ **Columnar is almost locally reacting, and may potentially perform well in duct lining applications**

Summary

- 3D printed spinodoid shows good broadband sound absorption performance, while holding potentials in such as optimization flexibility, structural durability, etc.
- Fully-isotropic spinodoids' acoustical performance can be accurately characterized and predicted by the JCA model
- **Transversely-isotropic poro-elastic (TIP) model developed based on the Biot theory** is capable of predicting sound absorption for anisotropic spinodoids: i.e., columnar and lamellar
- The **acoustic anisotropy analyzed by the TIP model** proved locally-reacting acoustical feature and random incidence sound absorption potentials of columnar spinodoids
- Future work:
 - Examine columnar locally-reacting advantage by random incidence and duct lining tests
 - 3D printing and acoustic modeling of gradient spinodoid
- **For more information, please refer to the our publication in *Additive Manufacturing* [23] and Brittany's thesis [30]**
- **Presentation will be available on Herrick E-Pubs: <http://docs.lib.purdue.edu/herrick/>**

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**THANK YOU
FOR YOUR ATTENTION!**